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PROPELLANT SURVEILLANCE REPORT MINUTEMAN III STAGE III, (U)  
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1 OF 3  
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1	2	3	4	5	6	7	8	9	10
11	12	13	14	15	16	17	18	19	20
21	22	23	24	25	26	27	28	29	30
31	32	33	34	35	36	37	38	39	40
41	42	43	44	45	46	47	48	49	50
51	52	53	54	55	56	57	58	59	60
61	62	63	64	65	66	67	68	69	70
71	72	73	74	75	76	77	78	79	80
81	82	83	84	85	86	87	88	89	90
91	92	93	94	95	96	97	98	99	100

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MINUTEMAN III STAGE III

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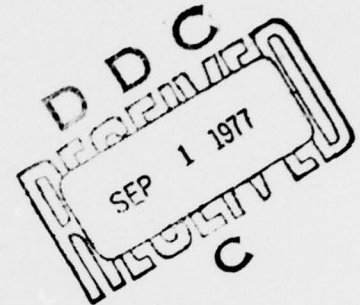
PROPELLANT SURVEILLANCE REPORT  
MINUTEMAN III STAGE III

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## ABSTRACT

This report contains test results from testing of Minuteman III, Stage III propellant manufactured by Aerojet Solid Propulsion Company and Thiokol Corporation, Wasatch Division. These results are compared statistically with propellant of similar ages from Minuteman II Stage II.

Regressions are given for only statistically significant parameters from very low rate tensile, high rate biaxial tensile under pressure, stress relaxation and thermal coefficient of linear expansion tests. There are some significant regressions in each of these tests.

Case liner bonds also show significant changes which are potentially life limiting.

Significant changes in other parameters may be the result of limited testing, both in numbers and ages.

Analysis of covariance for test data from lined and unlined cartons of Stage II and Stage III propellant and for the four tests listed above are given in the statistical appendix.

# TABLE OF CONTENTS

<u>Section</u>		<u>Page</u>
	Abstract	ii
	List of Tables	iv
	List of Figures	viii
	List of References	xi
	Glossary of Abbreviations & Terms	xiii
I	Introduction	1-1
II	Test Program	2-1
III	Statistical Summary & Conclusions	3-1
IV	Very Low Rate Tensile	4-1
V	High Rate Triaxial Tensile	5-1
VI	Stress Relaxation	6-1
VII	Thermal Coefficient of Linear Expansion	7-1
VIII	Case Liner Bonds	8-1
A	Appendix - Analysis of Covariance	A-1

# LIST OF TABLES

<u>Table Nr</u>		<u>Page</u>
1-1	Alert Limits for Possible Failure Modes	1-2
2-1	Plot Symbol Legend	2-2
3-1	Regression Analysis Summary of Significance	3-6
8-1	Summary of Regression Analysis, Stress	8-2
	Stress vs Time to Failure	
Appendix	Analysis of Covariance Tables	
	Very Low Rate Tensile	
A-A	Summary of Significance	A-2
A-1	ANT Lined vs Unlined Cartons Max Stress	A-3
A-2	ANT Lined vs Unlined Cartons Strain at Rupture	A-4
A-3	ANT Lined vs Unlined Cartons, Modulus	A-5
A-4	ANB vs ANT Lined Cartons, Max Stress	A-6
A-5	ANB vs ANT Lined Cartons, Strain at Rupture	A-7
A-6	ANB vs ANT Lined Cartons, Modulus	A-8
A-7	ANA vs ANB Unlined Cartons, Max Stress	A-9
A-8	ANA vs ANB Unlined Cartons, Strain at Rupture	A-10
A-9	ANA vs ANB Unlined Cartons, Modulus	A-11
A-10	ANA vs ANB & ANT Unlined Cartons, Max Stress	A-12
A-11	ANA vs ANB & ANT Unlined Cartons, Strain at Rupture	A-13
A-12	ANA vs ANB & ANT Unlined Cartons, Modulus	A-14
A-13	ANB Lined Cartons, Lot-to-Lot, Max Stress	A-15
A-14	ANB Lined Cartons, Lot-to-Lot, Strain at Rupture	A-16
A-15	ANB Lined Cartons, Lot-to-Lot, Modulus	A-17
A-16	ANT Lined Cartons, Lot-to-Lot, Max Stress	A-18



# LIST OF TABLES (cont)

<u>Table Nr.</u>		<u>Page</u>
A-17	ANT Lined Cartons, Lot-to-Lot, Strain at Rupture	A-19
A-18	ANT Lined Cartons, Lot-to-Lot, Modulus	A-20
A-19	ANA Unlined Cartons, Lot-to-Lot, Max Stress	A-21
A-20	ANA Unlined Cartons, Lot-to-Lot, Strain at Rupture	A-22
A-21	ANA Unlined Cartons, Lot-to-Lot, Modulus	A-23
A-22	ANB Unlined Cartons, Lot-to-Lot, Max Stress	A-24
A-23	ANB Unlined Cartons, Lot-to-Lot, Strain at Rupture	A-25
A-24	ANB Unlined Cartons, Lot-to-Lot, Modulus	A-26
A-25	ANT Unlined Cartons, Lot-to-Lot, Max Stress	A-27
A-26	ANT Unlined Cartons, Lot-to-Lot, Strain at Rupture	A-28
A-27	ANT Unlined Cartons, Lot-to-Lot, Modulus	A-29
	High Rate Triaxial Tensile	
A-28	ANT Lined vs Unlined Cartons, Max Stress	A-30
A-29	ANT Lined vs Unlined Cartons, Strain at Rupture	A-31
A-30	ANT Lined vs Unlined Cartons, Modulus	A-32
A-31	ANB vs ANT Lined Cartons, Max Stress	A-33
A-32	ANB vs ANT Lined Cartons, Strain at Rupture	A-34
A-33	ANB vs ANT Lined Cartons, Modulus	A-35
A-34	ANA vs ANB Unlined Cartons, Max Stress	A-36
A-35	ANA vs ANB Unlined Cartons, Strain at Rupture	A-37
A-36	ANA vs ANB Unlined Cartons, Modulus	A-38
A-37	ANA vs ANB & ANT Unlined Cartons, Max Stress	A-39
A-38	ANA vs ANB & ANT Unlined Cartons, Strain at Rupture	A-40
A-39	ANA vs ANB & ANT Unlined Cartons, Modulus	A-41
A-40	ANB Lined Cartons, Lot-to-Lot, Max Stress	A-42
A-41	ANB Lined Cartons, Lot-to-Lot, Strain at Rupture	A-43



# LIST OF TABLES (cont)

<u>Table Nr.</u>		<u>Page</u>
A-42	ANB Lined Cartons, Lot-to-Lot, Modulus	A-44
A-43	ANT Lined Cartons, Lot-to-Lot, Max Stress	A-45
A-44	ANT Lined Cartons, Lot-to-Lot, Strain At Rupture	A-46
A-45	ANT Lined Cartons, Lot-to-Lot, Modulus	A-47
A-46	ANA Unlined Cartons, Lot-to-Lot, Max Stress	A-48
A-47	ANA Unlined Cartons, Lot-to-Lot, Strain at Rupture	A-49
A-48	ANA Unlined Cartons, Lot-to-Lot, Modulus	A-50
A-49	ANB Unlined Cartons, Lot-to-Lot, Max Stress	A-51
A-50	ANB Unlined Cartons, Lot-to-Lot, Strain at Rupture	A-52
A-51	ANB Unlined Cartons, Lot-to-Lot, Modulus	A-53
A-52	ANT Unlined Cartons, Lot-to-Lot, Max Stress	A-54
A-53	ANT Unlined Cartons, Lot-to-Lot, Strain at Rupture	A-55
A-54	ANT Unlined Cartons, Lot-to-Lot, Modulus	A-56
	Stress Relaxation Modulus, 1% Strain	
A-55	ANT Lined vs Unlined Cartons - 10 sec	A-57
A-56	ANT Lined vs Unlined Cartons - 100 sec	A-58
A-57	ANB vs ANT Lined Cartons - 10 sec	A-59
A-58	ANB vs ANT Lined Cartons - 1000 sec	A-60
A-59	ANA vs ANB Unlined Cartons - 10 sec	A-61
A-60	ANA vs ANB Unlined Cartons - 1000 sec	A-62
A-61	ANA vs ANB & ANT Unlined Cartons - 10 sec	A-63
A-62	ANA vs ANB & ANT Unlined Cartons - 1000 sec	A-64

# LIST OF TABLES (cont)

<u>Table Nr.</u>		<u>Page</u>
A-63	ANT Lined Cartons, Lot-to-Lot, 10 sec	A-65
A-64	ANT Lined Cartons, Lot-to-Lot, 1000 sec	A-66
A-65	ANA Unlined Cartons, Lot-to-Lot, 10 sec	A-67
A-66	ANA Unlined Cartons, Lot-to-Lot, 1000 sec	A-68
A-67	ANT Unlined Cartons, Lot-to-Lot, 10 sec	A-69
A-68	ANT Unlined Cartons, Lot-to-Lot, 1000 sec	A-70
	TCLE	
A-69	ANT Lined vs Unlined Cartons, Above Tg	A-71
A-70	ANT Lined vs Unlined Cartons, Tg	A-72
A-71	ANA Unlined vs ANB Unlined Cartons, Above Tg	A-73
A-72	ANA Unlined vs ANB Unlined Cartons, Tg	A-74
A-73	ANA vs ANB vs ANT Unlined Cartons, Above Tg	A-75
A-74	ANA vs ANB vs ANT Unlined Cartons, Tg	A-76

# LIST OF FIGURES

<u>Figure Nr.</u>		<u>Page</u>
	Data Plots, Very Low Rate Tensile	
	Strain at Rupture	
4-1	ANB vs ANT Lined Cartons	4-3
4-2	ANB Lined Cartons	4-5
4-3	ANT Lined Cartons	4-7
4-4	ANB Unlined Cartons	4-9
4-5	ANT Unlined Cartons	4-12
4-6	All ANB Cartons	4-15
	Maximum Stress	
4-7	ANA Unlined Cartons	4-20
4-8	ANB Unlined Cartons	4-23
4-9	ANT Unlined Cartons	4-26
4-10	ANB Lined Cartons	4-29
4-11	ANT Lined Cartons	4-31
4-12	All ANB Cartons	4-33
	Modulus	
4-13	ANA vs ANB Unlined Cartons	4-38
4-14	ANB vs ANT Lined Cartons	4-41
4-15	ANT Lined vs Unlined Cartons	4-43
4-16	ANB Lined Cartons	4-46
4-17	ANT Unlined Cartons	4-48
4-18	ANT Lined Cartons	4-51
4-19	All ANB Cartons	4-53

# LIST OF FIGURES (cont)

<u>Figure Nr.</u>		<u>Page</u>
	Data Plots, High Rate Triaxial Tensile	
	Strain at Rupture	
5-1	ANT Lined Cartons	5-2
5-2	ANB Lined Cartons	5-4
	Maximum Stress	
5-3	ANT Lined Cartons	5-6
5-4	ANB Unlined Cartons	5-8
5-5	ANT Unlined Cartons	5-11
	Modulus	
5-6	ANA Unlined Cartons	5-14
5-7	ANB Unlined Cartons	5-16
	Data Plots, Stress Relaxation	
	Modulus, 1% Strain, 77°F	
6-1	ANA Unlined Cartons - 10 sec	6-3
6-2	ANA Unlined Cartons - 1000 sec	6-5
6-3	ANB Unlined Cartons - 10 sec	6-7
6-4	ANB Unlined Cartons - 1000 sec	6-9
6-5	ANA vs ANB Unlined Cartons - 10 sec	6-11
6-6	ANA vs ANB Unlined Cartons - 1000 sec	6-13
6-7	ANT Lined Cartons - 10 sec	6-15
6-8	ANT Lined Cartons - 1000 sec	6-17
6-9	All ANB Cartons - 10 sec	6-19
6-10	All ANB Cartons - 1000 sec	6-22
6-11	ANB Stress Relaxation Master Plot	6-25
6-12	ANT Stress Relaxation Master Plot	6-26

# LIST OF FIGURES (cont)

<u>Figure Nr.</u>		<u>Page</u>
6-13	ANA Stress Relaxation Master Plot	6-27
6-14	Modulus vs Distance from Bond Line 10 sec	6-28
6-15	Modulus vs Distance from Bond Line 1000 sec	6-29
	Data Plots, TCLE	
7-1	ANA Unlined Cartons, Above Tg	7-2
7-2	ANB Unlined Cartons, Tg	7-4
7-3	ANT Unlined Cartons, Above Tg	7-7
7-4	ANT Unlined Cartons, Tg	7-10
7-5	ANB Lined Cartons, Above Tg	7-13
7-6	ANT Lined Cartons, Tg	7-15
7-7	ANT Lined Cartons, Below Tg	7-17
7-8	All ANB Tg Temperature	7-19
7-9	All ANB, Below Tg	7-24
	Data Plots Case Liner Bonds	
8-1	ANB Constant Load Tensile Log Time to Failure vs Log Stress at Rupture	8-3
8-2	ANB, Constant Load Shear Log Time to Failure vs Log Stress at Rupture	8-4
8-3	ANT Constant Load Tensile Log Time to Failure vs Log Stress at Rupture	8-5
8-4	ANT Constant Load Shear Log Time to Failure vs Log Stress at Rupture	8-6



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MAGCP 142 (68)	ATP Test Results LGM-30, Stage II Propellant, Wing VI, Phase I Series II	Nov 68
MAGCP 188 (70)	ATP Test Results LGM-30, Stage II Propellant, Wing VI, Phase I Series II	Jul 70
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0162-06-AS-F	Stage	
Appendix E	Motor Propellant Aging	

## GLOSSARY OF ABBREVIATIONS AND TERMS

Aging Trend	A change in properties of performance resulting from aging of material or component
ANA	Aerojet Propellant, Stage III (ANB 3066 Formulation)
ANT	Thiokol Propellant, Stage III (ANB 3066 Formulation)
ANB	Aerojet Propellant, Stage II (ANB 3066 Formulation)
ASPC	Aerojet Solid Propulsion Company
CSA	Cross Sectional Area
DB	Dogbone
Degradation	Gradual deterioration of properties or performance
E	Modulus (psi), defined as the slope of the line drawn tangent to the initial linear portion of the curve
EB	End Bonded
EGL	Effective Gage Length
$e_m$	Strain at Maximum Stress (in/in)
$e_r$	Strain at Rupture (in/in)
"F" ratio	The ratio of the variance accounted for by the regression function to the random unexplained variance. The regression function having the most significant "F" ratio is used for plotting data. The ratio is also used in detecting significant changes in random variation between succeeding time points.
JANNAF	Joint Army, Navy, NASA, Air Force Committee
MAGCP	Propellant Laboratory at OOAMA
OOALC	Ogden Air Logistics Command
Post Curing	Period up to 12-16 months after manufacture

# GLOSSARY OF ABBREVIATIONS AND TERMS (CONT.)

Regression	The general form of the regression equation is $Y = a + bx$
Regression Line	Line representing mean test values with respect to time
$S_b$	Standard error of estimate of the regression coefficient
$S_e$ or $S_{Y.X}$	Standard deviation of the data about the regression line
$S_m$	Maximum Stress (psi)
$S_r$	Stress at Rupture (psi)
Standard Deviation ( $S_y$ )	Square root of variance
Strain Rate	Crosshead speed divided by the EGL
TCC	Thiokol Chemical Corp.
"t" test	A statistical test used to detect significant differences between a measured parameter and an expected value of the parameter (determines if regression slope differs from zero at the 95% confidence level)
Variance	The sum of squares of deviations of the test results from the mean of the series after division by one less than the total number of test results
3 Sigma Band	The area between the upper and lower 3 sigma limit. It can be expected that 99.73% of the inventory represented by the test samples would fall within this range assuming that the population is normally distributed.
90-90 Band	It can be stated with 90% confidence that 90% of the inventory represented by the test samples would fall within this range assuming that the population is normally distributed



## SECTION I INTRODUCTION

### A. PURPOSE:

The purpose of testing ANB-3066 propellant, used in Minuteman II Stage II and Minuteman III Stage II and Stage III, is to monitor and evaluate aging effects on this propellant which will contribute to the operational motor serviceability prediction. Testing was performed according to General Test Directive GTD-2C, Amendment 1, and MMWR Project M83257C.

### B. BACKGROUND:

Service life testing of ANB-3066 carton propellant from Aerojet production began at Ogden ALC in 1966. When production for Minuteman III Stage II was transferred to Thiokol, the propellant samples from both Aerojet and Thiokol were tested. As lined cartons were produced these also were tested, adding propellant liner bond specimens to the program. The current report contains data from all these sources for propellant aged 13 to 72 months.

Failure criteria for ANB 3066 propellant which were developed from structural stress analysis are reiterated in Aerojet Report 0162-06SAAS-17. Inner bore hoop strain failure is the predicted failure mode. These criteria are shown in Table 1-1.



## SECTION II TEST PROGRAM

Cartons representing raw material combinations were subjected to a random selection process designed to test all material lots within a two year-four test periods interval. When propellant cartons have been aged one year, they are added to the test program.

Propellant cartons are identified by source of manufacture. Stage II and III propellant manufactured by Aerojet Solid Propulsion Company is identified as ANB and ANA respectively. Thiokol Company Stage III propellant is identified as ANT. All regressions used this nomenclature and the additional information as to the type of carton, lined or unlined. Symbols identifying the carton types are given in Table 2-1.

Stage II ANB-3066 propellant has been tested for more than 10 years, but in this report only propellant up to 72 months has been used in covariance analysis to coincide with the age span of Stage III propellant. Lined and unlined cartons of ANB have been combined in regression analysis for comparison purposes and cover the time span from 13 through 137 months.

The physical-mechanical tests which relate directly to stress analysis are limited. Very low rate tensile test is related to storage conditions, and high rate rails tested under pressure relate to ignition. Stress relaxation modulus also relates to storage conditions. Thermal coefficient of linear expansion reflects some of the thermal stresses to which the motor is exposed.

Low rate uniaxial tensile tests and hardness are routine tests for all propellant. The data from these tests do not relate to structural

analyses. Poisson's ratio and cohesive tear energy tests have been applied to only a portion of the cartons. The data from these tests have not been subjected to statistical analyses. Test data for all these tests appear similar to previous test data. All these data will appear in subsequent reports.

TABLE 2 - 1  
PLOT SYMBOL LEGEND

<u>Symbol</u>	<u>Carton Type</u>
□	ANA Unlined
△	ANB Lined
×	ANB Unlined
◇	ANT Lined
*	ANT Unlined

SECTION III  
STATISTICAL SUMMARY AND CONCLUSIONS

Data analyses of all propellant tested by MANCP having the ANB 3066 formulation are contained in this report. ANB 3066 propellant is divided into three groups, each group pertaining to a specific rocket motor application. The three propellant groups are designated in this report by a three letter code as follows:

<u>Code</u>	<u>Manufacturer and System Application</u>
ANA	Aerojet: MINUTEMAN III, Stage III
ANB	Aerojet: MINUTEMAN II, Stage II
ANT	Thiokol: MINUTEMAN III, Stage III

Propellant specimens for the ANA group were taken from unlined cartons. Specimens for the ANB and ANT groups were taken from unlined cartons and also from cartons having a simulated case liner along one surface of the carton. Each propellant group is further sub-divided into propellant lots.

Laboratory test data were studied to determine if lined cartons differ from unlined cartons. The data were also examined to determine if the propellant groups (ANA, ANB and ANT) differ among themselves. The following comparisons, as directed by the project engineer, were performed to satisfy periodic service life estimate requirements:

1. Compare lined and unlined cartons of MINUTEMAN III Stage III propellant manufactured by Thiokol (ANT propellant group).
2. Compare Aerojet Stage II lined cartons (ANB propellant group) with Thiokol Stage III lined cartons (ANT propellant group).
3. Perform joint comparisons for unlined cartons from ANA, ANB and ANT propellant groups.

4. Perform lot-to-lot comparisons for unlined cartons from ANA, ANB and ANT propellant groups.
5. Perform lot-to-lot comparisons for lined cartons from ANB and ANT propellant groups. (Lined cartons are not available for ANA propellant).

Propellant age is considered a possible source of bias in laboratory test data. That is, part of the observed differences in a given test response might be ascribed to propellant age. Because of the possible age effect it was necessary to provide a means of analysis where the bias, or age effect, could be removed allowing an unbiased evaluation of the true parameter response.

Analysis of covariance was chosen as the method to determine the effect or "significance" of propellant age on the test response. The general linear regression model,  $Y = a + b(X_{ij})$ , is modified for the analysis of covariance by introducing a "correction term" into the model to adjust the data for the average effect of the variable  $X_{ij}$ . Propellant age was assigned to the variable  $X_{ij}$  in this report. The F ratio for determining the significance of the propellant age is shown in Tables A-1 thru A-74.

Similarity among carton types and among propellant groups was determined by comparing regression lines for each of the data sets. The purpose was to examine whether the linear regressions of the test response on propellant age could be regarded as the same. It is possible for the regressions to differ in slope, intercept or residual variance. Differences due to slope could indicate dissimilar aging characteristics among groups while differences due to intercept could indicate bias among the data sets.



When the regression lines were statistically similar (slopes and intercepts were not significantly different) the data sets were accepted as being equal and were combined to provide an expanded data base. A "total" or composite regression line was then used to estimate the aging trend for the combined data.

The results of the analysis of covariance used in making propellant group comparisons (previously discussed on p. 3-1) are summarized in Table A-A of the appendix and as follows:

- a. ANT lined and unlined cartons are significantly different for all observed test parameters.
- b. ANB and ANT lined cartons are significantly different for all test parameters except modulus on very low rate tensile ( $2 \times 10^{-4}$  in/min cross-head speed).
- c. Joint comparisons of ANA, ANB, and ANT unlined cartons indicate that the three groups are significantly different for all observed test parameters.
- d. The individual propellant lots are significantly different (with respect to the observed test data) for unlined cartons from ANA, ANB, and ANT propellant groups.
- e. Individual propellant lots are significantly different for lined cartons from ANB and ANT propellant groups.

Analysis of covariance tables included in the appendix may be consulted for information relating to specific F tests used in the above comparisons.

ANB 3066 propellant exhibits incomplete curing and inconsistent test results if aged less than 13 months. All data aged less than 13 months was excluded from analysis in this report.



In those cases where test data from various carton types or propellant groups could be combined, plots of the combined data and regression lines are provided. Carton types or propellant groups are differentiated on these plots with different plotting symbols. These are shown in the applicable test sections. In addition to the combined regression plots, plots of individual group regression lines have been provided for each test parameter where the regression slope is statistically significant.

The results of the linear regression analysis are summarized in Table 3-1. From this table, several conclusions can be drawn.

1. Very low rate tensile:
  - a. There is a significant increase in maximum stress for all types of ANB 3066.
  - b. There is a significant decrease in strain at rupture for lined cartons but a significant increase in unlined cartons except for ANA which showed no change.
  - c. There is a significant increase in modulus for ANB lined and ANT lined and unlined cartons.
2. High rate triaxial (rails under 600 psi  $N_2$ ):
  - a. There is a significant increase in maximum stress for all types of cartons except ANA.
  - b. There is a significant decrease in strain at rupture for ANT lined cartons.
  - c. There is a significant decrease in modulus for ANA and ANB unlined cartons.
3. Stress Relaxation Modulus:

There is a significant increase in stress relaxation modulus

for ANA and ANB unlined cartons and ANT lined cartons, indicating increased hardness in the propellant.

4. TCLE:

a. There is a significant increase in TCLE above glass point except for lined cartons of ANB.

b. There is a significant decrease in glass point for all ANT cartons and an increase for ANB unlined cartons.

5. Case Liner Bond Specimens:

Interface tensile and shear specimens show signs of early failure in some lots. These lots still must be more fully characterized.

6. Testing Conclusions:

The testing shows changes which are potentially life-limiting in the case of liner bonds. Other significant parameters may not present this problem since there is the possibility that the changes are significant because of limited testing in numbers and ages.

TABLE 3-1

REGRESSION ANALYSIS  
SUMMARY OF SIGNIFICANCE

Propellant Group	VLR Tensile			HR Triax Tensile			Stress Relax 1% Strain			TCLE	
	Sm	er	E	Sm	er	E	E <sub>10</sub>	E <sub>1000</sub>	TCLE Above Point	Glass Point	
ANA(Unlined)	Sig	N.S.	N.S.	N.S.	N.S.	Sig	Sig	Sig	Sig	N.S.	
ANB(Lined)	Sig	Sig	Sig	Sig	N.S.	N.S.	N.S.	N.S.	Sig	N.S.	
ANB(Unlined)	Sig	Sig	N.S.	Sig	N.S.	Sig	Sig	Sig	N.S.	Sig	
ANT(Lined)	Sig	Sig	Sig	Sig	Sig	N.S.	Sig	Sig	Sig	Sig	
ANT(Unlined)	Sig	Sig	Sig	Sig	N.S.	N.S.	N.S.	N.S.	Sig	Sig	

## SECTION IV

### VERY LOW RATE TENSILE

This test uses a 1/2 inch thick (1.27 cm) JANNAF dogbone. The specimens are tested at a crosshead speed of  $2 \times 10^{-4}$  in/min ( $8.5 \times 10^{-2}$  cm/sec). Very low rate tensile testing is related to strain capability for storage at 60°F.

Lined cartons show a statistically significant decrease in strain at rupture as shown in Figures 4-1, 4-2, and 4-3. The slope for the combined lined samples is less than for ANB lined cartons alone. Unlined cartons of ANB and ANT show a significant increase in strain at rupture with the slope greater for ANT than for ANB while ANA does not show a significant change (Figures 4-4 and 4-5). Strain at rupture for combined lined and unlined cartons of ANB up to 137 months shows a significant increase based upon the preponderance of unlined over lined cartons (Figure 4-6).

Maximum stress shows a significant increase (Figures 4-7 through 4-12). Slopes for ANB and ANT unlined cartons are steeper than for ANA with ANT steepest. Slopes for ANB and ANT lined cartons are similar. When ANB lined and unlined cartons are combined the slope is less than for ANB unlined and greater than for ANB lined.

There are three combinable groups for modulus, two of which have a significant increase. ANB unlined cartons and ANA unlined cartons when combined do not show a significant trend (Figure 4-13). Lined cartons of ANB and ANT show a significant increase (Figure 4-14) as do unlined and lined cartons of ANT (Figure 4-15). In this combined regression the slope and the standard deviation are larger than for dissimilar sources of lined

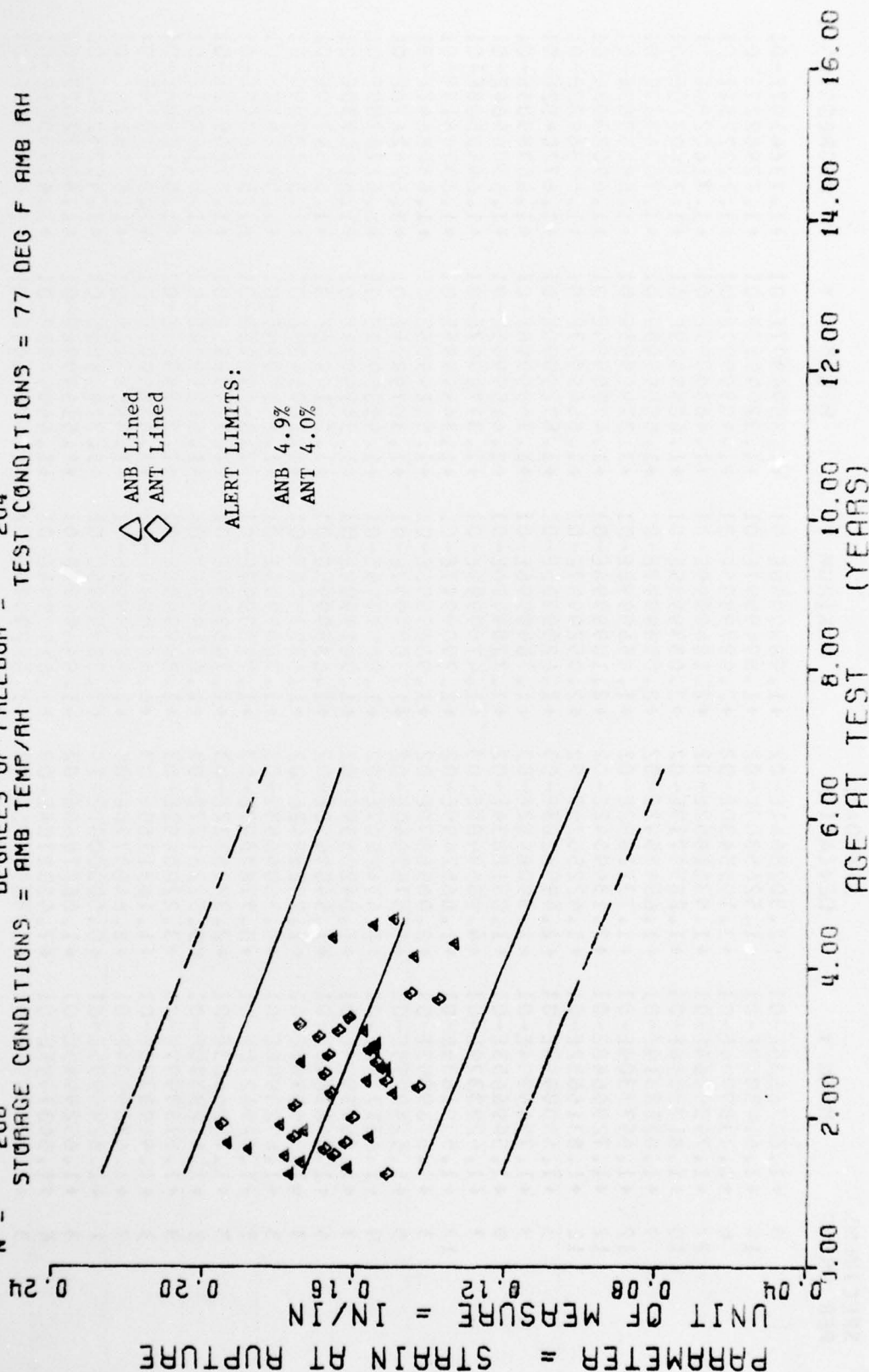


propellant cartons. There is a significant increase in modulus for ANB lined cartons and ANT unlined and lined cartons (Figures 4-16 thru 4-18). When ANB lined cartons are combined with unlined cartons, there is no significant change (Figure 4-19).

From the data cited, the similarity between lined cartons from different sources is greater than between unlined cartons from the same manufacturer.

At least for very low rate tensile testing, the conclusion that carton preparation has a greater influence on data than the source of the propellant is inescapable.

$\gamma = ((+1.8353779E-01) + (-6.5971902E-04) \times X)$   
 $F = +3.1365624E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G_1 = +1.8991157E-02$   
 $R = -3.6505260E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_1 = +1.1779640E-04$   
 $t = +5.6005021E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_2 = +1.7723800E-02$   
 $N = 206$  DEGREES OF FREEDOM = 204  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F AMB RH

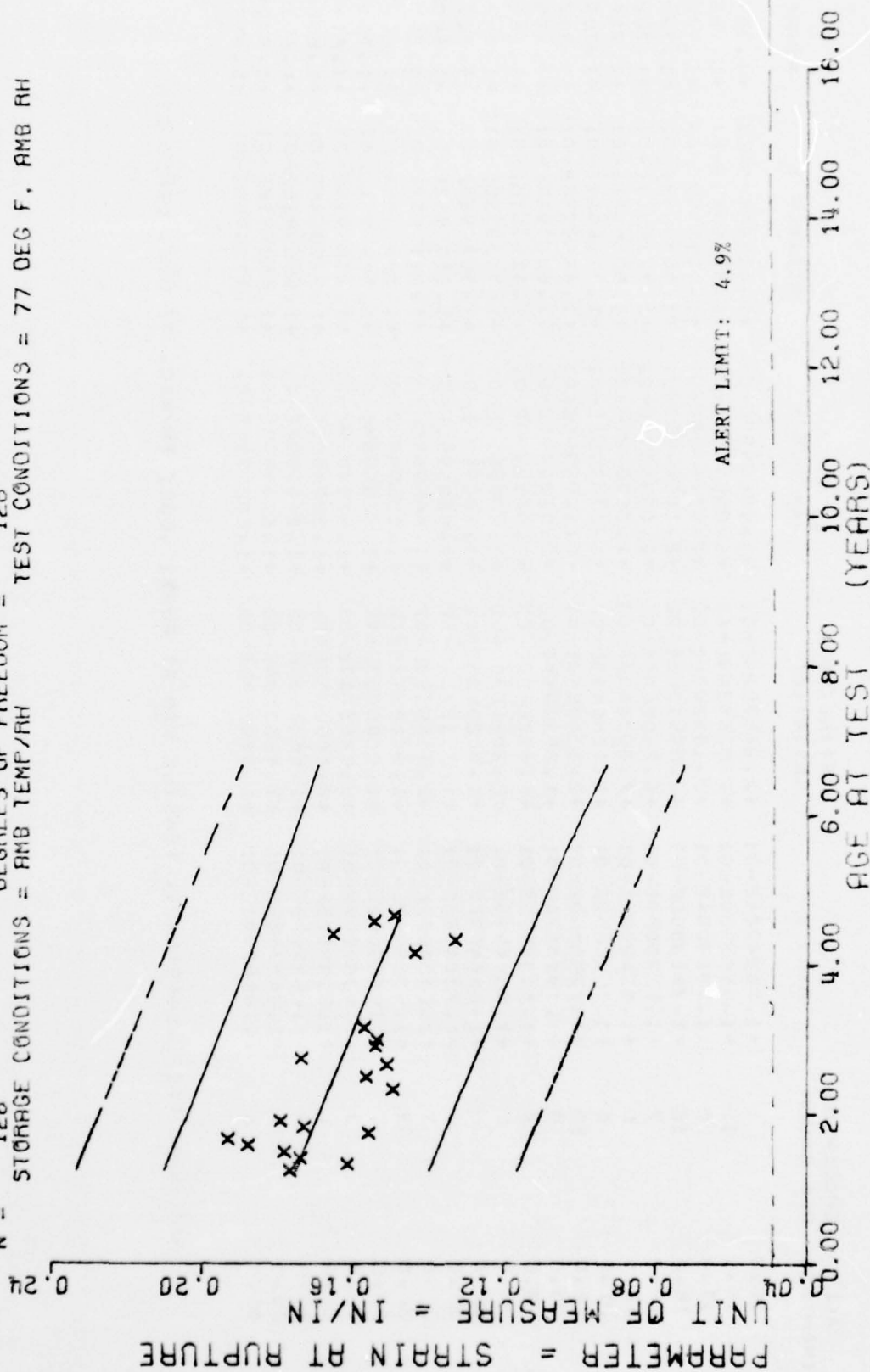


\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	9	+1.6826635E-01	+2.3028661E-02	+1.9889998E-01	+1.3595997E-01	+1.7364197E-01
16.0	15	+1.6143959E-01	+1.5265309E-02	+1.8949997E-01	+1.3299995E-01	+1.7298227E-01
17.0	6	+1.7389994E-01	+3.1955430E-02	+2.0879995E-01	+1.4099997E-01	+1.7232251E-01
18.0	22	+1.7459964E-01	+1.9351452E-02	+2.1869999E-01	+1.4639997E-01	+1.7166280E-01
19.0	10	+1.8173956E-01	+1.2854719E-02	+2.0339995E-01	+1.6085999E-01	+1.7100310E-01
20.0	9	+1.8283319E-01	+1.6847592E-02	+2.0599997E-01	+1.5555995E-01	+1.7034339E-01
21.0	12	+1.6573309E-01	+1.7372682E-02	+1.9569998E-01	+1.3795995E-01	+1.6968363E-01
22.0	12	+1.7296648E-01	+2.1349542E-02	+2.1099996E-01	+1.4799994E-01	+1.6902393E-01
23.0	12	+1.8316632E-01	+1.4225626E-02	+2.0529997E-01	+1.6645997E-01	+1.6836422E-01
24.0	3	+1.6009998E-01	+2.4955283E-03	+1.6209995E-01	+1.5725999E-01	+1.6770452E-01
26.0	3	+1.7569994E-01	+1.3908482E-03	+1.7649996E-01	+1.7409998E-01	+1.6638505E-01
28.0	9	+1.5496653E-01	+1.0318834E-02	+1.7289996E-01	+1.4155995E-01	+1.6506564E-01
29.0	3	+1.4283329E-01	+4.9059905E-03	+1.4759999E-01	+1.3775997E-01	+1.6440588E-01
30.0	12	+1.5391635E-01	+1.6652499E-02	+1.7909997E-01	+1.3435995E-01	+1.6374617E-01
31.0	3	+1.6769993E-01	+2.0656898E-02	+1.9089996E-01	+1.5129995E-01	+1.6308647E-01
32.0	9	+1.5139979E-01	+1.5757940E-02	+1.7009997E-01	+1.3079994E-01	+1.6242676E-01
33.0	9	+1.6717749E-01	+1.4342507E-02	+1.8899995E-01	+1.4935999E-01	+1.6176700E-01
34.0	3	+1.6669994E-01	+1.0420559E-02	+1.7419999E-01	+1.5475999E-01	+1.6110730E-01
35.0	6	+1.5481662E-01	+1.5489440E-02	+1.6889995E-01	+1.2615996E-01	+1.6044753E-01
36.0	3	+1.5359997E-01	+1.2928842E-02	+1.6359996E-01	+1.3895999E-01	+1.5978789E-01
37.0	3	+1.6929996E-01	+9.3604663E-03	+1.7889994E-01	+1.6019999E-01	+1.5912812E-01
38.0	7	+1.6294270E-01	+5.7787097E-03	+1.7189997E-01	+1.5695994E-01	+1.5846842E-01
39.0	3	+1.7426663E-01	+2.3238322E-03	+1.7689996E-01	+1.7249995E-01	+1.5780872E-01
40.0	3	+1.6123330E-01	+5.5228477E-03	+1.6719996E-01	+1.5625994E-01	+1.5714901E-01
43.0	3	+1.3739997E-01	+3.2200491E-03	+1.3999998E-01	+1.3375997E-01	+1.5516984E-01
44.0	3	+1.4493328E-01	+1.1631360E-03	+1.4619994E-01	+1.4389997E-01	+1.5451014E-01
50.0	3	+1.4369994E-01	+8.6483720E-03	+1.5299999E-01	+1.3589996E-01	+1.5055179E-01
52.0	1	+1.3299995E-01	+0.0000000E+19	+1.3299995E-01	+1.3299995E-01	+1.4923238E-01
53.0	3	+1.6529995E-01	+1.6627560E-02	+1.8449997E-01	+1.5569996E-01	+1.4857262E-01
55.0	4	+1.5437495E-01	+7.4682704E-03	+1.6199994E-01	+1.4499998E-01	+1.4725321E-01
56.0	3	+1.4909994E-01	+1.3692575E-03	+1.5029996E-01	+1.4755999E-01	+1.4659351E-01

$Y = ((+1.8507143E-01) + (-6.7310891E-04) \times X)$   
 $F = +1.9751294E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G_1 = +2.0959427E-02$   
 $R = -3.6812183E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $G_2 = +1.5145637E-04$   
 $t = +4.4442428E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $G_3 = +1.9564784E-02$   
 $N = 126$  DEGREES OF FREEDOM = 126  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH





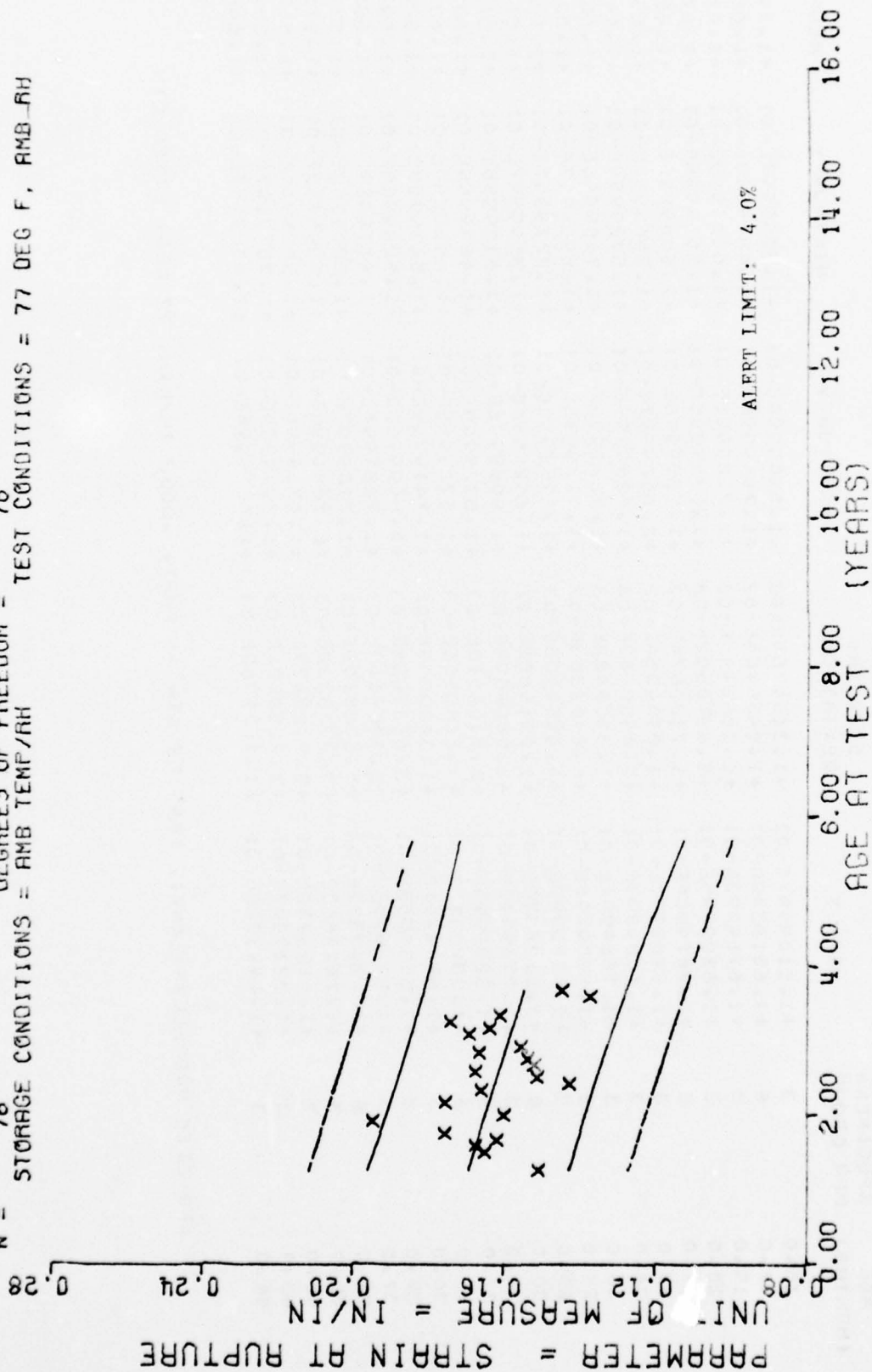
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MCHNTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	6	+1.7684984E-01	+2.2687529E-02	+1.5889998E-01	+1.4129556E-01	+1.7457479E-01
16.0	15	+1.6143959E-01	+1.5265309E-02	+1.8949997E-01	+1.3299995E-01	+1.7430168E-01
17.0	6	+1.7389994E-01	+3.1555430E-02	+2.0875955E-01	+1.4095557E-01	+1.7362856E-01
18.0	16	+1.7813098E-01	+2.0551301E-02	+2.1869999E-01	+1.4639997E-01	+1.7295545E-01
19.0	7	+1.8775689E-01	+9.7106640E-03	+2.0339955E-01	+1.7729997E-01	+1.7228233E-01
20.0	6	+1.9319993E-01	+7.3034406E-03	+2.0599997E-01	+1.8665558E-01	+1.7160922E-01
21.0	6	+1.5566558E-01	+1.1286418E-02	+1.6799998E-01	+1.3799995E-01	+1.7093610E-01
22.0	12	+1.7296648E-01	+2.1349542E-02	+2.1099996E-01	+1.4799994E-01	+1.7026299E-01
23.0	9	+1.7925524E-01	+1.3539914E-02	+2.0199996E-01	+1.6645557E-01	+1.6958587E-01
28.0	6	+1.4539993E-01	+6.4276420E-03	+1.5839999E-01	+1.4159955E-01	+1.6622436E-01
30.0	6	+1.5654993E-01	+2.1011330E-02	+1.7909997E-01	+1.3439995E-01	+1.6487812E-01
32.0	6	+1.5104997E-01	+1.9623435E-02	+1.7009997E-01	+1.3079994E-01	+1.6353189E-01
33.0	6	+1.7384988E-01	+1.2733701E-02	+1.8899995E-01	+1.6109997E-01	+1.6285884E-01
35.0	3	+1.5406662E-01	+2.4145953E-02	+1.6889995E-01	+1.2619556E-01	+1.6151261E-01
36.0	3	+1.5359997E-01	+1.2528842E-02	+1.6359996E-01	+1.3899999E-01	+1.6063949E-01
38.0	1	+1.5659994E-01	+0.000000E+71	+1.5659994E-01	+1.5659994E-01	+1.5949326E-01
50.0	3	+1.4369994E-01	+8.6483720E-03	+1.5299999E-01	+1.3585556E-01	+1.5141594E-01
52.0	1	+1.3299995E-01	+0.000000E+79	+1.3299995E-01	+1.3299995E-01	+1.5006977E-01
53.0	3	+1.6529995E-01	+1.6627560E-02	+1.8449997E-01	+1.5569996E-01	+1.4939665E-01
55.0	4	+1.5437495E-01	+7.4682704E-03	+1.6199994E-01	+1.4499998E-01	+1.4805042E-01
56.0	3	+1.4909994E-01	+1.3692575E-03	+1.5029996E-01	+1.4759999E-01	+1.4737731E-01

ANB 3066 PROPELLANT(ANB), TENSILE STN AT RUPT, .0002 IN/MIN, 77 DEG, LINED CTN

$Y = (C + 1.773086E-01) + (-5.1427393E-04) X$   
 $F = +7.0037686E+00$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = -2.9048050E-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +2.6464634E+00$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 78$  DEGREES OF FREEDOM = 76  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



ANB 3066 PROPELLANT (ANT), TENSILE STN AT RUPT, .0002 IN/MIN, 77 DEG, LINED CTN

Figure 4-3

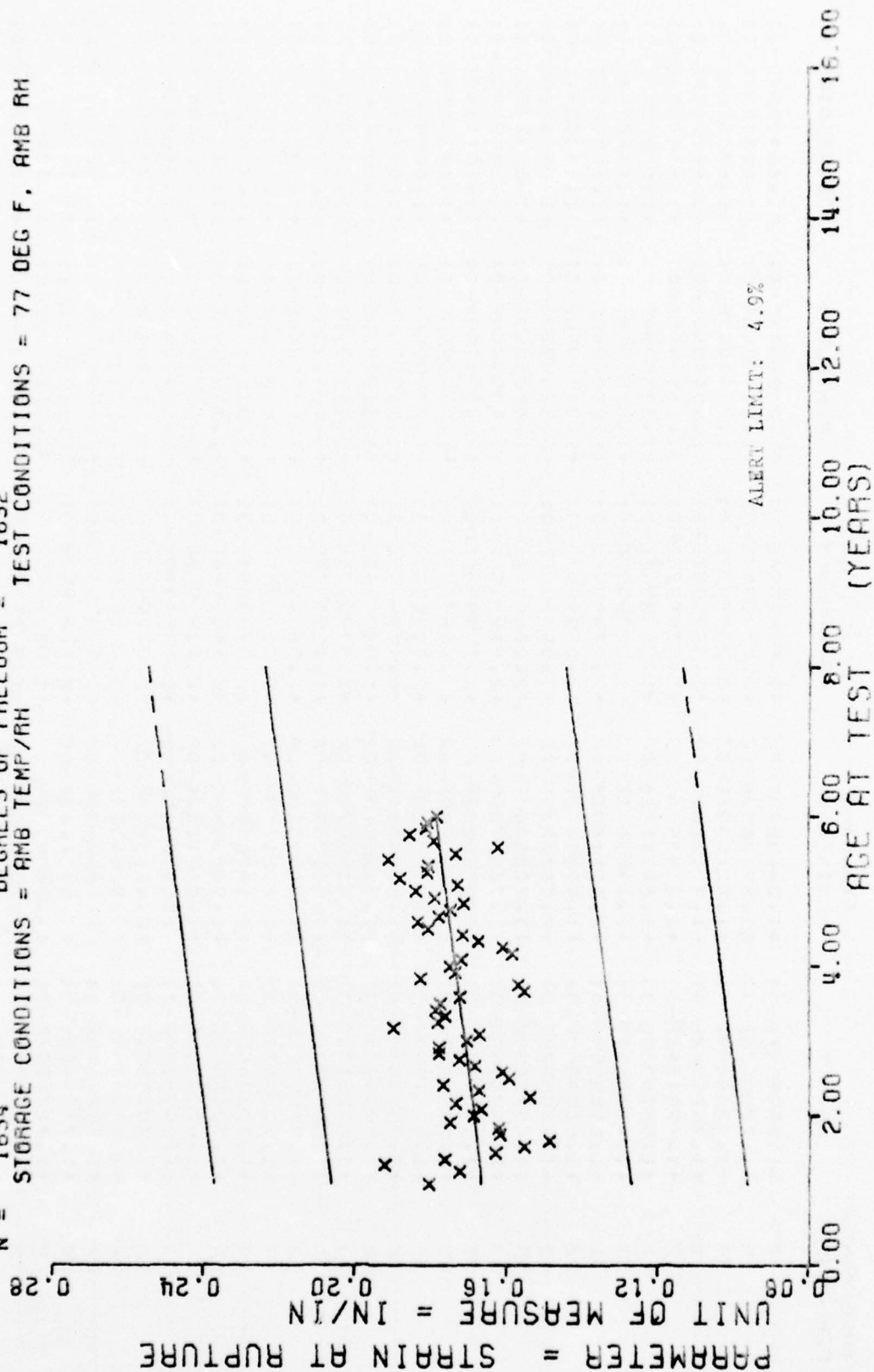
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+1.5109997E-01	+1.3084754E-02	+1.5509999E-01	+1.3599999E-01	+1.6958969E-01
18.0	6	+1.6518330E-01	+1.0459464E-02	+1.7649996E-01	+1.4849996E-01	+1.6804689E-01
19.0	3	+1.6769993E-01	+6.1568143E-03	+1.7289996E-01	+1.6089999E-01	+1.6753262E-01
20.0	3	+1.6209995E-01	+5.8940502E-03	+1.6709995E-01	+1.5559995E-01	+1.6701835E-01
21.0	6	+1.7579984E-01	+1.7125674E-02	+1.9569998E-01	+1.5469998E-01	+1.6650408E-01
23.0	3	+1.9489997E-01	+1.0204350E-02	+2.0529997E-01	+1.8489998E-01	+1.6547554E-01
24.0	3	+1.6009998E-01	+2.4552833E-03	+1.6209995E-01	+1.5729999E-01	+1.6496127E-01
26.0	3	+1.7569994E-01	+1.3508482E-03	+1.7649996E-01	+1.7409998E-01	+1.6393274E-01
28.0	3	+1.6609996E-01	+6.6102383E-03	+1.7289996E-01	+1.5969997E-01	+1.6290414E-01
29.0	3	+1.4283329E-01	+4.5059905E-03	+1.4759999E-01	+1.3779997E-01	+1.6238587E-01
30.0	6	+1.5128326E-01	+1.2315588E-02	+1.6529996E-01	+1.3599999E-01	+1.6187560E-01
31.0	3	+1.6769993E-01	+2.0656898E-02	+1.9089996E-01	+1.5129995E-01	+1.6136133E-01
32.0	3	+1.5209996E-01	+5.4104013E-03	+1.5729999E-01	+1.4649999E-01	+1.6084706E-01
33.0	3	+1.5383327E-01	+4.0680505E-03	+1.5739995E-01	+1.4939999E-01	+1.6033279E-01
34.0	3	+1.6669994E-01	+1.0420559E-02	+1.7419999E-01	+1.5479999E-01	+1.5981853E-01
35.0	3	+1.5556663E-01	+3.8638024E-03	+1.5999996E-01	+1.5289998E-01	+1.5930426E-01
37.0	3	+1.6929996E-01	+9.3604663E-03	+1.7889994E-01	+1.6019999E-01	+1.5827572E-01
38.0	6	+1.6393327E-01	+5.6388109E-03	+1.7189997E-01	+1.5869998E-01	+1.5776145E-01
39.0	3	+1.7426663E-01	+2.3238322E-03	+1.7689996E-01	+1.7249995E-01	+1.5724712E-01
40.0	3	+1.6123330E-01	+5.5228477E-03	+1.6719996E-01	+1.5629994E-01	+1.5673285E-01
43.0	3	+1.3739997E-01	+3.2200491E-03	+1.3999998E-01	+1.3379997E-01	+1.5519005E-01
44.0	3	+1.4493328E-01	+1.1631360E-03	+1.4619994E-01	+1.4389997E-01	+1.5467578E-01

ANB 3066 PROPELLANT(ANT). TENSILE STN AT RUPT. .0002 IN/MIN. 77 DEG. LINED CTN

$F = +3.4978912E+01$        $Y = ((+1.6370765E-01) + (+2.0899598E-04) * X)$        $\sigma_1 = +2.3798226E-02$   
 $R = +1.4485653E-01$       SIGNIFICANCE OF F = SIGNIFICANT       $S_e = +3.5337415E-05$   
 $t = +5.9142973E+00$       SIGNIFICANCE OF R = SIGNIFICANT       $S_t = +2.3554431E-02$   
 $N = 1634$       SIGNIFICANCE OF t = SIGNIFICANT      DEGREES OF FREEDOM = 1632  
 STORAGE CONDITIONS = AMB TEMP/RH      TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (AMB) TENSILE STN AT RUPT, .0002 IN/MIN, 77 DEG F, UNLND CTNS

Figure 4-4



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	7	+1.8035697E-01	+1.0419620E-02	+1.9399994E-01	+1.6929957E-01	+1.6642457E-01
15.0	15	+1.7226524E-01	+1.9327693E-02	+2.0599997E-01	+1.5109955E-01	+1.6584257E-01
16.0	30	+1.9299299E-01	+1.5015996E-02	+2.2399997E-01	+1.5399957E-01	+1.6705155E-01
17.0	15	+1.7625302E-01	+1.1743220E-02	+1.9399994E-01	+1.4999957E-01	+1.6726052E-01
18.0	12	+1.6291642E-01	+2.2563594E-02	+1.9399994E-01	+1.2689955E-01	+1.6746956E-01
19.0	11	+1.5526336E-01	+1.5414152E-02	+1.9599997E-01	+1.3329994E-01	+1.6767853E-01
20.0	21	+1.4870917E-01	+1.1783641E-02	+1.7839998E-01	+1.2559999E-01	+1.6788756E-01
21.0	31	+1.6169959E-01	+2.4511490E-02	+2.0799994E-01	+1.2399956E-01	+1.6809654E-01
22.0	23	+1.6202569E-01	+1.5725423E-02	+2.0599997E-01	+1.2479956E-01	+1.6830551E-01
23.0	10	+1.7485976E-01	+2.0877204E-02	+2.0849996E-01	+1.5259999E-01	+1.6851454E-01
24.0	15	+1.6870629E-01	+1.7220843E-02	+2.0289999E-01	+1.4199955E-01	+1.6872352E-01
25.0	33	+1.6670566E-01	+1.7064729E-02	+2.0195996E-01	+1.4359999E-01	+1.6893249E-01
26.0	27	+1.7354774E-01	+1.9385037E-02	+2.1999996E-01	+1.4239956E-01	+1.6914153E-01
27.0	22	+1.5395407E-01	+1.5593140E-02	+1.5885958E-01	+1.2399955E-01	+1.6935050E-01
28.0	30	+1.6731959E-01	+2.2181709E-02	+2.0599957E-01	+1.2799956E-01	+1.6955953E-01
29.0	12	+1.7676639E-01	+1.5299611E-02	+1.5799995E-01	+1.5199955E-01	+1.6976851E-01
30.0	10	+1.5939974E-01	+1.7129615E-02	+1.8399955E-01	+1.3199956E-01	+1.6997748E-01
31.0	13	+1.6116124E-01	+1.4255979E-02	+1.9399994E-01	+1.3999998E-01	+1.7018651E-01
32.0	21	+1.6835200E-01	+1.5067091E-02	+1.9599997E-01	+1.4359999E-01	+1.7039549E-01
33.0	33	+1.7249047E-01	+1.4692510E-02	+2.0865994E-01	+1.4799954E-01	+1.7060446E-01
34.0	17	+1.7789971E-01	+1.6221263E-02	+2.1199955E-01	+1.5599955E-01	+1.7081350E-01
35.0	20	+1.7790460E-01	+1.9436782E-02	+2.0799954E-01	+1.3759954E-01	+1.7102247E-01
36.0	44	+1.7046546E-01	+1.9420044E-02	+2.1409954E-01	+1.2799956E-01	+1.7123150E-01
37.0	26	+1.6708803E-01	+1.9481163E-02	+2.1199955E-01	+1.2959999E-01	+1.7144048E-01
38.0	33	+1.8968129E-01	+1.6402884E-02	+2.1799999E-01	+1.6299999E-01	+1.7164945E-01
39.0	12	+1.7808306E-01	+2.4213908E-02	+2.0499998E-01	+1.2799956E-01	+1.7185848E-01
40.0	27	+1.7613297E-01	+3.8244556E-02	+3.0599999E-01	+1.1709957E-01	+1.7206746E-01
41.0	22	+1.7872679E-01	+1.1686693E-02	+1.5799995E-01	+1.4799954E-01	+1.7227643E-01
42.0	20	+1.7748463E-01	+1.5714440E-02	+2.1069997E-01	+1.5199955E-01	+1.7248547E-01
43.0	9	+1.7231088E-01	+1.2659257E-02	+1.9299995E-01	+1.5119999E-01	+1.7269444E-01
44.0	25	+1.5532762E-01	+1.9235538E-02	+1.9679999E-01	+1.1399996E-01	+1.7290341E-01

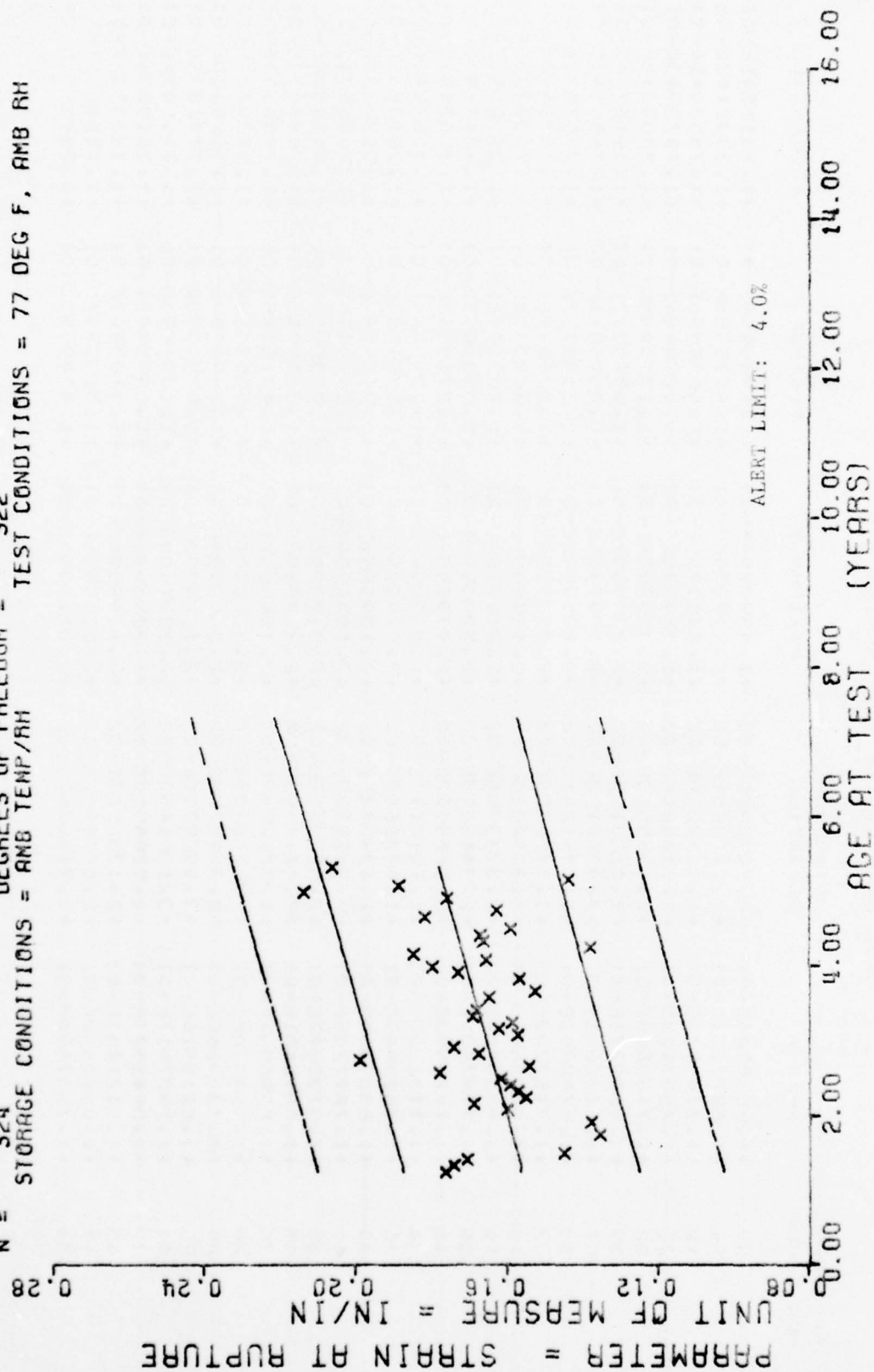
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
45.0	20	+1.5686964E-01	+2.2092980E-02	+1.5399994E-01	+1.1999994E-01	+1.7311245E-01
45.0	44	+1.8271321E-01	+2.1218051E-02	+2.3573094E-01	+1.4199995E-01	+1.7332142E-01
47.0	12	+1.7349970E-01	+1.7237205E-02	+1.5769995E-01	+1.4599996E-01	+1.7353045E-01
48.0	20	+1.7504958E-01	+2.0194668E-02	+1.8699996E-01	+1.1279994E-01	+1.7373943E-01
49.0	22	+1.7188596E-01	+2.4555513E-02	+2.3999994E-01	+1.1399996E-01	+1.7394840E-01
50.0	29	+1.5849274E-01	+3.0820163E-02	+2.2399997E-01	+1.0399997E-01	+1.7415744E-01
51.0	57	+1.6100651E-01	+3.9070103E-02	+2.1999996E-01	+9.9999964E-02	+1.7436641E-01
52.0	50	+1.6742753E-01	+1.7781341E-02	+2.1959996E-01	+1.2199997E-01	+1.7457538E-01
53.0	37	+1.7157793E-01	+1.7770688E-02	+2.0039999E-01	+1.3269996E-01	+1.7478442E-01
54.0	19	+1.8073648E-01	+2.3754936E-02	+2.1599996E-01	+1.3689994E-01	+1.7499339E-01
55.0	44	+1.8339729E-01	+2.3733086E-02	+2.2199994E-01	+1.2399995E-01	+1.7520242E-01
56.0	59	+1.7787408E-01	+2.3440098E-02	+2.3299998E-01	+1.0999995E-01	+1.7541140E-01
57.0	46	+1.7475599E-01	+2.0009052E-02	+2.0799994E-01	+1.2719994E-01	+1.7562037E-01
58.0	14	+1.7122306E-01	+1.7440113E-02	+2.0999997E-01	+1.2799996E-01	+1.7582941E-01
59.0	20	+1.7899960E-01	+1.5830866E-02	+2.0799994E-01	+1.5799999E-01	+1.7603838E-01
60.0	20	+1.8389958E-01	+1.6396725E-02	+2.1399998E-01	+1.2959999E-01	+1.7624735E-01
61.0	40	+1.7277705E-01	+2.3499183E-02	+2.1999996E-01	+1.0999995E-01	+1.7645639E-01
62.0	35	+1.8795377E-01	+2.6520363E-02	+2.3179996E-01	+1.0999995E-01	+1.7666536E-01
63.0	45	+1.8076401E-01	+2.7297793E-02	+2.3879994E-01	+1.3119995E-01	+1.7687439E-01
64.0	36	+1.8054950E-01	+1.7006843E-02	+2.1099996E-01	+1.4319998E-01	+1.7708337E-01
65.0	28	+1.9098168E-01	+2.5278450E-02	+2.5000000E-01	+1.5399998E-01	+1.7729234E-01
66.0	28	+1.7329245E-01	+2.8845798E-02	+2.3999994E-01	+1.2999999E-01	+1.7750138E-01
67.0	46	+1.6215610E-01	+3.0529775E-02	+2.1999996E-01	+1.0799998E-01	+1.7771035E-01
68.0	44	+1.7907917E-01	+3.1261405E-02	+2.5999999E-01	+1.1099994E-01	+1.7791932E-01
69.0	32	+1.8545570E-01	+1.5565560E-02	+2.2399997E-01	+1.5799999E-01	+1.7812836E-01
70.0	40	+1.8121451E-01	+2.1788523E-02	+2.6199996E-01	+1.2199997E-01	+1.7833733E-01
71.0	47	+1.8080592E-01	+2.6908443E-02	+2.5399994E-01	+1.0599994E-01	+1.7854630E-01
72.0	34	+1.7631426E-01	+1.7676768E-02	+2.0719999E-01	+1.4329999E-01	+1.7875534E-01

AND 30.66. PROPELLANT(AND) TENSILE STN AT RUPT. +0002 IN/MIN, 77 DEG F, UNLND CINS

$Y = ((+1.4937462E-01) + (+4.5271540E-04) * X)$   
 $F = +2.9249486E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $\alpha = +1.8732635E-02$   
 $R = +2.8857006E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +8.3707841E-05$   
 $t = +5.4082794E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_e = +1.7963555E-02$   
 $N = 324$  DEGREES OF FREEDOM = 322  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (ANT) TENSILE STN AT RUPT, 0.0002 IN/IN, 77 DEG F, UNLND CTN

Figure 4-5

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	1	+1.7629994E-01	+0.0000000E+71	+1.7639994E-01	+1.7639994E-01	+1.5616530E-01
16.0	3	+1.7419993E-01	+8.5454358E-03	+1.8419999E-01	+1.6739994E-01	+1.5661905E-01
17.0	2	+1.7069993E-01	+2.1281275E-03	+1.7219996E-01	+1.6919994E-01	+1.5707075E-01
18.0	3	+1.4596661E-01	+1.9038466E-02	+1.6639995E-01	+1.2959998E-01	+1.5752345E-01
21.0	3	+1.3546663E-01	+2.8113705E-03	+1.3839995E-01	+1.3279998E-01	+1.5888160E-01
23.0	3	+1.3786661E-01	+3.2349407E-03	+1.4079999E-01	+1.3439995E-01	+1.5978705E-01
25.0	3	+1.5999996E-01	+8.4272241E-03	+1.6799998E-01	+1.5119999E-01	+1.6069245E-01
26.0	17	+1.6892913E-01	+1.1218348E-02	+1.8319994E-01	+1.3799995E-01	+1.6114521E-01
27.0	33	+1.5507841E-01	+1.1200248E-02	+1.7439997E-01	+1.3199994E-01	+1.6159790E-01
28.0	22	+1.5709960E-01	+7.6840243E-03	+1.7799997E-01	+1.4639999E-01	+1.6205060E-01
29.0	8	+1.5924990E-01	+7.3804571E-03	+1.7399996E-01	+1.5039998E-01	+1.6250336E-01
30.0	15	+1.6165298E-01	+1.4151503E-02	+1.8799996E-01	+1.4559996E-01	+1.6295605E-01
31.0	30	+1.7796283E-01	+2.2530510E-02	+2.3449999E-01	+1.4479994E-01	+1.6340875E-01
32.0	22	+1.5429961E-01	+1.1200986E-02	+1.7279994E-01	+1.3079994E-01	+1.6386151E-01
33.0	5	+1.5893907E-01	+8.6661213E-03	+2.0959997E-01	+1.8569999E-01	+1.6431421E-01
34.0	15	+1.6763287E-01	+2.3727652E-02	+1.5769996E-01	+1.1679995E-01	+1.6476690E-01
35.0	11	+1.7419064E-01	+1.4494093E-02	+1.9559997E-01	+1.4639997E-01	+1.6521966E-01
37.0	4	+1.5734994E-01	+8.1139909E-03	+1.6679996E-01	+1.4699995E-01	+1.6612505E-01
38.0	3	+1.6239994E-01	+7.7140833E-03	+1.6799998E-01	+1.5359997E-01	+1.6657775E-01
39.0	3	+1.5879994E-01	+4.5468249E-03	+1.6319996E-01	+1.5359997E-01	+1.6703051E-01
40.0	1	+1.6919994E-01	+0.0000000E+51	+1.6919994E-01	+1.6919994E-01	+1.6748321E-01
41.0	6	+1.6814994E-01	+1.2680298E-02	+1.8719995E-01	+1.5119999E-01	+1.6793590E-01
43.0	3	+1.6479992E-01	+4.5552952E-03	+1.6879999E-01	+1.5919995E-01	+1.6884136E-01
44.0	4	+1.5269994E-01	+1.0420758E-02	+1.6259998E-01	+1.4339995E-01	+1.6929405E-01
46.0	6	+1.5693330E-01	+6.3065560E-03	+1.6799998E-01	+1.5119999E-01	+1.7019951E-01
47.0	10	+1.7209999E-01	+1.3812203E-02	+1.9079995E-01	+1.5679999E-01	+1.7065221E-01
48.0	6	+1.7991650E-01	+6.7499202E-03	+1.9099998E-01	+1.7299997E-01	+1.7110490E-01
49.0	5	+1.6563993E-01	+9.5680939E-03	+1.7839998E-01	+1.5359997E-01	+1.7155766E-01
50.0	9	+1.8478870E-01	+6.1775400E-03	+1.5839996E-01	+1.7679998E-01	+1.7201036E-01
51.0	3	+1.3816660E-01	+1.5619874E-03	+1.3999998E-01	+1.3609999E-01	+1.7246305E-01
52.0	3	+1.6643327E-01	+6.7678624E-03	+1.7419999E-01	+1.6179996E-01	+1.7291581E-01



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
53.0	17	+1.6729372E-01	+1.5295611E-02	+2.0059996E-01	+1.3219954E-01	+1.7336851E-01
54.0	7	+1.5915703E-01	+1.4255771E-02	+1.5239998E-01	+1.4169956E-01	+1.7382121E-01
55.0	9	+1.8178862E-01	+1.5530404E-02	+2.0089955E-01	+1.5229954E-01	+1.7472666E-01
57.0	9	+1.6276645E-01	+6.5242667E-03	+1.7069995E-01	+1.5319957E-01	+1.7517936E-01
59.0	3	+1.7586660E-01	+1.1597678E-02	+1.8909996E-01	+1.6569955E-01	+1.7608481E-01
60.0	3	+2.1369933E-01	+6.2859281E-03	+2.1929997E-01	+2.0689954E-01	+1.7653751E-01
61.0	3	+1.8866664E-01	+4.3153917E-03	+1.9349958E-01	+1.8519957E-01	+1.7699021E-01
62.0	3	+1.4433331E-01	+5.2173601E-03	+1.4789998E-01	+1.3809996E-01	+1.7744296E-01
64.0	6	+2.0605311E-01	+1.4557927E-02	+2.1839954E-01	+1.7719955E-01	+1.7834936E-01

ANR 3066 PROPELLANT(ANT) TENSILE STN AT RUPT. 0.0002 IN/MIN, 77 DEG F, UNLND CTN

$Y = (1 + 1.6371824E-01) + (1 + 2.1049035E-04) * X$   
 $F = +1.2557904E+02$  SIGNIFICANCE OF F = SIGNIFICANT  $G_1 = +2.4868294E-02$   
 $R = +2.2008608E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +1.8783374E-05$   
 $t = +1.1206205E+01$  SIGNIFICANCE OF t = SIGNIFICANT  $S_t = +2.4263451E-02$   
 $N = 2469$  DEGREES OF FREEDOM = 2467  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

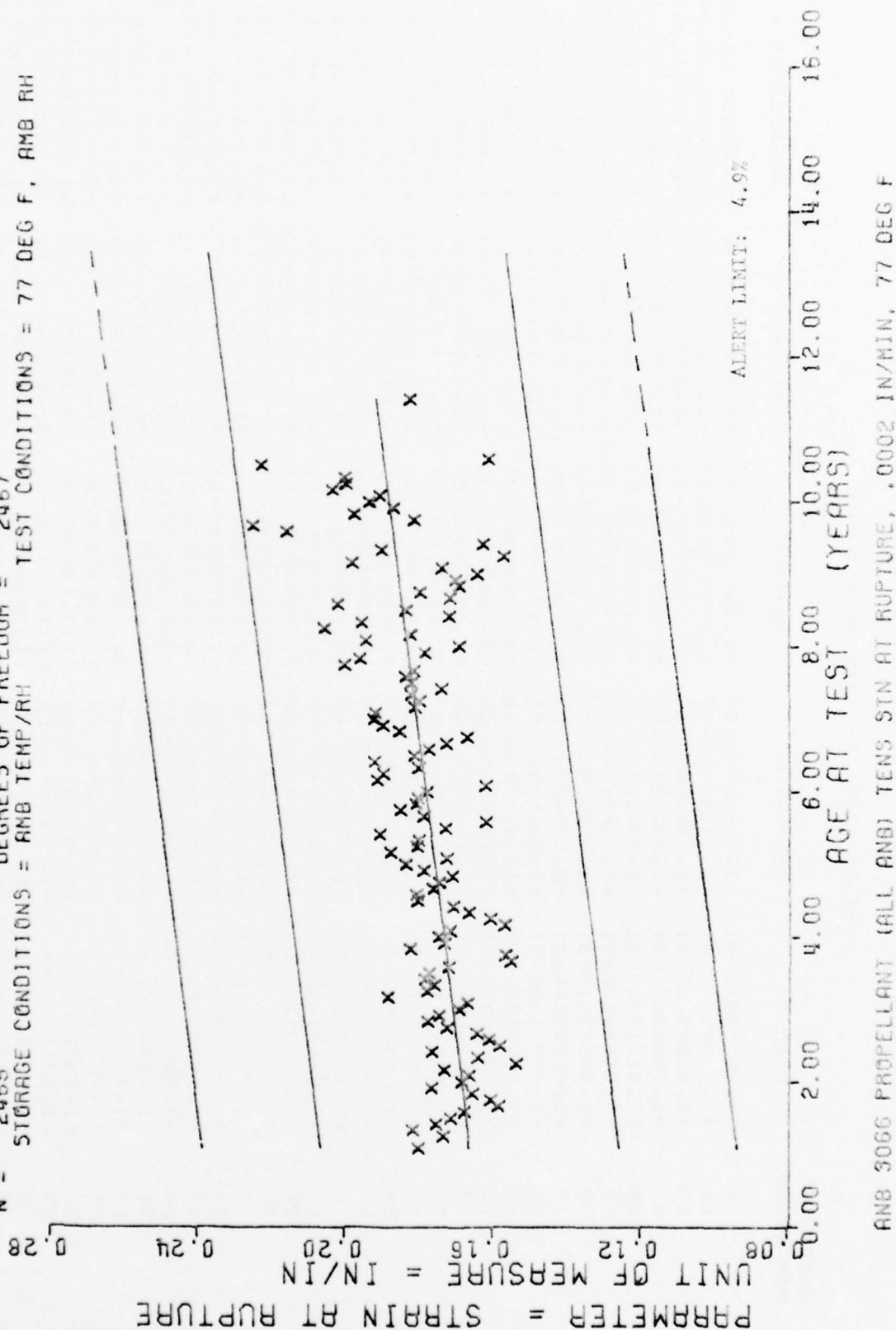


Figure 4-6

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	7	+1.8035697E-01	+1.0419620E-02	+1.9399994E-01	+1.6829957E-01	+1.6645461E-01
15.0	21	+1.7357575E-01	+1.9192339E-02	+2.0599997E-01	+1.4129996E-01	+1.6687560E-01
16.0	45	+1.8187510E-01	+2.2932069E-02	+2.2399997E-01	+1.3299955E-01	+1.6708606E-01
17.0	21	+1.7558062E-01	+1.8789349E-02	+2.0879995E-01	+1.4099957E-01	+1.6729652E-01
18.0	28	+1.7161029E-01	+2.2749496E-02	+2.1869999E-01	+1.2689955E-01	+1.6750705E-01
19.0	18	+1.6789960E-01	+2.2326174E-02	+2.0339995E-01	+1.3329954E-01	+1.6771751E-01
20.0	27	+1.5859591E-01	+2.1734157E-02	+2.0599997E-01	+1.2559998E-01	+1.6792804E-01
21.0	37	+1.6072118E-01	+2.2879600E-02	+2.0799994E-01	+1.2399955E-01	+1.6813850E-01
22.0	35	+1.6577678E-01	+2.0664273E-02	+2.1099996E-01	+1.2479956E-01	+1.6834902E-01
23.0	19	+1.7694163E-01	+1.7451774E-02	+2.0849996E-01	+1.5299999E-01	+1.6855949E-01
24.0	15	+1.6870629E-01	+1.7220843E-02	+2.0289999E-01	+1.4199955E-01	+1.6877001E-01
25.0	33	+1.6670566E-01	+1.7064729E-02	+2.0199996E-01	+1.4399999E-01	+1.6898047E-01
26.0	27	+1.7354774E-01	+1.5385037E-02	+2.1999996E-01	+1.4239996E-01	+1.6919094E-01
27.0	22	+1.5385407E-01	+1.8593140E-02	+1.9889998E-01	+1.2399955E-01	+1.6940146E-01
28.0	36	+1.6433292E-01	+2.1435593E-02	+2.0999997E-01	+1.2799956E-01	+1.6961193E-01
29.0	12	+1.7676639E-01	+1.5299011E-02	+1.9799995E-01	+1.5199955E-01	+1.6982245E-01
30.0	16	+1.5833097E-01	+1.8035537E-02	+1.8399995E-01	+1.3199956E-01	+1.7003291E-01
31.0	13	+1.6116124E-01	+1.4255979E-02	+1.9399994E-01	+1.3999998E-01	+1.7024344E-01
32.0	27	+1.6450697E-01	+1.8666485E-02	+1.9599997E-01	+1.3079994E-01	+1.7045390E-01
33.0	39	+1.7269957E-01	+1.4258270E-02	+2.0669994E-01	+1.4799994E-01	+1.7066442E-01
34.0	17	+1.7789971E-01	+1.5221263E-02	+2.1199995E-01	+1.5599995E-01	+1.7087489E-01
35.0	23	+1.7479526E-01	+2.1130133E-02	+2.0799994E-01	+1.2619956E-01	+1.7108535E-01
36.0	47	+1.6938894E-01	+1.5420894E-02	+2.1409994E-01	+1.2799956E-01	+1.7129588E-01
37.0	26	+1.6708803E-01	+1.9481163E-02	+2.1199995E-01	+1.2999999E-01	+1.7150634E-01
38.0	34	+1.8872010E-01	+1.7097072E-02	+2.1799999E-01	+1.5699994E-01	+1.7171686E-01
39.0	12	+1.7808306E-01	+2.4213908E-02	+2.0499998E-01	+1.2799996E-01	+1.7192733E-01
40.0	27	+1.7613297E-01	+3.8344596E-02	+3.0599999E-01	+1.1799957E-01	+1.7213785E-01
41.0	22	+1.7872679E-01	+1.1688693E-02	+1.9799995E-01	+1.4799994E-01	+1.7234832E-01
42.0	20	+1.7748463E-01	+1.5114440E-02	+2.1069997E-01	+1.5199995E-01	+1.7255878E-01
43.0	9	+1.7231088E-01	+1.2659257E-02	+1.9299995E-01	+1.5119999E-01	+1.7276930E-01
44.0	25	+1.5532362E-01	+1.9235538E-02	+1.9679999E-01	+1.1399956E-01	+1.7297977E-01

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
45.0	20	+1.5686964E-01	+2.2092980E-02	+1.9399994E-01	+1.1999994E-01	+1.7319029E-01
46.0	44	+1.8271321E-01	+2.1218051E-02	+2.3599994E-01	+1.4199995E-01	+1.7340075E-01
47.0	12	+1.7349970E-01	+1.7237205E-02	+1.9769996E-01	+1.4599996E-01	+1.7361128E-01
48.0	20	+1.7503958E-01	+2.0194668E-02	+1.9699996E-01	+1.1279994E-01	+1.7382174E-01
49.0	22	+1.7188596E-01	+2.4555513E-02	+2.3999994E-01	+1.1399996E-01	+1.7403227E-01
50.0	32	+1.5710586E-01	+2.9698195E-02	+2.2399997E-01	+1.0399997E-01	+1.7424273E-01
51.0	57	+1.6100651E-01	+3.0070103E-02	+2.1999996E-01	+9.9999964E-02	+1.7445319E-01
52.0	51	+1.6675245E-01	+1.6250804E-02	+2.1959996E-01	+1.2199997E-01	+1.7466372E-01
53.0	40	+1.7110705E-01	+1.7563350E-02	+2.0039999E-01	+1.3269996E-01	+1.7487418E-01
54.0	19	+1.8073648E-01	+2.3754936E-02	+2.1599996E-01	+1.3689994E-01	+1.7508471E-01
55.0	48	+1.8097877E-01	+2.4177954E-02	+2.2199994E-01	+1.2399995E-01	+1.7529517E-01
56.0	62	+1.7648178E-01	+2.3690128E-02	+2.3299998E-01	+1.0999995E-01	+1.7550569E-01
57.0	46	+1.7475599E-01	+2.0609052E-02	+2.0799994E-01	+1.2719994E-01	+1.7571616E-01
58.0	34	+1.7132306E-01	+1.7440113E-02	+2.0999997E-01	+1.2799996E-01	+1.7592668E-01
59.0	20	+1.7899960E-01	+1.6830866E-02	+2.0799994E-01	+1.5799999E-01	+1.7613714E-01
60.0	20	+1.8389958E-01	+1.6396725E-02	+2.1399998E-01	+1.2999999E-01	+1.7634761E-01
61.0	40	+1.7277705E-01	+2.3499183E-02	+2.1999996E-01	+1.0999995E-01	+1.7655813E-01
62.0	35	+1.8795377E-01	+2.6520363E-02	+2.3179996E-01	+1.0999995E-01	+1.7676860E-01
63.0	45	+1.8076401E-01	+2.7297793E-02	+2.3879998E-01	+1.3119995E-01	+1.7697912E-01
64.0	36	+1.8054950E-01	+1.7006843E-02	+2.1099996E-01	+1.4319995E-01	+1.7718958E-01
65.0	28	+1.9099169E-01	+2.5278450E-02	+2.5000000E-01	+1.5399998E-01	+1.7740011E-01
66.0	28	+1.7329245E-01	+2.8645798E-02	+2.3599994E-01	+1.2999999E-01	+1.7761057E-01
67.0	46	+1.6215610E-01	+3.0929775E-02	+2.1999996E-01	+1.0799998E-01	+1.7782109E-01
68.0	44	+1.7907917E-01	+3.1261405E-02	+2.5999999E-01	+1.1999994E-01	+1.7803156E-01
69.0	32	+1.8545579E-01	+1.5589560E-02	+2.2399997E-01	+1.5799999E-01	+1.7824202E-01
70.0	40	+1.8121451E-01	+2.1388523E-02	+2.6199996E-01	+1.2199997E-01	+1.7845255E-01
71.0	47	+1.8080592E-01	+2.6508443E-02	+2.5399994E-01	+1.0599994E-01	+1.7866301E-01
72.0	34	+1.7831426E-01	+1.7676768E-02	+2.0719999E-01	+1.4329999E-01	+1.7887353E-01
73.0	27	+1.62333658E-01	+1.5547724E-02	+1.9199997E-01	+1.1399996E-01	+1.7908400E-01
74.0	15	+1.9179958E-01	+1.2638456E-02	+2.0699995E-01	+1.6799998E-01	+1.7929452E-01
75.0	30	+1.9006609E-01	+1.7608359E-02	+2.2199994E-01	+1.3999998E-01	+1.7950499E-01

ANB 3066 PROPELLANT (ALL ANB) TENS SIN AT RUPTURE, .0002 IN./MIN. 77 DEG F



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
76.0	17	+1.8052309E-01	+9.9617969E-03	+2.0299994E-01	+1.5999996E-01	+1.7971551E-01
77.0	19	+1.9249957E-01	+2.1582643E-02	+2.4599999E-01	+1.6599994E-01	+1.7992597E-01
78.0	25	+1.8172764E-01	+2.3672027E-02	+2.3299998E-01	+1.3679999E-01	+1.8013644E-01
79.0	17	+1.7781144E-01	+2.3929570E-02	+2.2299998E-01	+1.2999999E-01	+1.8034696E-01
80.0	33	+1.7295718E-01	+2.1078770E-02	+2.1599996E-01	+1.2189996E-01	+1.8055742E-01
81.0	26	+1.6733380E-01	+2.3071100E-02	+2.1599996E-01	+1.1099994E-01	+1.8076795E-01
82.0	15	+1.8572634E-01	+1.9294208E-02	+2.2799998E-01	+1.6199994E-01	+1.8097841E-01
83.0	33	+1.9016617E-01	+2.0164813E-02	+2.3999994E-01	+1.6159999E-01	+1.8118894E-01
84.0	42	+1.9268763E-01	+2.2424166E-02	+2.5089997E-01	+1.4959996E-01	+1.8139940E-01
85.0	15	+1.9227951E-01	+1.6881057E-02	+2.0999997E-01	+1.4599996E-01	+1.8160986E-01
86.0	22	+1.8153142E-01	+1.4031415E-02	+2.0519995E-01	+1.4799994E-01	+1.8182039E-01
87.0	23	+1.8033862E-01	+3.5571556E-02	+2.6999998E-01	+1.1279994E-01	+1.8203085E-01
88.0	32	+1.8260890E-01	+3.2464416E-02	+2.6699995E-01	+8.5199952E-02	+1.8224138E-01
89.0	31	+1.7433512E-01	+1.8532494E-02	+2.3039996E-01	+1.2699997E-01	+1.8245184E-01
90.0	11	+1.8250876E-01	+2.3136175E-02	+2.1299999E-01	+1.4999997E-01	+1.8266236E-01
91.0	9	+1.8409979E-01	+1.4428929E-02	+2.1119999E-01	+1.6559994E-01	+1.8267283E-01
92.0	17	+1.8181139E-01	+1.1530091E-02	+1.9799995E-01	+1.4959996E-01	+1.8308335E-01
93.0	15	+2.0067954E-01	+2.9362383E-02	+2.8319996E-01	+1.6799998E-01	+1.8329381E-01
94.0	13	+1.9653040E-01	+2.0113837E-02	+2.2799998E-01	+1.5299999E-01	+1.8350428E-01
95.0	24	+1.7888295E-01	+2.1097116E-02	+2.1519994E-01	+1.4039999E-01	+1.8371480E-01
96.0	11	+1.6947239E-01	+2.2666155E-02	+2.1299999E-01	+1.3439995E-01	+1.8392527E-01
97.0	6	+1.9493323E-01	+1.3699310E-02	+2.1399998E-01	+1.7999994E-01	+1.8413579E-01
98.0	9	+1.8269969E-01	+2.1618974E-02	+2.1119999E-01	+1.6159999E-01	+1.8434625E-01
99.0	5	+2.0611989E-01	+2.8845961E-02	+2.4159997E-01	+1.6899996E-01	+1.8455678E-01
100.0	2	+1.9599997E-01	+5.2326007E-02	+2.3299998E-01	+1.5899997E-01	+1.8476724E-01
101.0	11	+1.7219066E-01	+1.9016205E-02	+2.0239996E-01	+1.3999998E-01	+1.8497776E-01
102.0	3	+1.8393325E-01	+8.7557784E-03	+1.9359999E-01	+1.7639994E-01	+1.8518823E-01
103.0	2	+2.0249992E-01	+1.9091691E-02	+2.1599996E-01	+1.8099995E-01	+1.8539869E-01
104.0	7	+1.7202836E-01	+4.1338857E-03	+1.7669999E-01	+1.6559994E-01	+1.8560922E-01
105.0	9	+1.8013304E-01	+2.7896107E-02	+2.2199994E-01	+1.3679999E-01	+1.8581968E-01
106.0	11	+1.6949063E-01	+5.1342709E-02	+2.5269997E-01	+9.3299984E-02	+1.8603020E-01

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
107.0	2	+1.7059993E-01	+4.8100599E-03	+1.7399996E-01	+1.6719996E-01	+1.8624067E-01
108.0	3	+1.6469997E-01	+9.9225311E-03	+1.7609995E-01	+1.5799999E-01	+1.8645119E-01
109.0	14	+1.7429971E-01	+1.0564565E-02	+1.9599997E-01	+1.5999996E-01	+1.8666166E-01
110.0	11	+1.9871789E-01	+3.2342236E-02	+2.5779998E-01	+1.6239994E-01	+1.8687218E-01
111.0	5	+1.5747994E-01	+4.1513829E-02	+2.2299998E-01	+1.1069995E-01	+1.8708264E-01
112.0	6	+1.9066649E-01	+5.4617228E-02	+2.5219994E-01	+1.1819994E-01	+1.8729311E-01
113.0	18	+1.6313850E-01	+4.2041126E-02	+2.5099998E-01	+9.1999957E-02	+1.8750363E-01
115.0	6	+2.1636658E-01	+2.9278187E-02	+2.5999999E-01	+1.9029998E-01	+1.8792462E-01
116.0	6	+2.2569972E-01	+1.5551211E-02	+2.4799996E-01	+2.0439994E-01	+1.8813508E-01
117.0	3	+1.8179994E-01	+3.9222634E-03	+1.8449997E-01	+1.7729997E-01	+1.8834561E-01
118.0	4	+1.9807493E-01	+1.2276390E-02	+2.0889997E-01	+1.8089997E-01	+1.8855607E-01
119.0	9	+1.8741083E-01	+5.7280928E-03	+1.9849997E-01	+1.6799998E-01	+1.8876659E-01
120.0	2	+1.9394999E-01	+4.4369543E-04	+1.9429999E-01	+1.9359999E-01	+1.8897706E-01
121.0	3	+1.9119999E-01	+5.1882549E-03	+1.9699996E-01	+1.8699997E-01	+1.8918752E-01
122.0	3	+2.0399993E-01	+2.9430655E-02	+2.3629999E-01	+1.7869997E-01	+1.8939805E-01
123.0	9	+2.0031088E-01	+3.1568413E-02	+2.5359994E-01	+1.6199994E-01	+1.8960851E-01
124.0	6	+2.0064973E-01	+2.7534156E-02	+2.3499995E-01	+1.5599995E-01	+1.8981903E-01
126.0	6	+2.2331649E-01	+5.0069649E-02	+2.8899997E-01	+1.5469998E-01	+1.9024002E-01
127.0	3	+1.6163331E-01	+3.0679355E-02	+1.8419998E-01	+1.2669998E-01	+1.9045048E-01
137.0	1	+1.8299996E-01	+0.0000000E+27	+1.8299996E-01	+1.8299996E-01	+1.9255536E-01

ANB 3066 PROPELLANT (ALL ANB) TENS SIN AT RUPTURE, .0002 IN/MIN, 77 DEG F

$Y = ((+7.7363761E+01) + (+8.7645405E-02) * X)$   
 F = +2.1491278E+01 SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_1 = +6.1082845E+00$   
 R = +2.7153032E-01 SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +1.8905929E-02$   
 t = +4.6358686E+00 SIGNIFICANCE OF t = SIGNIFICANT  $S_t = +5.8896721E+00$   
 N = 272 DEGREES OF FREEDOM = 270  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

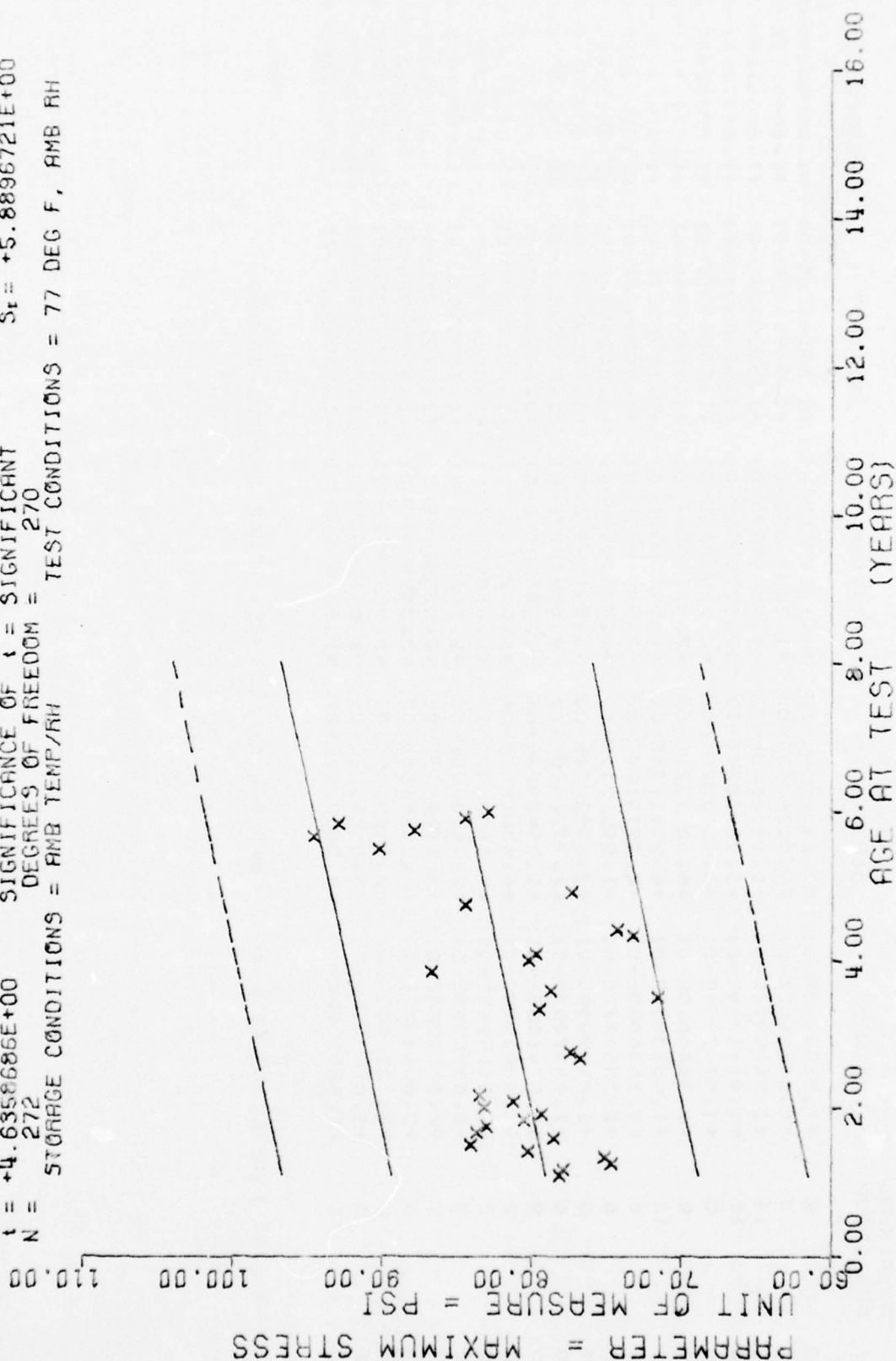


Figure 4-7

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	5	47.8129938E+01	43.0442391E+00	48.2695556E+01	47.4395553E+01	47.5103149E+01
14.0	16	47.7899948E+01	43.1051766E+00	48.2595990E+01	47.2695556E+01	47.5190759E+01
15.0	14	47.4685607E+01	43.4370305E+00	48.1195996E+01	46.5295557E+01	47.5278442E+01
16.0	5	47.5159957E+01	43.2682476E+00	47.9195996E+01	47.0195996E+01	47.9366073E+01
17.0	10	48.0269943E+01	45.1423995E+00	48.8195996E+01	47.4795557E+01	47.5453720E+01
18.0	15	48.4119918E+01	43.6621899E+00	49.2895993E+01	47.7195996E+01	47.5541366E+01
19.0	13	47.8546096E+01	46.3249474E+00	49.1595990E+01	47.1195996E+01	47.5629013E+01
20.0	12	48.3733245E+01	45.1453979E+00	49.2395993E+01	47.5000000E+01	47.5716659E+01
21.0	15	48.3039901E+01	45.6716507E+00	49.2595990E+01	47.3695996E+01	47.5804306E+01
22.0	14	48.0528503E+01	45.0795171E+00	49.1195996E+01	47.2195996E+01	47.5891952E+01
23.0	10	47.9239904E+01	43.6352626E+00	48.7895993E+01	47.5195996E+01	47.5979559E+01
24.0	10	48.3189941E+01	46.006001E+00	48.9295987E+01	46.8895553E+01	48.0067245E+01
25.0	15	48.1226593E+01	43.9112141E+00	49.0000000E+01	47.6395993E+01	48.01548E+01
26.0	15	48.3493240E+01	43.8780009E+00	49.1000000E+01	47.6595990E+01	48.02425E+01
32.0	5	47.6779922E+01	43.5791757E+00	48.1000000E+01	47.0295557E+01	48.0768491E+01
33.0	5	47.7419967E+01	42.4452230E+00	48.0395993E+01	47.3895993E+01	48.085604E+01
40.0	5	47.9505950E+01	41.5405702E+00	48.0765558E+01	47.7250000E+01	48.146957E+01
42.0	5	47.1579925E+01	43.8764027E+00	47.6645993E+01	46.6615555E+01	48.164426E+01
43.0	5	47.6759948E+01	41.2004833E+00	48.0155988E+01	47.7375989E+01	48.1732513E+01
46.0	5	48.6717864E+01	45.7864520E+01	48.7555997E+01	48.6235990E+01	48.1995437E+01
48.0	3	48.0226654E+01	44.2191657E+00	48.3075986E+01	47.5375985E+01	48.2170730E+01
49.0	7	47.5714202E+01	41.3715568E+00	48.0875989E+01	47.7459951E+01	48.2259377E+01
52.0	8	47.3221191E+01	42.6777899E+00	47.6725995E+01	46.5935996E+01	48.2521316E+01
53.0	11	47.4310606E+01	42.8511881E+00	47.9115995E+01	47.0625989E+01	48.2608963E+01
57.0	3	48.4429987E+01	48.4981377E+01	48.5295987E+01	48.3595990E+01	48.2959543E+01
59.0	5	47.7349945E+01	41.1144771E+00	47.8500000E+01	47.5865995E+01	48.3134826E+01
66.0	3	49.0196609E+01	41.0900035E+00	49.0925992E+01	48.8945996E+01	48.3748352E+01
68.0	3	49.4566578E+01	41.0548824E+00	49.5535993E+01	49.3465985E+01	48.3923645E+01
69.0	9	48.7852127E+01	44.4864500E+00	49.4545987E+01	49.0155996E+01	48.4011251E+01
70.0	8	49.2536157E+01	42.0646839E+00	49.6375989E+01	49.0095990E+01	48.4098537E+01
71.0	10	48.4428883E+01	47.0187119E+00	49.5325986E+01	47.4575986E+01	48.4186584E+01

ANB 3066 PROPELLANT(ANA), TENSILE MAX STRESS, .0002 IN./MIN, 77 DEC F, UNLAD CTN



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
72.0	3	+8.2509988E+01	+1.4826656E+00	+8.4175952E+01	+8.1279998E+01	+8.4274215E+01

ANB 3066 PROPELLANT(ANA). TENSILE MAX STRESS. .0002 IN/MIN. 77 DEG F. UNLND CTN

$F = +1.0465704E+02$   
 $R = +2.4562774E-01$   
 $t = +1.0230202E+01$   
 $N = 1632$   
 $Y = ((+7.4953221E+01) + (+1.1879981E-01) * X)$   
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM = 1630  
 STORAGE CONDITIONS = AMB TEMP/RH  
 TEST CONDITIONS = 77 DEG F, AMB RH

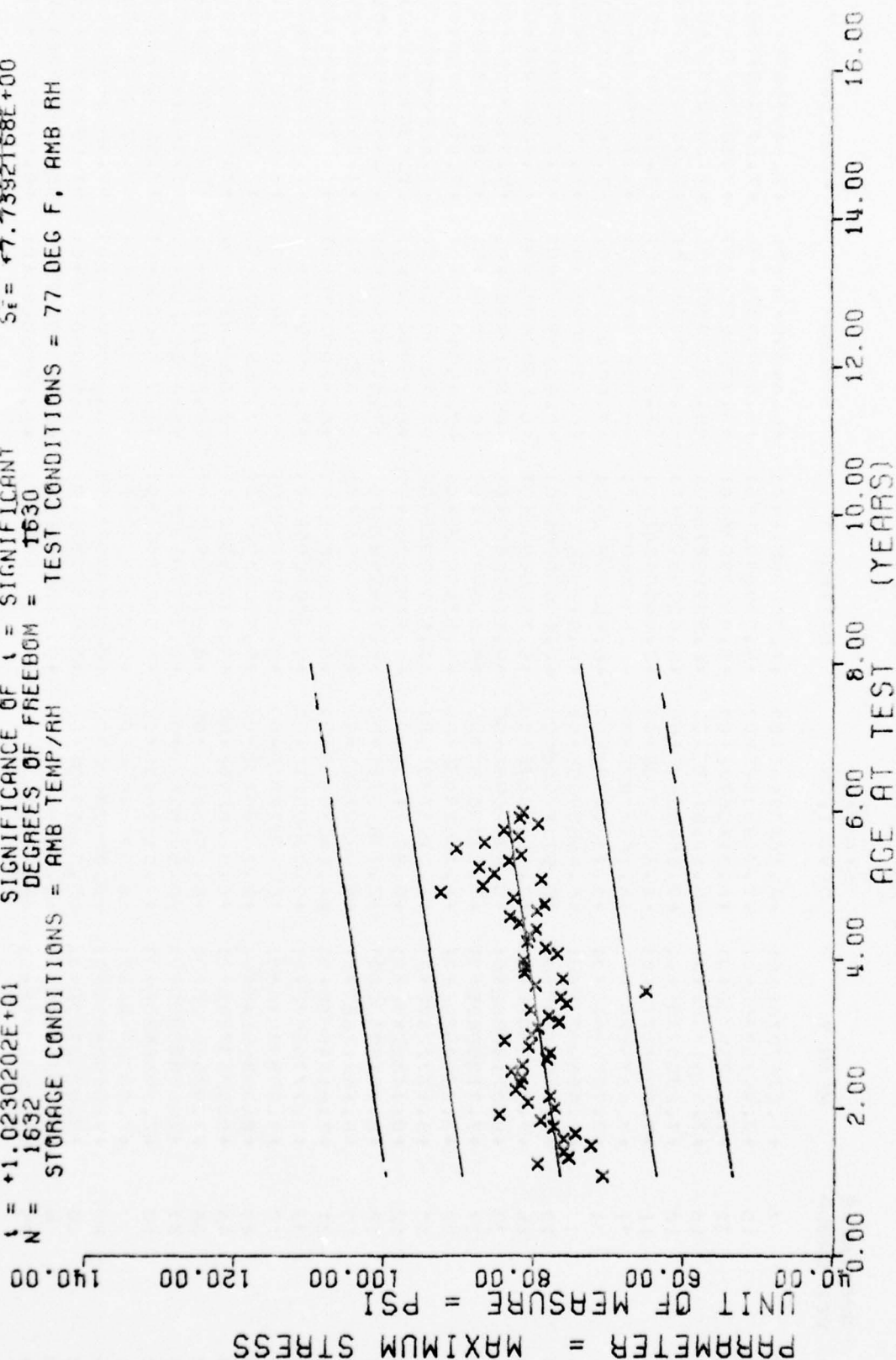


Figure 4-8

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	7	+7.0747070E+01	+4.1623244E+00	+7.7299987E+01	+6.6439987E+01	+7.6497543E+01
15.0	15	+7.9473236E+01	+7.2095352E+00	+9.0399993E+01	+6.6299987E+01	+7.6735137E+01
16.0	30	+7.5225570E+01	+8.3120671E+00	+8.9899993E+01	+5.4250000E+01	+7.6853927E+01
17.0	15	+7.5951232E+01	+8.8055137E+00	+8.8299987E+01	+5.9500000E+01	+7.6972732E+01
18.0	12	+7.2300735E+01	+7.0548569E+00	+8.6399993E+01	+5.0099900E+01	+7.7091522E+01
19.0	11	+7.5997177E+01	+2.8974313E+00	+7.9500000E+01	+7.2599990E+01	+7.7210311E+01
20.0	01	+7.4375625E+01	+6.1556707E+00	+8.5349990E+01	+6.2049987E+01	+7.7329116E+01
21.0	31	+7.7272781E+01	+4.2121273E+00	+8.4519989E+01	+7.0769989E+01	+7.7447906E+01
22.0	23	+7.9059875E+01	+6.4563950E+00	+9.0799987E+01	+6.7099990E+01	+7.7566696E+01
23.0	10	+8.4555923E+01	+5.9137795E+00	+9.1099990E+01	+7.4319992E+01	+7.7635501E+01
24.0	15	+7.7172607E+01	+7.1584867E+00	+8.7699996E+01	+6.6000000E+01	+7.7804290E+01
25.0	33	+8.0718638E+01	+5.8762098E+00	+9.1000000E+01	+6.8919998E+01	+7.7923080E+01
26.0	27	+7.7725845E+01	+7.0738828E+00	+9.0369999E+01	+6.7820085E+01	+7.8041885E+01
27.0	22	+8.2398529E+01	+6.2563343E+00	+9.5399993E+01	+7.4599990E+01	+7.8160675E+01
28.0	30	+8.1772247E+01	+1.0792770E+01	+1.0629998E+02	+4.4699990E+01	+7.8279464E+01
29.0	12	+8.1480743E+01	+5.8047124E+00	+8.9000000E+01	+6.7899993E+01	+7.8398269E+01
30.0	10	+8.2972946E+01	+3.3451370E+00	+8.7799987E+01	+7.8489990E+01	+7.8517059E+01
31.0	13	+8.1445266E+01	+4.5739158E+00	+9.0399993E+01	+7.6259994E+01	+7.8635948E+01
32.0	21	+7.8154663E+01	+4.6407963E+00	+8.6799987E+01	+6.9299987E+01	+7.8754653E+01
33.0	33	+7.7770507E+01	+9.9269201E+00	+9.3500000E+01	+5.8799987E+01	+7.8873443E+01
34.0	17	+8.0550341E+01	+6.3257201E+00	+9.0899993E+01	+7.1500000E+01	+7.8992233E+01
35.0	20	+8.3836914E+01	+3.7613813E+00	+9.1500000E+01	+7.5599990E+01	+7.9111039E+01
36.0	44	+8.0243774E+01	+6.3484296E+00	+9.6799987E+01	+6.6329986E+01	+7.9229827E+01
37.0	26	+7.9354522E+01	+6.5715818E+00	+8.9199996E+01	+6.6299987E+01	+7.9348617E+01
38.0	33	+7.6569595E+01	+6.5018167E+00	+8.7399993E+01	+6.4000000E+01	+7.9467422E+01
39.0	12	+7.7916625E+01	+1.0132610E+01	+9.5000000E+01	+6.7000000E+01	+7.9586212E+01
40.0	27	+8.0336944E+01	+6.5774631E+00	+9.2000000E+01	+7.1000000E+01	+7.9705001E+01
41.0	22	+7.5490829E+01	+6.0693368E+00	+8.5799987E+01	+6.6500000E+01	+7.9823806E+01
42.0	20	+7.6303405E+01	+5.6731970E+00	+8.8549987E+01	+6.8000000E+01	+7.9942596E+01
43.0	9	+6.4928817E+01	+1.4048470E+01	+9.2239990E+01	+5.0599990E+01	+8.0061386E+01
44.0	25	+7.9696304E+01	+6.4566581E+00	+8.9389999E+01	+6.1500000E+01	+8.0180191E+01

ANB 3066 PROPELLANT(ANB) TENSILE MAX STRESS, +0002 IN/MIN, 77 DEG F, UNLND CINS

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

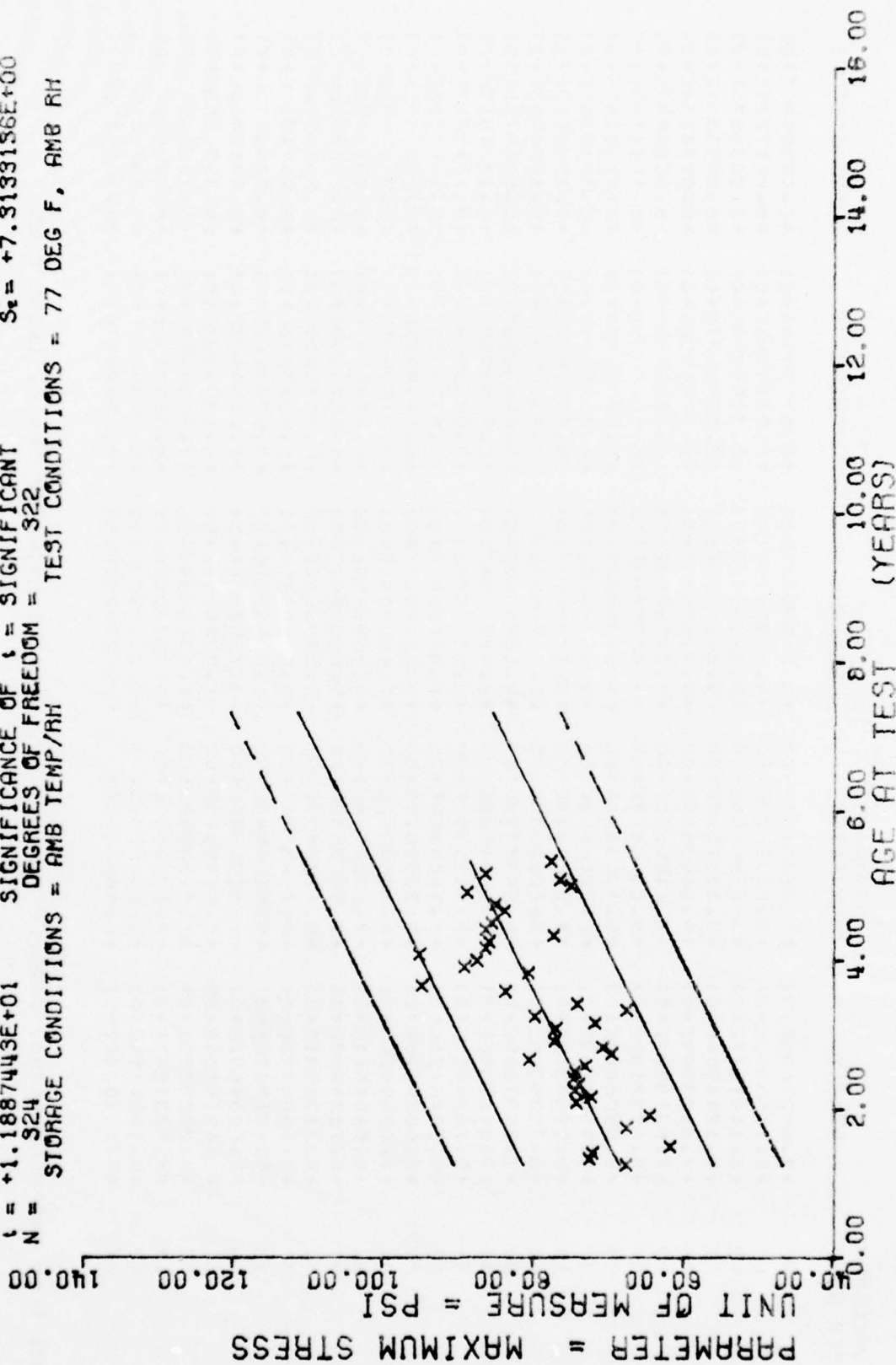
\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
45.0	20	+7.6027404E+01	+5.7595151E+00	+8.3799987E+01	+6.5759054E+01	+8.0298980E+01
46.0	44	+8.1155593E+01	+5.6097673E+00	+9.3299993E+01	+7.0199996E+01	+8.0417770E+01
47.0	12	+8.1101577E+01	+6.8296346E+00	+9.3259994E+01	+7.3199996E+01	+8.0536575E+01
48.0	20	+8.1214904E+01	+6.1397259E+00	+9.5419998E+01	+7.3299987E+01	+8.0655364E+01
49.0	22	+7.6723999E+01	+9.0693504E+00	+9.7269989E+01	+5.3199996E+01	+8.0774154E+01
50.0	29	+7.8313527E+01	+7.7125550E+00	+9.2399993E+01	+6.2899993E+01	+8.0892959E+01
51.0	57	+8.0777130E+01	+7.0747497E+00	+9.6039993E+01	+6.5019999E+01	+8.1011749E+01
52.0	50	+8.0506484E+01	+5.1203490E+00	+9.5799987E+01	+6.5799987E+01	+8.1130538E+01
53.0	37	+7.9544769E+01	+6.5216908E+00	+9.5039993E+01	+7.0159989E+01	+8.1249343E+01
54.0	19	+8.1768310E+01	+7.6525664E+00	+9.1799987E+01	+5.8799987E+01	+8.1368133E+01
55.0	42	+8.3036346E+01	+5.8206339E+00	+9.7699996E+01	+7.2299987E+01	+8.1486923E+01
56.0	59	+7.9427169E+01	+4.5957379E+00	+9.1399993E+01	+6.6666998E+01	+8.1605728E+01
57.0	46	+7.8460556E+01	+6.5721580E+00	+8.9699996E+01	+6.9399993E+01	+8.1724517E+01
58.0	34	+8.2624023E+01	+6.8119551E+00	+9.5000000E+01	+7.0909988E+01	+8.1843307E+01
59.0	20	+9.2346420E+01	+6.7405369E+00	+1.0300000E+02	+7.6729995E+01	+8.1952112E+01
60.0	20	+8.6679870E+01	+7.3399614E+00	+9.3299987E+01	+6.0899993E+01	+8.2080902E+01
61.0	40	+7.8849624E+01	+8.6978910E+00	+9.4000000E+01	+6.1199996E+01	+8.2199691E+01
62.0	35	+8.5151611E+01	+7.8220164E+00	+9.5599990E+01	+6.4899993E+01	+8.2318496E+01
63.0	45	+8.7134567E+01	+7.9507533E+00	+9.8599990E+01	+6.5599990E+01	+8.2437286E+01
64.0	36	+8.3136581E+01	+9.4503437E+00	+1.0050000E+02	+6.1500000E+01	+8.2556076E+01
65.0	28	+8.1550979E+01	+6.7543374E+00	+9.0109985E+01	+6.6500000E+01	+8.2674880E+01
66.0	28	+9.0215826E+01	+9.5156443E+00	+1.0559999E+02	+7.5799987E+01	+8.2793670E+01
67.0	46	+8.6434692E+01	+6.8096820E+00	+9.7500000E+01	+7.4299987E+01	+8.2912460E+01
68.0	44	+8.1919204E+01	+6.6299910E+00	+1.0029998E+02	+6.1399993E+01	+8.3031265E+01
69.0	32	+8.3825225E+01	+6.9233374E+00	+1.0319999E+02	+7.0599990E+01	+8.3150054E+01
70.0	40	+7.9231643E+01	+8.1702557E+00	+9.3599990E+01	+6.6099990E+01	+8.3268844E+01
71.0	47	+8.1680114E+01	+1.1563504E+01	+1.0539999E+02	+5.7599990E+01	+8.3387649E+01
72.0	34	+8.1316360E+01	+6.4662732E+00	+9.4279998E+01	+7.0399993E+01	+8.3506439E+01

ANB 3066 PROPELLANT(AND) TENSILE MAX STRESS, .0002 IN/IN, 77 DEG F, UNLND CINS



$F = +1.4131132E+02$  SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_t = +8.7588965E+00$   
 $R = +5.5227072E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_a = +3.4079094E-02$   
 $t = +1.1887443E+01$  SIGNIFICANCE OF t = SIGNIFICANT  $S_t = +7.3133156E+00$   
 $N = 324$  DEGREES OF FREEDOM = 322 TEST CONDITIONS = 77 DEG F, AMB RH  
 $Y = (( +6.2641558E+01 ) + ( +4.0511332E-01 ) * X)$  STORAGE CONDITIONS = AMB TEMP/RH



ANB 3086 PROPELLANT (ANT) TENSILE MAX STRESS, .0002 IN/MIN, 77 DEG F, UNLND CTNS

Figure 4-9

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	1	15.776989E+01	10.000000E+00	16.776989E+01	15.776989E+01	16.8718246E+01
16.0	3	17.252332E+01	13.011771E+00	17.472995E+01	16.913676E+01	16.5123367E+01
17.0	2	17.727497E+01	14.134471E+00	17.257997E+01	17.195955E+01	16.9528472E+01
18.0	3	16.190332E+01	11.221021E+00	16.314993E+01	16.070991E+01	16.9933593E+01
21.0	3	16.768331E+01	16.662090E+00	16.828999E+01	16.705997E+01	17.1143925E+01
23.0	3	16.452665E+01	14.385736E+00	16.481952E+01	16.401958E+01	17.1959152E+01
25.0	4	17.430431E+01	17.995181E+00	17.826998E+01	17.027995E+01	17.2769378E+01
26.0	17	17.235754E+01	15.741327E+00	18.006995E+01	16.500000E+01	17.3174469E+01
27.0	13	17.454437E+01	15.787139E+00	18.154596E+01	16.325957E+01	17.3579605E+01
28.0	12	17.397761E+01	16.130586E+00	18.585998E+01	16.550000E+01	17.3984725E+01
29.0	8	17.469619E+01	15.364925E+00	18.126598E+01	16.759990E+01	17.4389831E+01
30.0	15	17.449391E+01	17.519222E+00	18.050994E+01	15.519995E+01	17.4794952E+01
31.0	30	17.215156E+01	16.850291E+00	18.248999E+01	15.743098E+01	17.5200057E+01
32.0	22	18.098531E+01	15.789480E+00	19.033995E+01	15.817992E+01	17.5605178E+01
33.0	5	16.961091E+01	12.313845E+00	17.294595E+01	16.752595E+01	17.6010284E+01
34.0	15	17.091387E+01	17.808402E+00	17.909990E+01	15.226993E+01	17.6415405E+01
35.0	11	17.727355E+01	17.243549E+00	19.742995E+01	17.050995E+01	17.6820510E+01
37.0	4	17.706744E+01	19.860698E+00	19.175000E+01	17.145991E+01	17.7630737E+01
39.0	3	17.187321E+01	12.998286E+00	17.381992E+01	16.841995E+01	17.8035858E+01
40.0	3	17.090332E+01	11.950158E+00	18.186995E+01	17.796995E+01	17.8440963E+01
42.0	1	16.767092E+01	10.000000E+00	16.767092E+01	16.767092E+01	17.8846084E+01
43.0	8	17.418890E+01	11.800039E+00	17.611995E+01	17.138999E+01	17.9251130E+01
43.0	3	18.370991E+01	19.626520E+00	18.447995E+01	18.262998E+01	18.0061416E+01
44.0	4	19.483489E+01	15.755108E+00	19.003699E+02	18.957998E+01	18.0466537E+01
46.0	5	18.067324E+01	11.324528E+00	19.321995E+01	16.747995E+01	18.1276763E+01
47.0	10	18.919890E+01	18.487485E+00	19.843998E+01	17.610995E+01	18.1681869E+01
48.0	6	18.740661E+01	11.286587E+00	18.920991E+01	18.610995E+01	18.2026950E+01
49.0	5	19.517192E+01	13.002075E+00	19.838999E+01	19.111995E+01	18.2492095E+01
50.0	9	18.640876E+01	13.751514E+00	19.170999E+01	18.145991E+01	18.2897216E+01
51.0	3	18.556662E+01	11.226852E+00	18.689993E+01	18.457996E+01	18.3302322E+01
52.0	3	17.723332E+01	18.019395E+00	17.825994E+01	17.696995E+01	18.3707443E+01

AND 3000 POUNDS PER SQUARE INCH TENSILE MAX STRESS: 10000 IN/MIN: 77 DEG F: UNLND CTAS

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

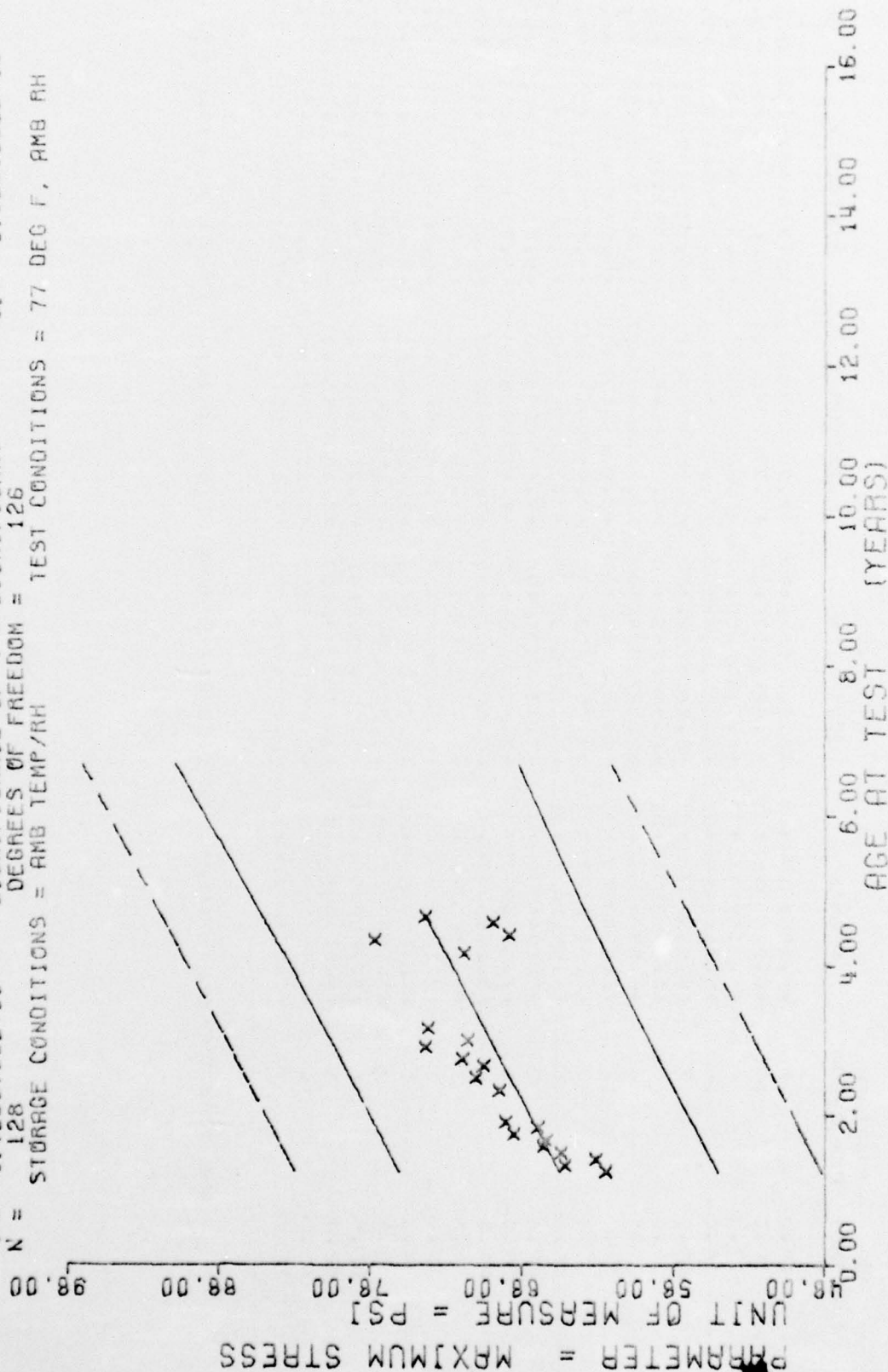
\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
53.0	12	+8.640400E+01	+5.1156223E+00	+9.367989E+01	+7.7435627E+01	+8.4112564E+01
54.0	7	+0.5541290E+01	+6.2430284E+00	+9.3259994E+01	+7.7030953E+01	+8.4517669E+01
55.0	9	+8.3382139E+01	+8.1244558E+00	+9.3259994E+01	+6.9466985E+01	+8.5327896E+01
57.0	9	+8.5069931E+01	+6.7172048E+00	+9.3500000E+01	+7.6199956E+01	+8.5733016E+01
59.0	3	+8.8853271E+01	+1.7234824E+00	+9.020991E+01	+8.6919958E+01	+8.6543243E+01
60.0	3	+7.5003325E+01	+1.0650442E+00	+7.6185987E+01	+7.4059957E+01	+8.6943348E+01
61.0	3	+7.6446655E+01	+6.3634595E+01	+7.7149993E+01	+7.5029992E+01	+8.7353469E+01
62.0	3	+8.6390378E+01	+2.1235556E+00	+8.8819992E+01	+8.4849990E+01	+8.7758575E+01
64.0	6	+7.7624930E+01	+1.4270700E+00	+7.5089996E+01	+7.6000000E+01	+8.8568801E+01

AND 3066 FREPELLANT(ANT) TENSILE MAX STRESS, .0002 IN/MIN, 77 DEG F, UNLND CINS



$Y = (1 + 6.2961507E+01) + ( +2.1447310E-01 ) \times X$   
 $F = +2.2597409E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_t = +6.3042696E+00$   
 $R = +3.8996327E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_a = +4.5117342E-02$   
 $t = +4.7536733E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_e = +5.8281539E+00$   
 $N = 128$  DEGREES OF FREEDOM = 126  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (AMB), TENSILE MAX STRESS, .0002 IN/MIN, 77 DEG F, LINED CTN

Figure 4-10



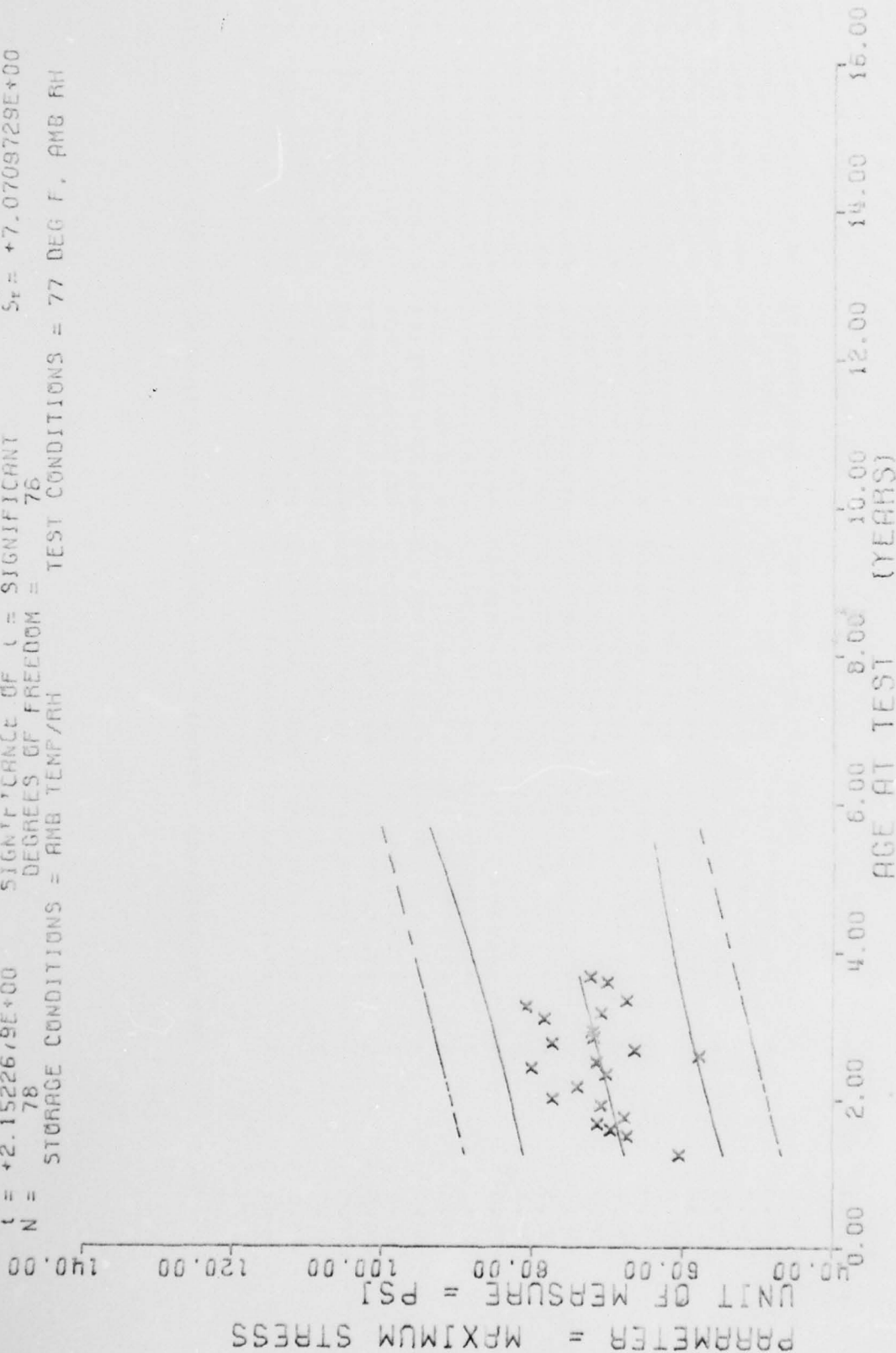
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	6	+6.2604213E+01	+6.3571556E+00	+7.0469985E+01	+5.3185587E+01	+6.5598602E+01
16.0	15	+6.5209372E+01	+8.942537E+00	+7.7725955E+01	+4.4149553E+01	+6.5813064E+01
17.0	6	+6.2150042E+01	+5.7245412E+00	+6.8105935E+01	+5.2395563E+01	+6.6027542E+01
18.0	16	+6.5460510E+01	+6.3159264E+00	+7.6255994E+01	+5.257998E+01	+6.6242019E+01
19.0	7	+6.8592773E+01	+2.8618732E+00	+7.0520998E+01	+6.1509598E+01	+6.6456481E+01
20.0	6	+6.1458251E+01	+6.0586645E+00	+7.4719985E+01	+5.553993E+01	+6.6670959E+01
21.0	6	+6.2564760E+01	+8.1871379E+00	+7.7739990E+01	+5.4709551E+01	+6.685437E+01
22.0	12	+6.6953240E+01	+2.3417458E+00	+6.9765998E+01	+6.1730950E+01	+6.709914E+01
23.0	3	+6.9102127E+01	+7.3574803E+00	+7.5665998E+01	+6.1979555E+01	+6.731437E+01
24.0	6	+6.9511427E+01	+3.233580E+00	+7.2115955E+01	+6.6459551E+01	+6.8386749E+01
30.0	6	+7.1044952E+01	+5.1315921E+00	+7.6279998E+01	+6.5325986E+01	+6.8815689E+01
32.0	6	+7.0534942E+01	+2.6507938E+00	+7.4225955E+01	+6.7699556E+01	+6.5244644E+01
33.0	6	+7.1943267E+01	+6.606662E+00	+7.9015989E+01	+6.4409538E+01	+6.5459106E+01
35.0	3	+7.4373321E+01	+3.7803253E+00	+7.8095990E+01	+7.0525358E+01	+6.5888061E+01
36.0	3	+7.1566540E+01	+4.8447194E+00	+7.7189987E+01	+6.8699556E+01	+7.0122535E+01
38.0	1	+7.4189963E+01	+6.000000E+00	+7.4195995E+01	+7.4155555E+01	+7.053147E+01
50.0	3	+7.1833312E+01	+3.2078970E+00	+7.4959991E+01	+6.8565587E+01	+7.3105148E+01
52.0	1	+7.7699996E+01	+6.000000E+00	+7.7699996E+01	+7.7699996E+01	+7.3534103E+01
53.0	3	+6.8819992E+01	+2.615337E+00	+7.1839996E+01	+6.7289593E+01	+7.374858E+01
55.0	4	+6.9927470E+01	+1.6610187E+00	+7.2299987E+01	+6.8459551E+01	+7.4177520E+01
56.0	3	+7.2319592E+01	+2.405684E+00	+7.625000E+01	+7.1619555E+01	+7.4391598E+01

ANB 30.66 PROPELLANT(ANB); TENSILE MAX STRESS, .0002 IN./MIN, 77 DEG F, LINED C/N

$F = +4.6322572E+00$   
 $R = +2.3968559E-01$   
 $t = +2.1522679E+00$   
 $N = 78$   
 STORAGE CONDITIONS = AMB TEMP/RH  
 TEST CONDITIONS = 77 DEG F, AMB RH  
 $Y = ((+6.4735807E+01) + (+2.0870193E-01) * X)$   
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF S = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM = 76  
 $S_t = +7.2358278E+00$   
 $S_e = +9.6968380E-02$   
 $S_f = +7.0709729E+00$



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME CELLS \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+6.046658E+01	+2.6502907E+00	+6.2610655E+01	+5.5220955E+01	+6.7806333E+01
18.0	4	+6.7306405E+01	+2.3622025E+00	+7.0139900E+01	+6.2659931E+01	+6.8432431E+01
19.0	3	+6.5566650E+01	+1.3812032E+00	+7.0719095E+01	+6.8130990E+01	+6.8701141E+01
20.0	3	+7.1366653E+01	+1.8506830E+00	+7.3719902E+01	+7.0209953E+01	+6.8909835E+01
21.0	5	+6.7855502E+01	+6.5774821E+00	+7.4929552E+01	+5.5739991E+01	+6.5118545E+01
22.0	3	+7.0853327E+01	+7.6119503E+01	+7.1855998E+01	+7.0139999E+01	+6.5535949E+01
24.0	3	+7.7259943E+01	+1.2396162E+00	+7.8359995E+01	+7.5059958E+01	+6.5744644E+01
26.0	3	+7.4073325E+01	+1.5071576E+00	+7.5299997E+01	+7.1839956E+01	+7.0162048E+01
28.0	3	+7.7126647E+01	+1.5080501E+00	+7.1639973E+01	+6.8670952E+01	+7.0579452E+01
29.0	3	+9.0103317E+01	+1.8411265E+00	+8.2215995E+01	+7.8862955E+01	+7.0788162E+01
30.0	6	+7.1495602E+01	+9.163989E+00	+8.3819992E+01	+6.2239990E+01	+7.0958565E+01
31.0	3	+5.7723322E+01	+2.0791314E+01	+7.0449996E+01	+3.3739990E+01	+7.1205566E+01
32.0	3	+6.6363327E+01	+1.7331658E+00	+6.8289903E+01	+6.4929952E+01	+7.1414260E+01
33.0	3	+7.7373321E+01	+1.712952E+00	+7.8759994E+01	+7.5869956E+01	+7.1522570E+01
34.0	3	+7.1786651E+01	+9.4652111E+01	+7.2559997E+01	+7.0559982E+01	+7.1831665E+01
35.0	3	+7.1966659E+01	+1.3129942E+00	+7.3059997E+01	+7.0505956E+01	+7.2040374E+01
37.0	3	+7.5466644E+01	+5.1546235E+01	+7.8565985E+01	+7.7519090E+01	+7.2457763E+01
38.0	5	+7.0829910E+01	+7.737572E+00	+7.9075986E+01	+6.3539993E+01	+7.2866473E+01
39.0	3	+8.0859985E+01	+2.7236949E+01	+8.1259994E+01	+9.0519989E+01	+7.2875167E+01
40.0	3	+6.7583315E+01	+1.7536146E+00	+6.8009985E+01	+5.5419955E+01	+7.3083877E+01
42.0	3	+6.5993310E+01	+5.5336810E+01	+7.0549957E+01	+6.9419958E+01	+7.3709576E+01
44.0	3	+7.2226654E+01	+9.4874195E+01	+7.2679905E+01	+7.1155988E+01	+7.3818685E+01

ANB-3065 PROPELLANT(ANT), TENSILE MAX STRESS, \*0002 IN/MIN, 77 DEG F, LINED CTN

$F = +6.6566261E+01$   
 $R = +1.6215577E-01$   
 $t = +8.1588145E+00$   
 $N = 2467$   
 $Y = [(+7.6679785E+01) + (+5.4120781E-02) * X]$   
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM = 2465  
 STORAGE CONDITIONS = AMB TEMP/RH  
 TEST CONDITIONS = 77 DEG F, AMB RH

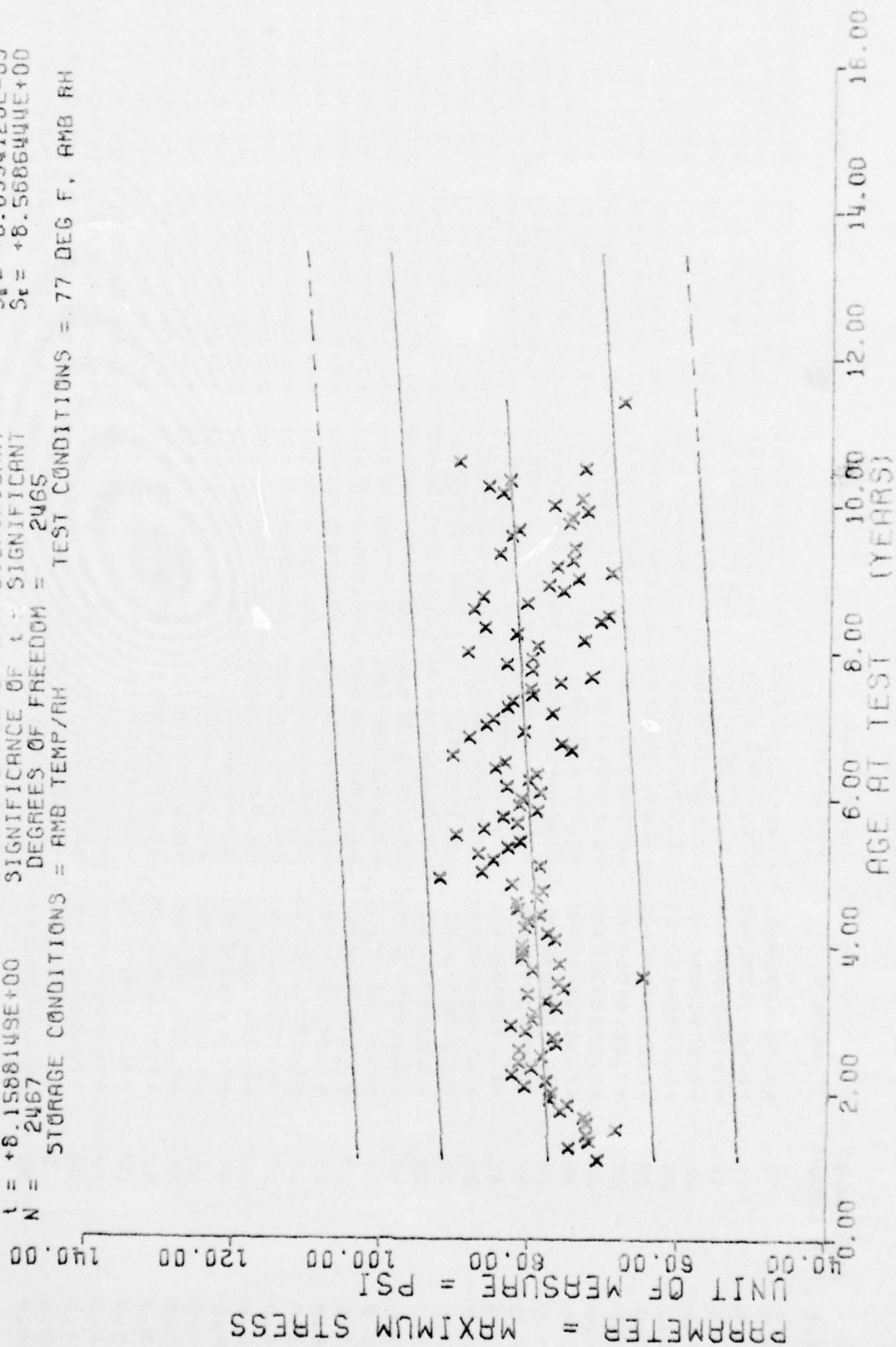


Figure 4-12



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	7	+7.0747070E+01	+4.1623044E+00	+7.7299987E+01	+6.6439987E+01	+7.7383346E+01
15.0	21	+7.4625137E+01	+1.0756648E+01	+9.0399993E+01	+5.3189987E+01	+7.7491592E+01
16.0	45	+7.1886566E+01	+9.6561599E+00	+8.5899993E+01	+4.4141499E+01	+7.7545715E+01
17.0	21	+7.2296554E+01	+9.8754172E+00	+8.8299987E+01	+5.2399993E+01	+7.7599838E+01
18.0	26	+6.8392013E+01	+7.2290808E+00	+8.6399993E+01	+5.2579986E+01	+7.7653945E+01
19.0	18	+7.2339889E+01	+5.4844288E+00	+7.9500000E+01	+6.1909988E+01	+7.7708068E+01
20.0	27	+7.2616195E+01	+6.8553858E+00	+8.5349990E+01	+5.9539993E+01	+7.7762191E+01
21.0	37	+7.5863937E+01	+5.8849156E+00	+8.4519589E+01	+5.4709991E+01	+7.7816314E+01
22.0	35	+7.4922744E+01	+7.5276271E+00	+9.0799987E+01	+6.1739990E+01	+7.7870437E+01
23.0	19	+7.7235687E+01	+1.0122201E+01	+9.1099990E+01	+6.1979995E+01	+7.7924560E+01
24.0	15	+7.7172607E+01	+7.1584867E+00	+8.7699991E+01	+6.6000000E+01	+7.7978683E+01
25.0	33	+8.0718688E+01	+5.8762098E+00	+9.1000000E+01	+5.8919995E+01	+7.8032791E+01
26.0	27	+7.7725845E+01	+7.0736028E+00	+9.0389999E+01	+6.7829986E+01	+7.8086914E+01
27.0	22	+8.2398529E+01	+6.2963343E+00	+9.5399993E+01	+7.4599990E+01	+7.8141036E+01
28.0	36	+7.9728805E+01	+1.0523251E+01	+1.0629998E+02	+4.4699995E+01	+7.8155159E+01
29.0	12	+8.1460743E+01	+5.807124E+00	+8.9000000E+01	+6.7899993E+01	+7.8249282E+01
30.0	16	+7.8499923E+01	+7.1452392E+00	+8.7799987E+01	+6.5329986E+01	+7.8303405E+01
31.0	13	+8.1445266E+01	+4.5739158E+00	+9.0399993E+01	+7.6259994E+01	+7.8357528E+01
32.0	27	+7.6461380E+01	+5.3232861E+00	+8.6799987E+01	+6.7699995E+01	+7.8411636E+01
33.0	39	+7.6874008E+01	+9.6566160E+00	+9.3500000E+01	+5.8799987E+01	+7.8465799E+01
34.0	17	+8.0559341E+01	+6.3267201E+00	+9.0899993E+01	+7.1500000E+01	+7.8519882E+01
35.0	23	+8.2602508E+01	+4.9132385E+00	+9.1500000E+01	+7.0529998E+01	+7.8574005E+01
36.0	47	+7.9691833E+01	+6.5771665E+00	+9.6799987E+01	+6.6329986E+01	+7.8628128E+01
37.0	26	+7.9354522E+01	+6.9715818E+00	+8.9199996E+01	+6.6299987E+01	+7.8682250E+01
38.0	34	+7.6499908E+01	+6.4154128E+00	+8.7399993E+01	+6.4000000E+01	+7.8736375E+01
39.0	12	+7.7916625E+01	+1.0132610E+01	+9.5000000E+01	+6.7000000E+01	+7.8790481E+01
40.0	27	+8.0336944E+01	+6.5774463E+00	+9.2000000E+01	+7.1000000E+01	+7.8844604E+01
41.0	22	+7.5490829E+01	+6.0693360E+00	+8.5799997E+01	+6.6500000E+01	+7.8898727E+01
42.0	20	+7.6303405E+01	+5.6731970E+00	+8.8549987E+01	+6.8000000E+01	+7.8952850E+01
43.0	9	+6.4928817E+01	+1.4048470E+01	+9.2239990E+01	+5.0599990E+01	+7.9006973E+01
44.0	25	+7.9696304E+01	+6.4566581E+00	+8.9389999E+01	+6.1500000E+01	+7.9061030E+01

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
45.0	20	+7.6027404E+01	+5.7585151E+00	+6.3799987E+01	+6.5759994E+01	+7.9115219E+01
46.0	44	+8.1155593E+01	+5.6697673E+00	+9.3399993E+01	+7.0199996E+01	+7.9169326E+01
47.0	12	+8.1101577E+01	+6.8396346E+00	+9.3259994E+01	+7.3199996E+01	+7.9223449E+01
48.0	20	+8.1214904E+01	+6.1387259E+00	+9.5419998E+01	+7.3299987E+01	+7.9277572E+01
49.0	22	+7.6723999E+01	+9.0693504E+00	+9.7269989E+01	+6.3199996E+01	+7.9331695E+01
50.0	32	+7.7710525E+01	+7.6208536E+00	+9.2399993E+01	+6.2899993E+01	+7.9385818E+01
51.0	57	+8.0777130E+01	+7.0749497E+00	+9.6039993E+01	+6.5019989E+01	+7.9439941E+01
52.0	51	+8.0451431E+01	+5.0644985E+00	+9.5799987E+01	+6.5799987E+01	+7.9494064E+01
53.0	40	+7.8740386E+01	+6.9134652E+00	+9.5039993E+01	+6.7289993E+01	+7.9549171E+01
54.0	19	+8.1768310E+01	+7.6525664E+00	+9.1799987E+01	+5.8799987E+01	+7.9602294E+01
55.0	46	+8.1894699E+01	+6.7115737E+00	+9.7699996E+01	+6.8459991E+01	+7.9656417E+01
56.0	62	+7.9179992E+01	+4.6405623E+00	+9.1399993E+01	+6.6669998E+01	+7.9710540E+01
57.0	46	+7.8460556E+01	+6.5721580E+00	+8.9699996E+01	+6.9399993E+01	+7.9764663E+01
58.0	34	+8.2624023E+01	+6.8119551E+00	+9.5000000E+01	+7.0909988E+01	+7.9818786E+01
59.0	20	+9.2346420E+01	+6.7405369E+00	+1.0300000E+02	+7.6729955E+01	+7.9872909E+01
60.0	20	+8.6679870E+01	+7.3299614E+00	+9.3299987E+01	+6.0899993E+01	+7.9927032E+01
61.0	40	+7.6849624E+01	+8.6878910E+00	+9.4000000E+01	+6.1199996E+01	+7.9981140E+01
62.0	35	+8.5151611E+01	+7.8220164E+00	+9.5599990E+01	+6.4899993E+01	+8.0035263E+01
63.0	45	+8.7134567E+01	+7.9507533E+00	+9.8599990E+01	+6.5599990E+01	+8.0089385E+01
64.0	36	+8.3136581E+01	+9.4803437E+00	+1.0050000E+02	+6.1500000E+01	+8.0143508E+01
65.0	28	+8.1550979E+01	+6.7543374E+00	+9.0109985E+01	+6.6500000E+01	+8.0197631E+01
66.0	28	+9.0218826E+01	+9.5156443E+00	+1.0559999E+02	+7.5799987E+01	+8.0261754E+01
67.0	46	+8.6434692E+01	+6.8096820E+00	+9.7500000E+01	+7.4299987E+01	+8.0305877E+01
68.0	44	+8.1919204E+01	+6.6299910E+00	+1.0029998E+02	+6.1399993E+01	+8.0359985E+01
69.0	32	+8.3825225E+01	+6.8235374E+00	+1.0319999E+02	+7.0599990E+01	+8.0414108E+01
70.0	40	+7.9231643E+01	+8.1702557E+00	+9.3599990E+01	+6.6099990E+01	+8.0468231E+01
71.0	47	+8.1680114E+01	+1.1568504E+01	+1.0539999E+02	+5.7599990E+01	+8.0522354E+01
72.0	34	+8.1316360E+01	+6.4662739E+00	+9.4279998E+01	+7.0399993E+01	+8.0576477E+01
73.0	27	+7.8836578E+01	+1.1196590E+01	+9.6500000E+01	+5.9799987E+01	+8.0630599E+01
74.0	15	+8.3332066E+01	+9.1079563E+00	+9.9799987E+01	+7.2000000E+01	+8.0684722E+01
75.0	30	+8.0409927E+01	+8.5612448E+00	+1.0250000E+02	+6.7899993E+01	+8.0733330E+01

ANB 3066 PROPELLANT (ALL AND) TENS MAXIMUM STRESS, +0002 IN./MIN, 77 DEG F

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
76.0	17	+7.9348144E+01	+8.2102625E+00	+9.0479995E+01	+6.5899993E+01	+8.0792953E+01
77.0	19	+8.4942520E+01	+6.5832009E+00	+9.6299987E+01	+6.9459991E+01	+8.0847076E+01
78.0	25	+8.3640701E+01	+5.0011610E+00	+9.1449996E+01	+7.4599990E+01	+8.0901199E+01
79.0	17	+9.0724609E+01	+1.1623707E+01	+1.0729998E+02	+7.5119995E+01	+8.0955322E+01
80.0	33	+7.4674728E+01	+6.5664380E+00	+8.9399993E+01	+6.1099990E+01	+8.1009045E+01
81.0	26	+7.5976806E+01	+7.6763172E+00	+8.7099990E+01	+5.5299987E+01	+8.1063568E+01
82.0	15	+8.8485244E+01	+6.1514958E+00	+9.8599990E+01	+7.8699995E+01	+8.1117675E+01
83.0	33	+8.1082916E+01	+7.2365410E+00	+9.4659988E+01	+6.4500000E+01	+8.1171798E+01
84.0	42	+8.6194885E+01	+8.1795939E+00	+1.0600000E+02	+6.7239990E+01	+8.1225921E+01
85.0	15	+8.5252532E+01	+9.2033330E+00	+9.4759994E+01	+6.4239990E+01	+8.1280044E+01
86.0	22	+7.7230361E+01	+9.7167447E+00	+9.4719985E+01	+5.3000000E+01	+8.1334167E+01
87.0	23	+8.3348648E+01	+6.3046897E+00	+9.7539993E+01	+7.3199996E+01	+8.1388290E+01
88.0	32	+8.2632720E+01	+7.6341121E+00	+9.7519989E+01	+6.6829986E+01	+8.1442413E+01
89.0	31	+8.008911E+01	+7.6228379E+00	+9.5329986E+01	+6.2079986E+01	+8.1496520E+01
90.0	11	+8.0208084E+01	+1.1467175E+01	+9.4000000E+01	+6.5369995E+01	+8.1550643E+01
91.0	9	+7.6204360E+01	+5.6337466E+00	+8.6209991E+01	+7.0219985E+01	+8.1604766E+01
92.0	17	+7.1992843E+01	+5.0883257E+00	+8.0799987E+01	+6.2699996E+01	+8.1658889E+01
93.0	15	+8.0060577E+01	+9.1607346E+00	+9.3049987E+01	+6.8199995E+01	+8.1713012E+01
94.0	13	+8.357141E+01	+7.6648805E+00	+9.2899993E+01	+6.9799987E+01	+8.1767135E+01
95.0	24	+8.0096130E+01	+6.8216720E+00	+9.3129989E+01	+6.6299987E+01	+8.1821258E+01
96.0	11	+8.8782638E+01	+3.7830879E+00	+9.6500000E+01	+8.5429992E+01	+8.1875366E+01
97.0	6	+7.9348297E+01	+5.9631456E+00	+8.6129989E+01	+7.1250000E+01	+8.1929489E+01
98.0	9	+7.3146606E+01	+2.0215930E+00	+7.6039993E+01	+6.9199996E+01	+8.1983612E+01
99.0	5	+8.2201950E+01	+8.1736401E+00	+9.3000000E+01	+7.2500000E+01	+8.2037734E+01
100.0	2	+8.6500000E+01	+1.2020815E+01	+9.5000000E+01	+7.8000000E+01	+8.2091857E+01
101.0	11	+7.0931716E+01	+9.7539530E+00	+9.3909988E+01	+5.9539993E+01	+8.2145980E+01
102.0	3	+6.5896652E+01	+2.1884838E+00	+7.2159986E+01	+6.7789993E+01	+8.2200103E+01
103.0	2	+8.0000000E+01	+2.8284271E+00	+9.6000000E+01	+8.6000000E+01	+8.2254211E+01
104.0	7	+8.0849914E+01	+6.5404646E+00	+8.9939987E+01	+7.2999993E+01	+8.2308334E+01
105.0	9	+8.6852157E+01	+6.4330381E+00	+9.7579986E+01	+7.8539993E+01	+8.2362457E+01
106.0	11	+7.6024444E+01	+9.9640234E+00	+9.4000000E+01	+6.2679992E+01	+8.2416580E+01



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

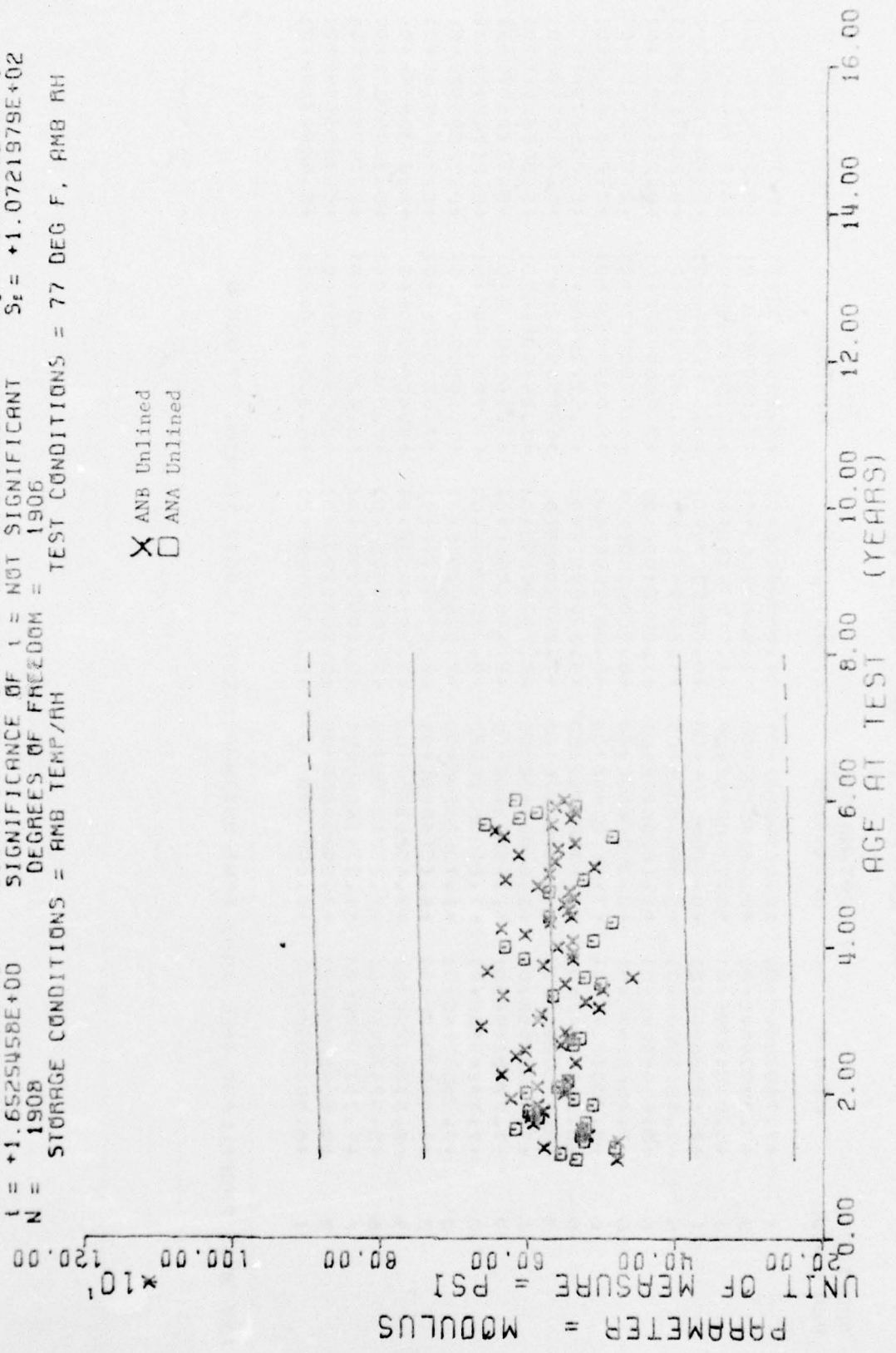
AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
107.0	2	+7.7999984E+01	+8.4689085E-01	+7.8599990E+01	+7.7399993E+01	+8.2470703E+01
108.0	3	+7.3999984E+01	+2.0884523E+00	+7.5969985E+01	+7.1809997E+01	+8.2524826E+01
109.0	14	+6.9454879E+01	+6.0300546E+00	+7.9459991E+01	+6.1989990E+01	+8.2578948E+01
110.0	11	+7.6852645E+01	+8.0280570E+00	+9.2299987E+01	+6.5479995E+01	+8.2633056E+01
111.0	5	+7.4815963E+01	+6.3561829E+00	+8.3419998E+01	+6.7479995E+01	+8.2687179E+01
112.0	6	+8.4594924E+01	+1.1615481E+01	+1.0252999E+02	+7.2969985E+01	+8.2741302E+01
113.0	18	+7.4566543E+01	+8.3504482E+00	+8.3000000E+01	+4.8799987E+01	+8.2795425E+01
115.0	6	+8.3001617E+01	+3.4692844E+00	+8.9639999E+01	+8.0399993E+01	+8.2903671E+01
116.0	6	+8.2041534E+01	+6.1798626E+00	+9.2209991E+01	+7.5779998E+01	+8.2957794E+01
117.0	3	+7.5339996E+01	+4.9571951E+00	+7.8279998E+01	+6.9569992E+01	+8.3011917E+01
118.0	4	+7.4887451E+01	+1.6706445E+00	+7.7379989E+01	+7.3919998E+01	+8.3066024E+01
119.0	9	+7.2792144E+01	+1.1557399E+00	+7.4459991E+01	+7.1059997E+01	+8.3120147E+01
120.0	2	+7.7324996E+01	+7.6103512E-02	+7.7389999E+01	+7.7259994E+01	+8.3174270E+01
121.0	3	+7.3553314E+01	+1.7352654E+00	+7.5389999E+01	+7.1939987E+01	+8.3228393E+01
122.0	3	+8.4193313E+01	+6.6214665E+00	+8.8709991E+01	+7.6579986E+01	+8.3282516E+01
123.0	9	+8.6126571E+01	+7.4528330E+00	+9.4019989E+01	+7.4099990E+01	+8.3336639E+01
124.0	6	+8.3243240E+01	+7.2501275E+00	+9.1979995E+01	+7.3059997E+01	+8.3390762E+01
126.0	6	+7.3171585E+01	+1.2381426E+01	+9.1099990E+01	+5.9250000E+01	+8.3498992E+01
127.0	3	+9.0096588E+01	+3.3526286E+00	+9.3639993E+01	+8.6389999E+01	+8.3553115E+01
137.0	1	+6.8000000E+01	+0.0000000E+27	+6.8000000E+01	+6.8000000E+01	+8.4094329E+01

ANB 3066 PROPELLANT (ALL ANB) TENS MAXIMUM STRESS. .0002 IN/MIN, 77 DEG F



$T = ((+5.5688449E+02) + (+2.3061761E-01) * X)$   
 SIGNIFICANCE OF F = NOT SIGNIFICANT  
 $G_1 = +1.0726844E+02$   
 SIGNIFICANCE OF R = NOT SIGNIFICANT  
 $S_2 = +1.3955293E-01$   
 SIGNIFICANCE OF I = NOT SIGNIFICANT  
 $S_3 = +1.0721979E+02$   
 DEGREES OF FREEDOM = 1906  
 STORAGE CONDITIONS = AMB TEMP/AM TEST CONDITIONS = 77 DEG F, AMB RH

X ANB Unlined  
 □ ANA Unlined



ANB 3056 PROPELLANT TENSILE MODULUS CHS .0002, 77 DEG F, ANA UNLND VS ANB UNLND

Figure 4-13

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	12	+5.0125000E+02	+4.4393130E+01	+5.8200000E+02	+4.3200000E+02	+5.5988232E+02
14.0	16	+5.5587500E+02	+3.4711909E+01	+5.9600000E+02	+4.6200000E+02	+5.6011303E+02
15.0	29	+5.3151708E+02	+7.1975005E+01	+6.7300000E+02	+4.1200000E+02	+5.6024375E+02
16.0	35	+4.8408569E+02	+6.3731685E+01	+6.2900000E+02	+3.4400000E+02	+5.6057421E+02
17.0	25	+5.2303979E+02	+6.9719366E+01	+7.1300000E+02	+4.0900000E+02	+5.6080493E+02
18.0	27	+5.7833325E+02	+8.5133631E+01	+7.1900000E+02	+4.2000000E+02	+5.6103540E+02
19.0	24	+5.5470825E+02	+8.3641823E+01	+6.7300000E+02	+3.8300000E+02	+5.6126611E+02
20.0	33	+5.9372705E+02	+7.6981439E+01	+8.1400000E+02	+4.4800000E+02	+5.6149682E+02
21.0	46	+5.8621728E+02	+7.9019804E+01	+7.8500000E+02	+4.4000000E+02	+5.6172729E+02
22.0	37	+5.5910791E+02	+8.9983573E+01	+7.6800000E+02	+3.7700000E+02	+5.6195800E+02
23.0	20	+5.8104980E+02	+8.3289902E+01	+7.0700000E+02	+4.5300000E+02	+5.6218847E+02
24.0	25	+5.7167993E+02	+7.1687237E+01	+7.1500000E+02	+4.6200000E+02	+5.6241918E+02
25.0	48	+5.7887500E+02	+7.3412743E+01	+7.0400000E+02	+4.3700000E+02	+5.6264990E+02
26.0	42	+5.4611889E+02	+6.4943954E+01	+6.7500000E+02	+4.1800000E+02	+5.6288037E+02
27.0	22	+6.3645434E+02	+6.6871395E+01	+7.6000000E+02	+5.2200000E+02	+5.6311108E+02
28.0	30	+5.9863330E+02	+6.4444300E+01	+6.9300000E+02	+3.8700000E+02	+5.6324155E+02
29.0	12	+5.3591650E+02	+7.6623588E+01	+6.2700000E+02	+4.0000000E+02	+5.6357226E+02
30.0	10	+6.1739990E+02	+7.4326905E+01	+7.3600000E+02	+5.1800000E+02	+5.6380297E+02
31.0	13	+6.0500000E+02	+6.8944422E+01	+7.3100000E+02	+5.1600000E+02	+5.6403344E+02
32.0	26	+5.5288452E+02	+4.9533283E+01	+6.3900000E+02	+4.5900000E+02	+5.6426416E+02
33.0	38	+5.4389453E+02	+8.2854411E+01	+7.3600000E+02	+4.0400000E+02	+5.6449487E+02
34.0	17	+5.4994116E+02	+1.0127960E+02	+6.9300000E+02	+4.0000000E+02	+5.6472534E+02
35.0	20	+6.6479980E+02	+2.0543729E+02	+1.3240000E+03	+5.1200000E+02	+5.6495605E+02
36.0	44	+5.8729541E+02	+8.1696141E+01	+7.4600000E+02	+4.1300000E+02	+5.6518652E+02
37.0	26	+5.8319213E+02	+1.0678427E+02	+7.7300000E+02	+4.2100000E+02	+5.6541723E+02
38.0	33	+5.0348461E+02	+6.7692374E+01	+6.6700000E+02	+3.9500000E+02	+5.6564794E+02
39.0	13	+5.2200000E+02	+1.5598931E+02	+8.7200000E+02	+3.8700000E+02	+5.6587841E+02
40.0	32	+6.2428125E+02	+1.9911695E+02	+1.2130000E+03	+4.6000000E+02	+5.6610913E+02
41.0	22	+4.9331811E+02	+4.6054198E+01	+5.6500000E+02	+4.0500000E+02	+5.6623959E+02
42.0	25	+5.4055981E+02	+4.9085877E+01	+6.4600000E+02	+4.5800000E+02	+5.6657031E+02
43.0	14	+4.8207128E+02	+1.1259762E+02	+7.1600000E+02	+3.3600000E+02	+5.6680102E+02

ANB 3066 PROPELLANT TENSILE MODULUS CHS .0002, 77 DEG F, ANA UNLND V5 ANB UNLND

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

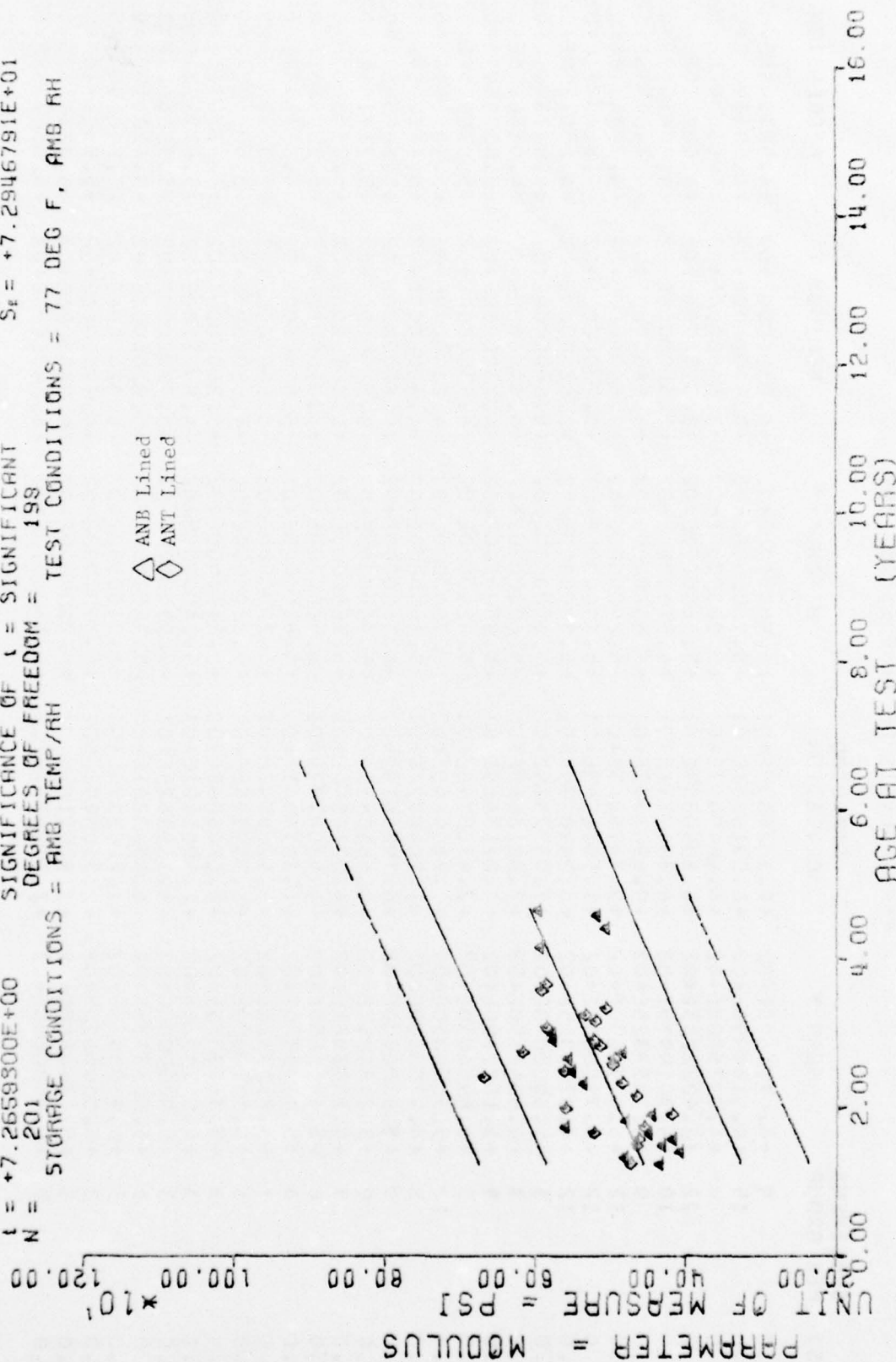
\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
44.0	25	+6.5679980E+02	+1.1186226E+02	+9.6600000E+02	+4.5800000E+02	+5.6703149E+02
45.0	20	+5.8050000E+02	+8.4686729E+01	+7.5200000E+02	+4.5500000E+02	+5.6726220E+02
46.0	49	+5.4675488E+02	+5.4226197E+01	+6.5800000E+02	+4.4900000E+02	+5.6749267E+02
47.0	12	+5.3925000E+02	+3.9055031E+01	+5.7600000E+02	+4.7700000E+02	+5.6772338E+02
48.0	23	+5.7047802E+02	+1.1380800E+02	+9.7400000E+02	+4.7900000E+02	+5.6795410E+02
49.0	29	+5.3327563E+02	+9.8313600E+01	+8.0500000E+02	+4.1700000E+02	+5.6818457E+02
50.0	29	+6.0448266E+02	+1.4666960E+02	+9.4200000E+02	+4.0000000E+02	+5.6841528E+02
51.0	57	+6.3729809E+02	+1.9012627E+02	+1.3460000E+03	+4.3100000E+02	+5.6864599E+02
52.0	58	+5.5905151E+02	+6.5922315E+01	+6.9000000E+02	+4.4900000E+02	+5.6887646E+02
53.0	48	+5.4906250E+02	+5.6993992E+01	+7.1000000E+02	+4.1500000E+02	+5.6910717E+02
54.0	19	+5.4605249E+02	+6.1264883E+01	+6.7800000E+02	+4.5300000E+02	+5.6933764E+02
55.0	44	+5.5220434E+02	+9.5665497E+01	+8.5900000E+02	+4.1300000E+02	+5.6956835E+02
56.0	59	+5.3847436E+02	+8.7368296E+01	+8.4800000E+02	+3.9500000E+02	+5.6979907E+02
57.0	49	+5.4712231E+02	+8.7329031E+01	+7.3600000E+02	+4.1600000E+02	+5.7002954E+02
58.0	35	+5.8848559E+02	+1.0062375E+02	+8.7000000E+02	+4.5300000E+02	+5.7026025E+02
59.0	25	+6.115991E+02	+8.5582163E+01	+7.6000000E+02	+5.1900000E+02	+5.7049072E+02
60.0	20	+5.7264990E+02	+4.4530622E+01	+6.4000000E+02	+4.7000000E+02	+5.7072143E+02
61.0	40	+5.1144995E+02	+1.1212674E+02	+6.7800000E+02	+1.9700000E+02	+5.7095214E+02
62.0	35	+5.6379980E+02	+9.7291194E+01	+9.4700000E+02	+4.0500000E+02	+5.7118261E+02
63.0	45	+6.1444433E+02	+1.9297969E+02	+1.5150000E+03	+4.4000000E+02	+5.7141333E+02
64.0	36	+5.6050000E+02	+9.1732063E+01	+7.8800000E+02	+3.6700000E+02	+5.7164379E+02
65.0	28	+5.3767846E+02	+7.6896781E+01	+6.7500000E+02	+3.9200000E+02	+5.7187451E+02
66.0	31	+6.1954833E+02	+1.2651556E+02	+8.9500000E+02	+4.3000000E+02	+5.7210522E+02
67.0	46	+6.4671728E+02	+1.4961196E+02	+9.4700000E+02	+4.2400000E+02	+5.7233569E+02
68.0	47	+5.7419140E+02	+1.2135998E+02	+9.6000000E+02	+3.6300000E+02	+5.7256640E+02
69.0	41	+5.5848779E+02	+6.2393958E+01	+6.9300000E+02	+4.5300000E+02	+5.7279687E+02
70.0	48	+5.4520825E+02	+8.6118166E+01	+8.0000000E+02	+4.2200000E+02	+5.7302758E+02
71.0	57	+5.5869408E+02	+1.2957935E+02	+1.0740000E+03	+3.8500000E+02	+5.7325830E+02
72.0	37	+5.5829711E+02	+7.6297977E+01	+7.6600000E+02	+4.1600000E+02	+5.7348876E+02

ANB 3066 PROPELLANT TENSILE MODULUS CHS .0002, 77 DEG F, ANA UNLND VS ANB UNLND



$Y = ((+4.0078459E+02) + (+3.6645906E+00) * X)$   
 $F = +5.2793739E+01$  SIGNIFICANCE OF  $F =$  SIGNIFICANT  $G_1 = +8.1849052E+01$   
 $R = +4.5789800E-01$  SIGNIFICANCE OF  $R =$  SIGNIFICANT  $S_2 = +5.0436636E-01$   
 $t = +7.2659300E+00$  SIGNIFICANCE OF  $t =$  SIGNIFICANT  $S_2 = +7.2946791E+01$   
 $N = 201$  DEGREES OF FREEDOM = 199  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT TENSILE MODULUS CHS 0.0002 IN/MIN, 77 DEG, AMB VS ANT LINED

Figure 4-14



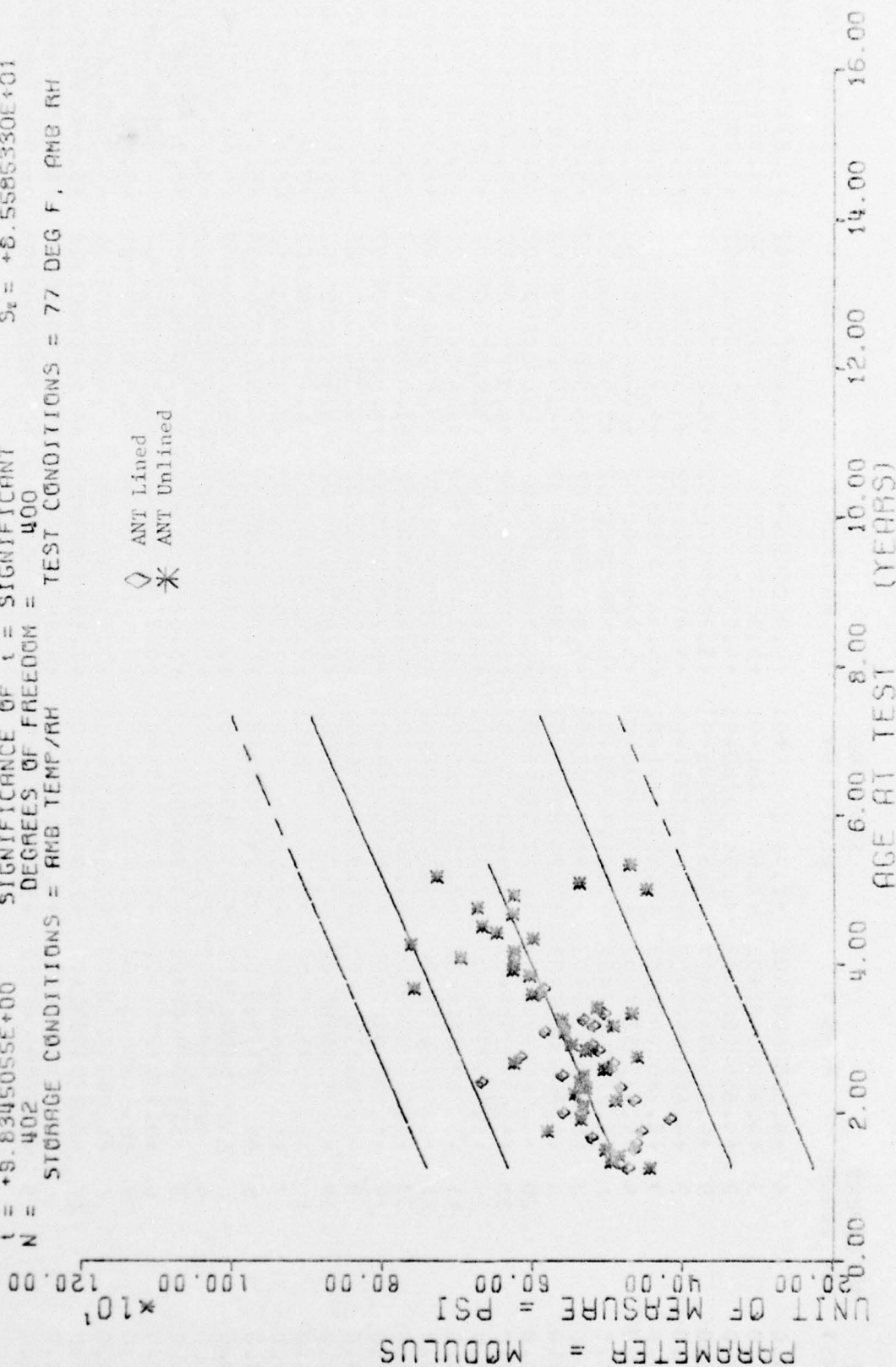
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	9	+4.4711108E+02	+2.3829836E+01	+4.9000000E+02	+4.2300000E+02	+4.5575488E+02
16.0	15	+4.8139990E+02	+6.0310861E+01	+5.7600000E+02	+3.6600000E+02	+4.5941967E+02
17.0	4	+4.0725000E+02	+6.4649697E+01	+5.0200000E+02	+3.6400000E+02	+4.6308422E+02
18.0	22	+4.4022705E+02	+6.8050353E+01	+5.5600000E+02	+3.3100000E+02	+4.6674902E+02
19.0	10	+4.3019995E+02	+4.3307171E+01	+4.8100000E+02	+3.5800000E+02	+4.7041357E+02
20.0	9	+4.7333325E+02	+9.6961332E+01	+6.5500000E+02	+3.5600000E+02	+4.7407836E+02
21.0	12	+5.0791650E+02	+9.7675865E+01	+6.2900000E+02	+3.5600000E+02	+4.7774316E+02
22.0	12	+4.7900000E+02	+7.1018563E+01	+5.7000000E+02	+3.7200000E+02	+4.8140771E+02
23.0	12	+4.3783325E+02	+5.2990279E+01	+5.2900000E+02	+3.6200000E+02	+4.8507250E+02
24.0	3	+5.6000000E+02	+7.9372539E+00	+5.6900000E+02	+5.5400000E+02	+4.8873706E+02
26.0	3	+4.6566650E+02	+2.0816659E+00	+4.6800000E+02	+4.6400000E+02	+4.9606655E+02
28.0	9	+5.1877758E+02	+4.2713515E+01	+5.8000000E+02	+4.7500000E+02	+5.0339599E+02
29.0	3	+6.6966650E+02	+2.4785748E+01	+6.9200000E+02	+6.4300000E+02	+5.0706054E+02
30.0	12	+5.5650000E+02	+1.2169148E+02	+6.7600000E+02	+4.2300000E+02	+5.1072534E+02
31.0	3	+4.9700000E+02	+1.7058722E+01	+5.1600000E+02	+4.8300000E+02	+5.1438989E+02
32.0	9	+5.3600000E+02	+4.7924419E+01	+6.1100000E+02	+4.8200000E+02	+5.1805469E+02
33.0	9	+5.2788867E+02	+9.6610615E+01	+6.2500000E+02	+3.8300000E+02	+5.2171948E+02
34.0	3	+5.1333325E+02	+4.0216083E+01	+5.5800000E+02	+4.8000000E+02	+5.2538403E+02
35.0	6	+5.4916650E+02	+4.9300777E+01	+6.4100000E+02	+5.0100000E+02	+5.2904882E+02
36.0	3	+5.7733325E+02	+1.3576941E+01	+5.9300000E+02	+5.6900000E+02	+5.3271337E+02
37.0	3	+5.8533325E+02	+3.4268547E+01	+6.2300000E+02	+5.5600000E+02	+5.3637817E+02
38.0	6	+5.1950000E+02	+6.3597955E+01	+5.8600000E+02	+4.5700000E+02	+5.4004272E+02
39.0	3	+5.3333325E+02	+8.0208062E+00	+5.4100000E+02	+4.5250000E+02	+5.4370751E+02
40.0	3	+5.0533325E+02	+2.4906491E+01	+5.3400000E+02	+4.8900000E+02	+5.4737231E+02
43.0	3	+5.9200000E+02	+1.3453624E+01	+6.0300000E+02	+5.7700000E+02	+5.5836621E+02
44.0	3	+5.8633325E+02	+6.6583281E+00	+5.9400000E+02	+5.8200000E+02	+5.6203100E+02
50.0	3	+5.9333325E+02	+1.2662279E+01	+6.0700000E+02	+5.8200000E+02	+5.8401904E+02
53.0	3	+5.0566650E+02	+2.7300793E+01	+5.3700000E+02	+4.8700000E+02	+5.9501318E+02
55.0	3	+5.1766650E+02	+1.3051181E+01	+5.2800000E+02	+5.0300000E+02	+6.0234252E+02
56.0	3	+5.9600000E+02	+2.7784887E+01	+6.1400000E+02	+5.6400000E+02	+6.0600732E+02

$F = +9.6717499E+01$   
 $R = +4.4126329E-01$   
 $t = +9.8345055E+00$   
 $N = 402$   
 $Y = ( (+4.2979267E+02) + (+3.5720344E+00) * X )$   
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM = 400  
 STORAGE CONDITIONS = AMB TEMP/RH  
 TEST CONDITIONS = 77 DEG F, AMB RH

◇ ANT Lined  
 \* ANT Unlined



ANB 3066 PROPELLANT TENSILE MODULUS CHS 0.0002 77 DEG F, ANT LINED VS UNLINED

Figure 4-15

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	4	+4.660000E+02	+1.944222E+01	+4.9000000E+02	+4.4400000E+02	+4.8327304E+02
16.0	3	+4.9600000E+02	+2.6057628E+01	+5.2600000E+02	+4.7900000E+02	+4.8694506E+02
17.0	2	+4.8550000E+02	+1.3435028E+01	+4.9500000E+02	+4.7600000E+02	+4.9051708E+02
18.0	9	+4.775541E+02	+4.3508939E+01	+5.3900000E+02	+4.2900000E+02	+4.9408911E+02
19.0	3	+4.6266650E+02	+1.6258331E+01	+4.8100000E+02	+4.5000000E+02	+4.9766113E+02
20.0	3	+5.2200000E+02	+2.4515301E+01	+5.4600000E+02	+4.9700000E+02	+5.0123315E+02
21.0	9	+4.9733325E+02	+9.6437803E+01	+5.9700000E+02	+3.5600000E+02	+5.0480517E+02
23.0	6	+4.7700000E+02	+7.0447143E+01	+5.6700000E+02	+3.9800000E+02	+5.1194946E+02
24.0	3	+5.6000000E+02	+7.9372539E+00	+5.6900000E+02	+5.5400000E+02	+5.1552148E+02
25.0	3	+5.3400000E+02	+5.2373657E+01	+5.9300000E+02	+4.9300000E+02	+5.1909350E+02
26.0	20	+4.8644995E+02	+6.7014118E+01	+6.5200000E+02	+4.0800000E+02	+5.2266552E+02
27.0	33	+5.4575756E+02	+7.9142683E+01	+6.6000000E+02	+4.0300000E+02	+5.2623754E+02
28.0	25	+5.2547998E+02	+7.2329754E+01	+6.8600000E+02	+3.9200000E+02	+5.2980957E+02
29.0	11	+5.7427270E+02	+7.7966776E+01	+6.9200000E+02	+4.4500000E+02	+5.3338159E+02
30.0	21	+5.4171411E+02	+9.8284862E+01	+6.7600000E+02	+3.8100000E+02	+5.3695361E+02
31.0	33	+5.0500000E+02	+4.9822811E+01	+6.2200000E+02	+3.8200000E+02	+5.4052563E+02
32.0	25	+6.1047998E+02	+7.5596582E+01	+8.2200000E+02	+4.8200000E+02	+5.4409765E+02
33.0	8	+5.2037500E+02	+8.3237933E+01	+6.2500000E+02	+4.3300000E+02	+5.4766967E+02
34.0	18	+5.2766650E+02	+7.2352060E+01	+6.8000000E+02	+4.4400000E+02	+5.5124169E+02
35.0	14	+5.4407128E+02	+8.3354169E+01	+7.8200000E+02	+4.4000000E+02	+5.5481372E+02
37.0	7	+5.7042846E+02	+9.5874670E+01	+7.5500000E+02	+4.7700000E+02	+5.6195776E+02
38.0	9	+5.1077758E+02	+5.2377900E+01	+5.8600000E+02	+4.5700000E+02	+5.6552978E+02
39.0	6	+5.4750000E+02	+2.5351528E+01	+5.9700000E+02	+5.2500000E+02	+5.6910180E+02
40.0	4	+4.9625000E+02	+2.7268724E+01	+5.3400000E+02	+4.6900000E+02	+5.7267382E+02
41.0	8	+5.1500000E+02	+3.2000000E+01	+5.6200000E+02	+4.7900000E+02	+5.7624584E+02
43.0	6	+5.9683325E+02	+1.7394443E+01	+6.2100000E+02	+5.7700000E+02	+5.8339013E+02
44.0	7	+6.8542846E+02	+1.3505413E+02	+9.2800000E+02	+5.8200000E+02	+5.8696215E+02
46.0	6	+6.0433325E+02	+1.3954019E+02	+7.4700000E+02	+4.4200000E+02	+5.9410620E+02
47.0	10	+6.275985E+02	+1.0916368E+02	+7.5300000E+02	+4.6500000E+02	+5.9767822E+02
48.0	6	+6.2616650E+02	+4.2976350E+01	+6.9600000E+02	+5.8100000E+02	+6.0125024E+02
49.0	5	+6.9700000E+02	+5.7480431E+01	+7.7000000E+02	+6.3900000E+02	+6.0482226E+02



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

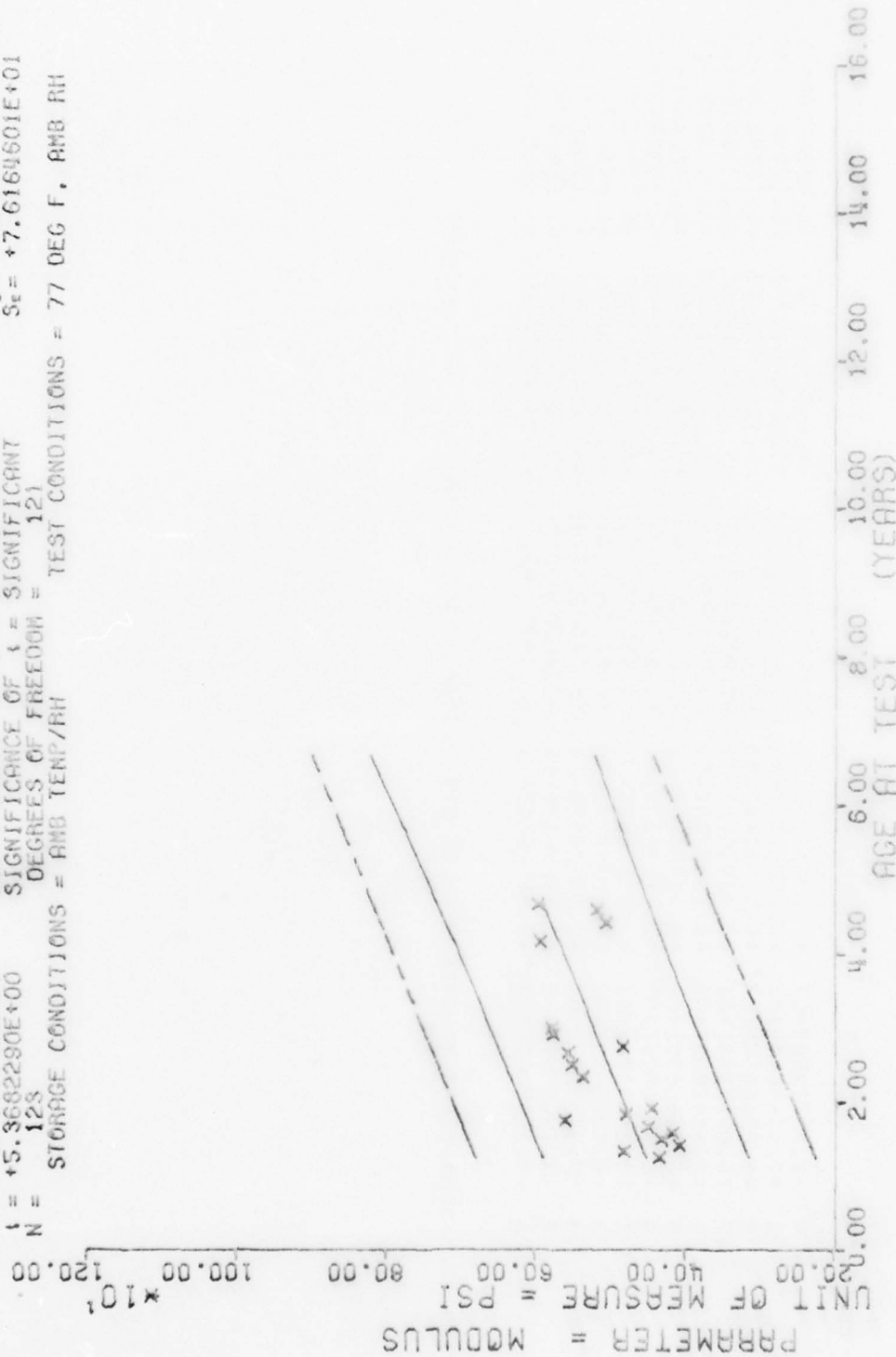
\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
50.0	9	+6.2577758E+02	+5.0751299E+01	+6.9700000E+02	+5.4300000E+02	+6.0839428E+02
51.0	3	+7.6366650E+02	+5.5075705E+00	+7.6900000E+02	+7.5800000E+02	+6.1156630E+02
52.0	3	+6.0066650E+02	+9.7125348E+00	+6.0900000E+02	+5.9000000E+02	+6.1553833E+02
53.0	17	+6.4911743E+02	+9.6211929E+01	+7.9300000E+02	+5.0900000E+02	+6.1911035E+02
54.0	7	+6.6842846E+02	+8.7089718E+01	+7.7000000E+02	+5.5200000E+02	+6.2268237E+02
56.0	9	+6.2766650E+02	+8.5290679E+01	+7.6600000E+02	+5.2700000E+02	+6.2982641E+02
57.0	9	+6.7500000E+02	+6.1777827E+01	+7.6000000E+02	+5.9500000E+02	+6.3339843E+02
59.0	3	+6.2633325E+02	+2.1962088E+01	+6.4000000E+02	+6.0100000E+02	+6.4054248E+02
60.0	3	+4.4900000E+02	+8.1853527E+00	+4.5600000E+02	+4.4000000E+02	+6.4411474E+02
61.0	3	+5.3833325E+02	+1.2342339E+01	+5.5200000E+02	+5.2800000E+02	+6.4768676E+02
62.0	3	+7.2900000E+02	+1.1269427E+01	+7.3600000E+02	+7.1600000E+02	+6.5125878E+02
64.0	6	+4.7100000E+02	+3.5899860E+01	+4.9900000E+02	+4.2400000E+02	+6.5840283E+02

ANB 3066 PROPELLANT TENSILE MODULUS CHS 0.0002 77 DEG F, ANT LINED VS UNLINED



$Y = ((+4.0179540E+02) + (+3.3576748E+00) * X)$   
 $F = +2.8617883E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G_1 = +8.4402456E+01$   
 $R = +4.3858039E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_2 = +6.2547160E-01$   
 $t = +5.3682290E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_3 = +7.6164601E+01$   
 $N = 128$  DEGREES OF FREEDOM = 121  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (AMB), TENSILE MODULUS, 0.0002 IN/IN, 77 DEG F, LINED CTNS

Figure 4-16

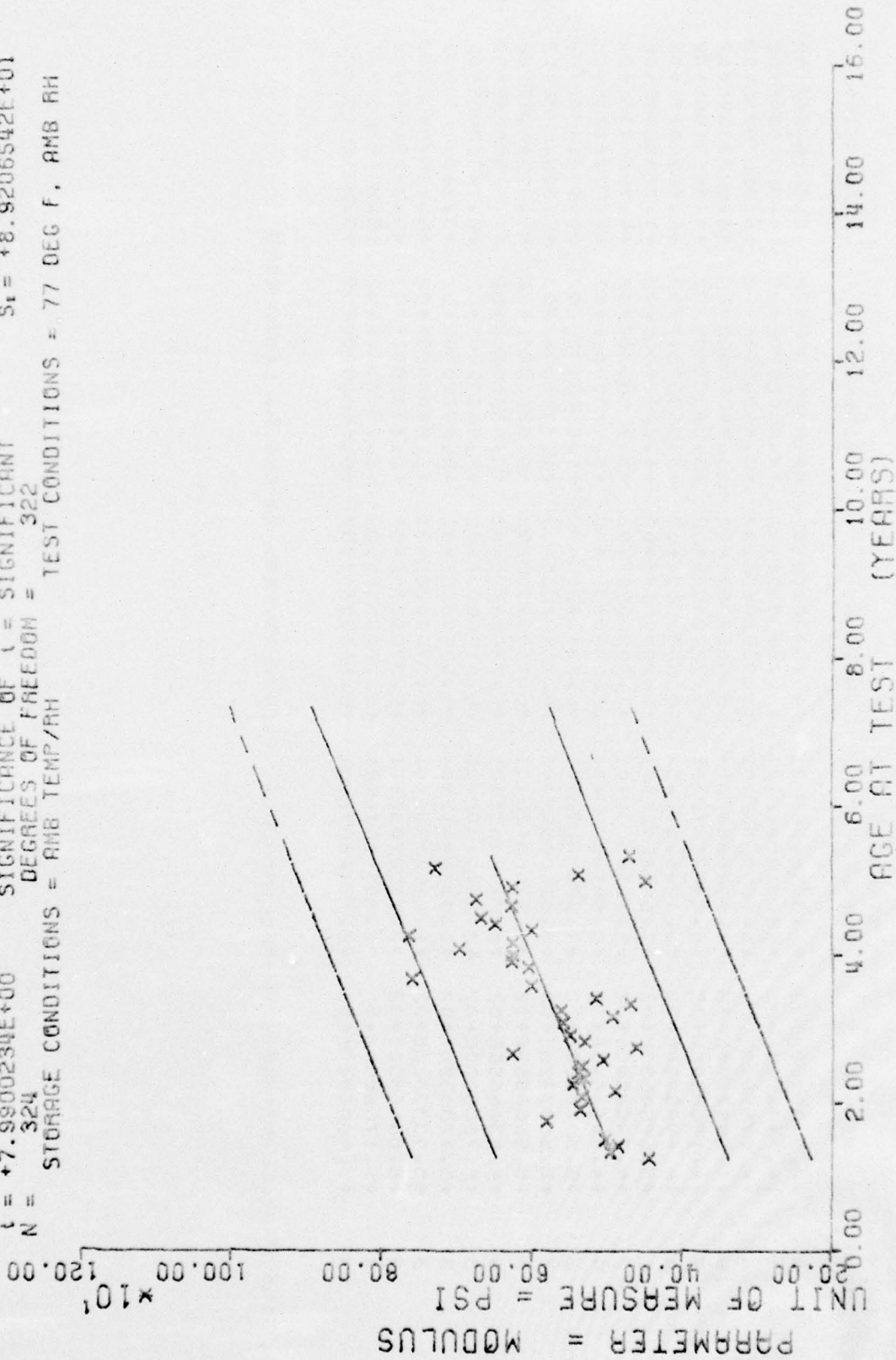
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	6	+4.3400000E+02	+1.3856406E+01	+4.59000000E+02	+4.23000000E+02	+4.5216040E+02
16.0	15	+4.8139990E+02	+6.0310861E+01	+5.76000000E+02	+3.66000000E+02	+4.5551806E+02
17.0	4	+4.8725000E+02	+6.4649637E+01	+5.02000000E+02	+3.64000000E+02	+4.5887573E+02
18.0	16	+4.3067500E+02	+7.5185880E+01	+5.56000000E+02	+3.31000000E+02	+4.6223339E+02
19.0	7	+4.1628554E+02	+4.4409887E+01	+4.72000000E+02	+3.58000000E+02	+4.6559106E+02
20.0	6	+4.4900000E+02	+1.1256287E+02	+6.55000000E+02	+3.56000000E+02	+4.6894873E+02
21.0	6	+5.6050000E+02	+7.6808202E+01	+6.29000000E+02	+4.44000000E+02	+4.7230639E+02
22.0	12	+4.7900000E+02	+7.1018563E+01	+5.70000000E+02	+3.72000000E+02	+4.7566406E+02
23.0	9	+4.4466650E+02	+5.8819639E+01	+5.29000000E+02	+3.62000000E+02	+4.7902172E+02
28.0	6	+5.3600000E+02	+4.2703629E+01	+5.90000000E+02	+4.85000000E+02	+4.9581030E+02
30.0	6	+5.5083325E+02	+1.3210059E+02	+6.75000000E+02	+4.23000000E+02	+5.0252563E+02
32.0	6	+5.5666650E+02	+4.5266617E+01	+6.11000000E+02	+5.09000000E+02	+5.0924096E+02
33.0	6	+4.8316650E+02	+8.7793887E+01	+5.73000000E+02	+3.83000000E+02	+5.1259863E+02
35.0	3	+5.7600000E+02	+5.8949130E+01	+6.41000000E+02	+5.26000000E+02	+5.1931396E+02
36.0	3	+5.7733325E+02	+1.3576941E+01	+5.93000000E+02	+5.69000000E+02	+5.2267163E+02
50.0	3	+5.9333325E+02	+1.2662279E+01	+6.07000000E+02	+5.82000000E+02	+5.6967895E+02
53.0	3	+5.0566650E+02	+2.7300793E+01	+5.37000000E+02	+4.87000000E+02	+5.7975195E+02
55.0	3	+5.1766650E+02	+1.3051181E+01	+5.28000000E+02	+5.03000000E+02	+5.8646728E+02
56.0	3	+5.9600000E+02	+2.7784887E+01	+6.14000000E+02	+5.64000000E+02	+5.8982519E+02

ANB 3066 PROPELLANT(ANB), TENSILE MODULUS, 0.0002 IN/MIN, 77 DEG F, LINED CINS

$Y = ((+4.4295959E+02) + (+3.3213803E+00) * X)$   
 $F = +6.3840474E+01$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = +4.0676554E-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +7.9900234E+00$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 324$  DEGREES OF FREEDOM = 322  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (ANT) TENSILE MODULUS, 0.0002 IN/MIN, 77 DEG F, UNLINED CTNS

Figure 4-17

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	1	44.4400000E+02	+0.0000000E+01	44.4400000E+02	44.4400000E+02	44.9278027E+02
16.0	3	44.5600000E+02	+2.6057628E+01	45.2600000E+02	44.7900000E+02	44.5610156E+02
17.0	2	44.8500000E+02	+1.3435028E+01	44.9500000E+02	44.7600000E+02	44.5942285E+02
18.0	3	45.0233325E+02	+5.0292477E+01	45.3900000E+02	44.4500000E+02	45.0274438E+02
21.0	3	45.8133325E+02	+1.3650356E+01	45.9700000E+02	45.7200000E+02	45.1270849E+02
23.0	3	45.3666650E+02	+3.1021497E+01	45.6700000E+02	45.0500000E+02	45.1935131E+02
25.0	3	45.7400000E+02	+5.2273657E+01	45.9300000E+02	44.9300000E+02	45.2599389E+02
26.0	17	44.9011743E+02	+7.2367831E+01	46.5200000E+02	44.0800000E+02	45.2931542E+02
27.0	33	45.4575750E+02	+7.5142683E+01	46.6000000E+02	44.0300000E+02	45.3263671E+02
28.0	22	45.2109082E+02	+7.5481886E+01	46.8600000E+02	43.9200000E+02	45.3595900E+02
29.0	8	45.2850000E+02	+5.6089214E+01	45.9700000E+02	44.4500000E+02	45.3927954E+02
30.0	15	45.2353320E+02	+9.0406120E+01	46.4100000E+02	43.8100000E+02	45.4260083E+02
31.0	39	45.0579980E+02	+5.2074482E+01	46.2200000E+02	43.8200000E+02	45.4592236E+02
32.0	22	46.2627270E+02	+6.5824573E+01	48.2200000E+02	45.3800000E+02	45.4924365E+02
33.0	5	44.6219995E+02	+2.5490349E+01	44.9800000E+02	44.3300000E+02	45.5256494E+02
34.0	15	45.3053320E+02	+7.7927499E+01	46.8000000E+02	44.4400000E+02	45.5598647E+02
35.0	11	45.5000000E+02	+9.3614101E+01	47.8200000E+02	44.4000000E+02	45.5920776E+02
37.0	4	45.5925000E+02	+1.2119546E+02	47.5500000E+02	44.7700000E+02	45.6585058E+02
38.0	3	44.9333325E+02	+1.2216656E+01	45.9800000E+02	44.8200000E+02	45.6917187E+02
39.0	3	45.6166650E+02	+3.0664955E+01	45.9700000E+02	45.4200000E+02	45.7249340E+02
40.0	1	44.6900000E+02	+0.0000000E+01	44.6900000E+02	44.6900000E+02	45.7581469E+02
41.0	8	45.1500000E+02	+3.2000000E+01	45.6200000E+02	44.7900000E+02	45.7913598E+02
43.0	3	46.0166650E+02	+2.2479620E+01	46.2100000E+02	45.7700000E+02	45.8577580E+02
44.0	4	47.5975000E+02	+1.3879811E+02	49.2800000E+02	46.3900000E+02	45.8910009E+02
46.0	6	46.0433325E+02	+1.3554019E+02	47.4700000E+02	44.4200000E+02	45.9574291E+02
47.0	10	46.2759985E+02	+1.0916368E+02	47.5700000E+02	44.6500000E+02	45.9906443E+02
48.0	6	44.2616650E+02	+4.2576350E+01	46.9600000E+02	45.8100000E+02	46.0238574E+02
49.0	5	46.9700000E+02	+5.7480431E+01	47.7000000E+02	46.3960000E+02	46.0576703E+02
50.0	9	46.2577758E+02	+5.0751299E+01	46.9700000E+02	45.4300000E+02	46.0902856E+02
51.0	3	47.6366650E+02	+5.5075705E+01	47.6900000E+02	47.5800000E+02	46.1234985E+02
52.0	3	46.0666650E+02	+9.7125348E+01	46.0900000E+02	45.9000000E+02	46.1567114E+02

ANB 3066 PROPELLANT(ANT) TENSILE MODULUS, 0.0002 IN./MIN., 77 DEG F, UNLINED CTNS



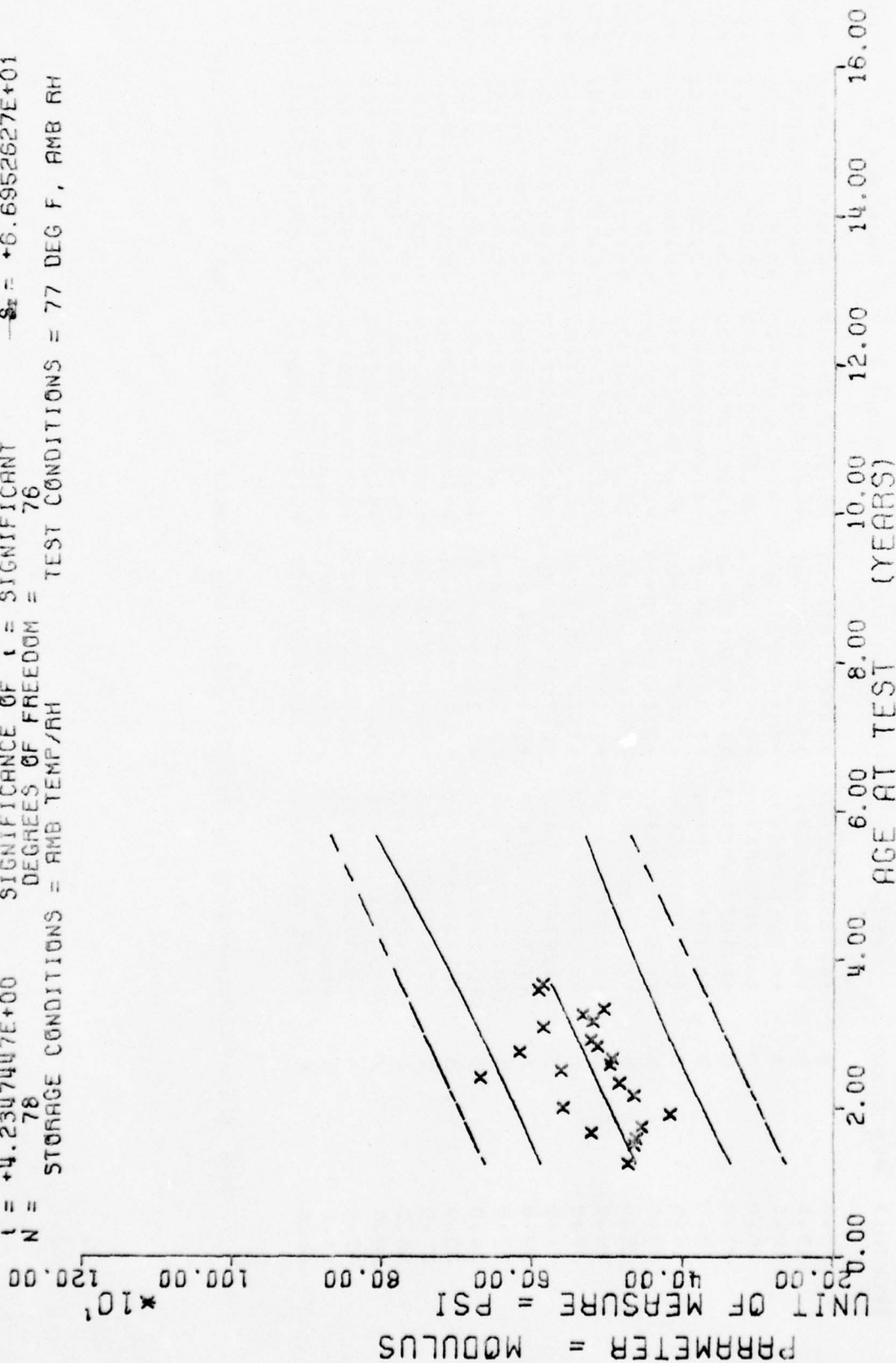
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
53.0	17	+6.4911743E+02	+9.6211920E+01	+7.9300000E+02	+5.0900000E+02	+6.1899267E+02
54.0	7	+6.6842846E+02	+8.7089718E+01	+7.7000000E+02	+5.5200000E+02	+6.2231396E+02
56.0	9	+6.2766650E+02	+8.5290679E+01	+7.6600000E+02	+5.2700000E+02	+6.2895678E+02
57.0	9	+6.7500000E+02	+6.1777827E+01	+7.8000000E+02	+5.9500000E+02	+6.3227807E+02
59.0	3	+6.2633325E+02	+2.1562088E+01	+6.4000000E+02	+6.0100000E+02	+6.3892089E+02
60.0	3	+4.4900000E+02	+8.1853527E+00	+4.5600000E+02	+4.4000000E+02	+6.4224218E+02
61.0	3	+5.3823325E+02	+1.2342339E+01	+5.5200000E+02	+5.2800000E+02	+6.4556372E+02
62.0	3	+7.2900000E+02	+1.1269427E+01	+7.3600000E+02	+7.1600000E+02	+6.4888500E+02
64.0	6	+4.7100000E+02	+3.5899860E+01	+4.9900000E+02	+4.2400000E+02	+6.5552783E+02

ANB 3066 PROPELLANT(ANT) TENSILE MODULUS, 0.0002 IN/MIN, 77 DEG F, UNLINED CTNS

$Y = [(+4.0492279E+02) + (+3.8881752E+00) * X]$   
 $F = +1.7933063E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G = +7.3948863E+01$   
 $R = +4.3693617E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +9.1816045E-01$   
 $t = +4.2347447E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $-S_e = +6.6952627E+01$   
 $N = 78$  DEGREES OF FREEDOM = 76  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (ANT), TENSILE MODULUS, 0.0002 IN/MIN, 77 DEG F, LINED CIN

Figure 4-18

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+4.7333325E+02	+1.5631165E+01	+4.9000000E+02	+4.5900000E+02	+4.6324536E+02
18.0	6	+4.6516650E+02	+3.8269657E+01	+5.0500000E+02	+4.2900000E+02	+4.7490966E+02
19.0	3	+4.6266650E+02	+1.6258331E+01	+4.8100000E+02	+4.5000000E+02	+4.7879785E+02
20.0	3	+5.2200000E+02	+2.4515301E+01	+5.4600000E+02	+4.9700000E+02	+4.8268603E+02
21.0	6	+4.5533325E+02	+9.1553611E+01	+5.6600000E+02	+3.5600000E+02	+4.8657421E+02
23.0	3	+4.1733325E+02	+2.7646579E+01	+4.4900000E+02	+3.9800000E+02	+4.9435058E+02
24.0	3	+5.6000000E+02	+7.9372539E+00	+5.6900000E+02	+5.5400000E+02	+4.9823876E+02
26.0	3	+4.6566650E+02	+2.0816659E+00	+4.6800000E+02	+4.6400000E+02	+5.0601513E+02
28.0	3	+4.8433325E+02	+8.3266639E+00	+4.9100000E+02	+4.7500000E+02	+5.1379150E+02
29.0	3	+6.6966650E+02	+2.4785748E+01	+6.9200000E+02	+6.4300000E+02	+5.1767968E+02
30.0	6	+5.6216650E+02	+1.2268564E+02	+6.7600000E+02	+4.3900000E+02	+5.2156787E+02
31.0	3	+4.9700000E+02	+1.7058722E+01	+5.1600000E+02	+4.8300000E+02	+5.2545605E+02
32.0	3	+4.9466650E+02	+1.4843629E+01	+5.1100000E+02	+4.8200000E+02	+5.2934423E+02
33.0	3	+6.1733325E+02	+8.0208062E+00	+6.2500000E+02	+6.0900000E+02	+5.3323242E+02
34.0	3	+5.1333325E+02	+4.0216083E+01	+5.5800000E+02	+4.8000000E+02	+5.3712060E+02
35.0	3	+5.2233325E+02	+2.1007935E+01	+5.4300000E+02	+5.0100000E+02	+5.4100878E+02
37.0	3	+5.8533325E+02	+3.4268547E+01	+6.2300000E+02	+5.5600000E+02	+5.4878515E+02
38.0	6	+5.1950000E+02	+6.3597955E+01	+5.8600000E+02	+4.5700000E+02	+5.5267333E+02
39.0	3	+5.3333325E+02	+8.0208062E+00	+5.4100000E+02	+5.2500000E+02	+5.5656152E+02
40.0	3	+5.0533325E+02	+2.4506491E+01	+5.3400000E+02	+4.8500000E+02	+5.6044970E+02
43.0	3	+5.9200000E+02	+1.3453624E+01	+6.0300000E+02	+5.7700000E+02	+5.7211425E+02
44.0	3	+5.8633325E+02	+6.6583281E+00	+5.9400000E+02	+5.8200000E+02	+5.7600244E+02

ANB 3066 PROPELLANT(ANT). TENSILE MODULUS, 0.0002 IN/MIN, 77 DEG F, LINED CIN

$Y = ((+5.6343885E+02) + (-6.0978842E-02) * X)$   
 $F = +4.4899411E-01$  SIGNIFICANCE OF F = NOT SIGNIFICANT  $G_1 = +1.1717830E+02$   
 $R = -1.3519661E-02$  SIGNIFICANCE OF R = NOT SIGNIFICANT  $S_1 = +9.1003659E-02$   
 $t = +6.7007022E-01$  SIGNIFICANCE OF t = NOT SIGNIFICANT  $S_2 = +1.1719144E+02$   
 $N = 2458$  DEGREES OF FREEDOM = 2456  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

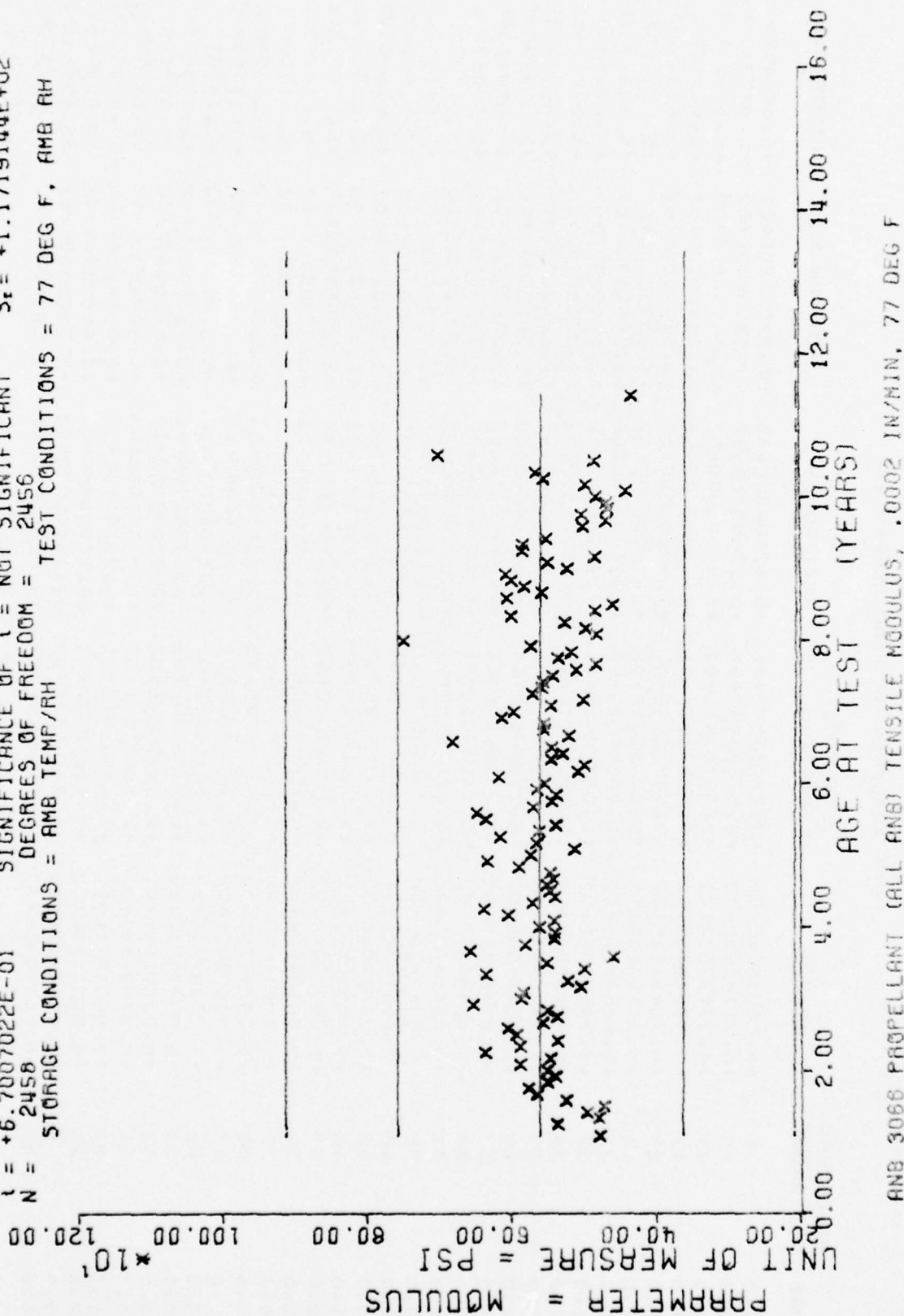


Figure 4-19



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	7	+4.7628564E+02	+3.2273385E+01	+5.1200000E+02	+4.3200000E+02	+5.6264599E+02
15.0	21	+5.3714282E+02	+8.5028398E+01	+6.7300000E+02	+4.2300000E+02	+5.6252416E+02
16.0	45	+4.7877758E+02	+6.230092E+01	+6.2900000E+02	+3.4400000E+02	+5.6246313E+02
17.0	19	+4.5557885E+02	+8.5877377E+01	+7.1300000E+02	+3.6400000E+02	+5.6240209E+02
18.0	28	+4.7246411E+02	+9.5430208E+01	+7.1900000E+02	+3.3100000E+02	+5.6234106E+02
19.0	18	+5.2455541E+02	+1.0355971E+02	+6.7300000E+02	+3.5800000E+02	+5.6228002E+02
20.0	27	+5.6459252E+02	+1.0602911E+02	+8.1400000E+02	+3.5600000E+02	+5.6221923E+02
21.0	37	+5.7627026E+02	+8.0604882E+01	+7.8500000E+02	+4.4000000E+02	+5.6215820E+02
22.0	35	+5.5048559E+02	+9.6325847E+01	+7.6800000E+02	+3.7200000E+02	+5.6209716E+02
23.0	19	+5.3915771E+02	+1.1548317E+02	+7.0700000E+02	+3.6200000E+02	+5.6203613E+02
24.0	15	+5.5046655E+02	+6.1855669E+01	+6.6000000E+02	+4.6600000E+02	+5.6197534E+02
25.0	33	+5.8778784E+02	+7.2206629E+01	+7.0400000E+02	+4.3700000E+02	+5.6191430E+02
26.0	27	+5.4644433E+02	+6.9516066E+01	+6.7500000E+02	+4.1800000E+02	+5.6185327E+02
27.0	22	+6.3645434E+02	+6.6871395E+01	+7.6000000E+02	+5.2200000E+02	+5.6179223E+02
28.0	36	+5.8819433E+02	+6.5284353E+01	+6.9300000E+02	+3.8700000E+02	+5.6173144E+02
29.0	12	+5.3591650E+02	+7.6623588E+01	+6.2700000E+02	+4.0000000E+02	+5.6167041E+02
30.0	16	+5.9243750E+02	+1.0118957E+02	+7.3600000E+02	+4.2300000E+02	+5.6160937E+02
31.0	13	+6.0500000E+02	+6.8944422E+01	+7.3100000E+02	+5.1600000E+02	+5.6154833E+02
32.0	27	+5.5637036E+02	+4.7654063E+01	+6.3900000E+02	+4.8000000E+02	+5.6148730E+02
33.0	39	+5.3638452E+02	+8.9986436E+01	+7.3600000E+02	+3.8300000E+02	+5.6142651E+02
34.0	17	+5.4994116E+02	+1.0127960E+02	+6.9300000E+02	+4.0000000E+02	+5.6136547E+02
35.0	23	+6.5321728E+02	+1.9416557E+02	+1.3240000E+03	+5.1200000E+02	+5.6130444E+02
36.0	47	+5.8665942E+02	+7.9076263E+01	+7.4600000E+02	+4.1300000E+02	+5.6124340E+02
37.0	26	+5.8319213E+02	+1.0678427E+02	+7.7300000E+02	+4.2100000E+02	+5.6118261E+02
38.0	33	+5.0348461E+02	+6.7692374E+01	+6.6700000E+02	+3.9500000E+02	+5.6112158E+02
39.0	13	+5.2200000E+02	+1.5598931E+02	+8.7200000E+02	+3.8700000E+02	+5.6106054E+02
40.0	27	+6.3492578E+02	+2.1501054E+02	+1.2130000E+03	+4.6000000E+02	+5.6099951E+02
41.0	22	+4.9831811E+02	+4.6054198E+01	+5.6500000E+02	+4.0500000E+02	+5.6093872E+02
42.0	20	+5.5050000E+02	+4.4221333E+01	+6.4600000E+02	+4.6400000E+02	+5.6087768E+02
43.0	9	+4.588867E+02	+1.3714722E+02	+7.1600000E+02	+3.3600000E+02	+5.6081665E+02
44.0	25	+6.5679980E+02	+1.186226E+02	+9.6600000E+02	+4.5800000E+02	+5.6075561E+02

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
45.0	20	+5.8050000E+02	+8.4686729E+01	+7.5200000E+02	+4.5500000E+02	+5.6069458E+02
46.0	44	+5.3988623E+02	+5.1504301E+01	+6.4300000E+02	+4.4900000E+02	+5.6063378E+02
47.0	12	+5.3925000E+02	+3.9055031E+01	+5.7600000E+02	+4.7700000E+02	+5.6057275E+02
48.0	20	+5.6109985E+02	+1.1707617E+02	+9.7400000E+02	+4.7900000E+02	+5.6051171E+02
49.0	22	+5.4022705E+02	+1.0644657E+02	+6.0500000E+02	+4.1700000E+02	+5.6045068E+02
50.0	32	+6.0343750E+02	+1.3946833E+02	+9.4200000E+02	+4.0000000E+02	+5.6038989E+02
51.0	57	+6.3729809E+02	+1.9012627E+02	+1.3460000E+03	+4.3100000E+02	+5.6032885E+02
52.0	50	+5.7073999E+02	+6.2869742E+01	+6.9000000E+02	+4.5300000E+02	+5.6026782E+02
53.0	40	+5.3917480E+02	+6.0028577E+01	+7.1000000E+02	+4.1500000E+02	+5.6020678E+02
54.0	19	+5.4605249E+02	+6.1264883E+01	+6.7800000E+02	+4.5300000E+02	+5.6014599E+02
55.0	47	+5.5000000E+02	+9.2526104E+01	+8.5900000E+02	+4.1300000E+02	+5.6008496E+02
56.0	62	+5.4125805E+02	+8.6243067E+01	+8.4800000E+02	+3.9500000E+02	+5.6002392E+02
57.0	46	+5.4539111E+02	+8.9556308E+01	+7.3600000E+02	+4.1600000E+02	+5.5996289E+02
58.0	35	+5.8848559E+02	+1.0062375E+02	+8.7000000E+02	+4.5300000E+02	+5.5990185E+02
59.0	20	+6.3239990E+02	+8.2873016E+01	+7.6000000E+02	+5.2800000E+02	+5.5984106E+02
60.0	20	+5.7264990E+02	+4.4530622E+01	+6.4000000E+02	+4.7000000E+02	+5.5978002E+02
61.0	40	+5.1144995E+02	+1.1212674E+02	+6.7800000E+02	+1.9700000E+02	+5.5971899E+02
62.0	35	+5.6379980E+02	+9.7291194E+01	+9.4700000E+02	+4.0500000E+02	+5.5965795E+02
63.0	45	+6.1444433E+02	+1.5297969E+02	+1.5150000E+03	+4.4000000E+02	+5.5959716E+02
64.0	36	+5.6050000E+02	+9.1732063E+01	+7.8800000E+02	+3.6700000E+02	+5.5953613E+02
65.0	28	+5.3767846E+02	+7.6896781E+01	+6.7500000E+02	+3.9200000E+02	+5.5947509E+02
66.0	28	+6.3385693E+02	+1.2416169E+02	+8.9500000E+02	+4.5300000E+02	+5.5941406E+02
67.0	46	+6.4671728E+02	+1.4561196E+02	+9.4700000E+02	+4.2400000E+02	+5.5935327E+02
68.0	44	+5.6829541E+02	+1.2326065E+02	+9.6000000E+02	+3.6300000E+02	+5.5929223E+02
69.0	32	+5.4312500E+02	+5.3109594E+01	+6.7100000E+02	+4.5300000E+02	+5.5923120E+02
70.0	40	+5.3644995E+02	+8.4065587E+01	+8.0000000E+02	+4.2200000E+02	+5.5917016E+02
71.0	47	+5.6348925E+02	+1.3605032E+02	+1.0740000E+03	+3.8500000E+02	+5.5910913E+02
72.0	34	+5.5288232E+02	+7.7209203E+01	+7.6600000E+02	+4.1600000E+02	+5.5904833E+02
73.0	24	+6.1633325E+02	+1.1446384E+02	+9.7300000E+02	+4.8700000E+02	+5.5898730E+02
74.0	15	+5.0626660E+02	+9.7847889E+01	+6.7900000E+02	+3.7500000E+02	+5.5892626E+02
75.0	30	+4.9683325E+02	+8.8224276E+01	+7.2000000E+02	+3.7300000E+02	+5.5886523E+02

ANB 3066 PROPELLANT (ALL ANB) TENSILE MODULUS, \*0002 18/MIN, 77 DEG F

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
76.0	17	+5.4347045E+02	+7.1110932E+01	+6.9200000E+02	+4.5300000E+02	+5.5880444E+02
77.0	19	+5.2726293E+02	+8.0067917E+01	+6.4000000E+02	+4.1300000E+02	+5.5874340E+02
78.0	24	+5.4291650E+02	+7.3757485E+01	+6.5700000E+02	+4.3500000E+02	+5.5868237E+02
79.0	17	+6.8005859E+02	+1.3534099E+02	+9.3300000E+02	+4.0900000E+02	+5.5862133E+02
80.0	33	+5.1906054E+02	+8.8404588E+01	+7.6100000E+02	+3.8200000E+02	+5.5856054E+02
81.0	26	+5.5326904E+02	+9.0564853E+01	+8.2900000E+02	+4.3200000E+02	+5.5849951E+02
82.0	15	+5.5346655E+02	+6.8312168E+01	+6.8000000E+02	+4.6600000E+02	+5.5843847E+02
83.0	33	+6.1181811E+02	+2.5071017E+02	+1.4150000E+03	+4.1600000E+02	+5.5837744E+02
84.0	42	+5.9507128E+02	+1.5119130E+02	+1.4100000E+03	+4.3700000E+02	+5.5831640E+02
85.0	15	+5.4393310E+02	+7.9652339E+01	+6.4000000E+02	+4.2000000E+02	+5.582561E+02
86.0	22	+4.9886352E+02	+6.9374961E+01	+5.9500000E+02	+3.7800000E+02	+5.5819458E+02
87.0	23	+5.6952172E+02	+1.3228889E+02	+9.5200000E+02	+3.4400000E+02	+5.5813354E+02
88.0	32	+5.5665625E+02	+1.1172189E+02	+8.7100000E+02	+3.0200000E+02	+5.5807250E+02
89.0	30	+5.5523315E+02	+8.7574867E+01	+8.0000000E+02	+4.2200000E+02	+5.5801171E+02
90.0	11	+5.4127270E+02	+8.4657062E+01	+6.6200000E+02	+4.3500000E+02	+5.5795068E+02
91.0	9	+5.0911108E+02	+4.4798003E+01	+6.0600000E+02	+4.7100000E+02	+5.5788964E+02
92.0	17	+4.8129394E+02	+3.6726633E+01	+5.6700000E+02	+4.1300000E+02	+5.5782861E+02
93.0	15	+5.3326660E+02	+6.6359913E+01	+6.3200000E+02	+4.2000000E+02	+5.5776782E+02
94.0	12	+5.1500000E+02	+6.6160960E+01	+6.5900000E+02	+4.0100000E+02	+5.5770678E+02
95.0	24	+5.7100000E+02	+8.9004152E+01	+7.1200000E+02	+4.1700000E+02	+5.5764575E+02
96.0	11	+7.4645434E+02	+2.6197685E+02	+1.3200000E+03	+5.1400000E+02	+5.5758471E+02
97.0	6	+4.8000000E+02	+3.9278492E+01	+5.4200000E+02	+4.3900000E+02	+5.5752368E+02
98.0	9	+4.5488867E+02	+3.1150619E+01	+5.5200000E+02	+4.6200000E+02	+5.5746289E+02
99.0	5	+5.2379980E+02	+1.0263381E+02	+6.6800000E+02	+4.0900000E+02	+5.5740185E+02
100.0	2	+5.5800000E+02	+1.0182337E+02	+6.7000000E+02	+5.2600000E+02	+5.5734082E+02
101.0	9	+4.8244433E+02	+8.9005773E+01	+7.0800000E+02	+3.9600000E+02	+5.5727978E+02
102.0	3	+4.5833325E+02	+1.6165807E+01	+4.7300000E+02	+4.4100000E+02	+5.5721899E+02
103.0	2	+6.0400000E+02	+6.2225396E+01	+6.4800000E+02	+5.6000000E+02	+5.5715795E+02
104.0	7	+5.5557128E+02	+6.1272226E+01	+6.5100000E+02	+4.8300000E+02	+5.5709692E+02
105.0	9	+5.7944433E+02	+9.2818520E+01	+7.2900000E+02	+4.3700000E+02	+5.5703588E+02
106.0	11	+5.9772705E+02	+2.1147439E+02	+1.0260000E+03	+3.4200000E+02	+5.5697509E+02



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
107.0	2	+6.0550000E+02	+6.5760930E+01	+6.5200000E+02	+5.5900000E+02	+5.5691406E+02
108.0	3	+5.2066650E+02	+9.4516312E+00	+5.2800000E+02	+5.1000000E+02	+5.5685302E+02
109.0	14	+5.4771411E+02	+2.0508888E+02	+1.0540000E+03	+4.1700000E+02	+5.5679199E+02
110.0	11	+4.0254541E+02	+6.5477268E+01	+6.3200000E+02	+3.9400000E+02	+5.5673095E+02
111.0	5	+5.8319995E+02	+1.4635812E+02	+7.7600000E+02	+3.9200000E+02	+5.5667016E+02
112.0	6	+5.8150000E+02	+1.7807947E+02	+8.6900000E+02	+3.7900000E+02	+5.5660913E+02
113.0	18	+5.4961108E+02	+1.0597226E+02	+8.0900000E+02	+4.1900000E+02	+5.5654809E+02
115.0	6	+4.9883325E+02	+4.1004471E+01	+5.5600000E+02	+4.4300000E+02	+5.5642626E+02
116.0	6	+4.6700000E+02	+6.255575E+01	+5.7500000E+02	+3.8800000E+02	+5.5636523E+02
117.0	3	+5.0066650E+02	+3.3080709E+01	+5.2500000E+02	+4.6300000E+02	+5.5630419E+02
118.0	4	+4.6525000E+02	+3.5415392E+01	+5.1800000E+02	+4.4200000E+02	+5.5624316E+02
119.0	9	+4.6666650E+02	+2.2901964E+01	+5.1000000E+02	+4.3800000E+02	+5.5618237E+02
120.0	2	+4.8100000E+02	+0.0000000E+99	+4.8100000E+02	+4.8100000E+02	+5.5612133E+02
121.0	3	+4.3966650E+02	+1.1239810E+01	+4.5200000E+02	+4.3000000E+02	+5.5606030E+02
122.0	3	+4.9500000E+02	+8.5854528E+01	+5.7600000E+02	+4.0500000E+02	+5.5599926E+02
123.0	9	+5.5244433E+02	+8.1083461E+01	+6.6900000E+02	+4.1700000E+02	+5.5593823E+02
124.0	6	+5.6416650E+02	+6.8527256E+01	+6.8500000E+02	+4.9400000E+02	+5.5587744E+02
126.0	6	+4.8300000E+02	+1.2959012E+02	+6.9200000E+02	+3.3800000E+02	+5.5575537E+02
127.0	3	+6.9866650E+02	+1.4910510E+02	+8.6500000E+02	+5.7700000E+02	+5.5569433E+02
137.0	1	+4.3200000E+02	+0.0000000E+27	+4.3200000E+02	+4.3200000E+02	+5.5508471E+02

ANB 3066 PROPELLANT (ALL ANB) TENSILE MODULUS: .0002 IN./MIN. 77 DEG F



SECTION V  
HIGH RATE TRIAXIAL

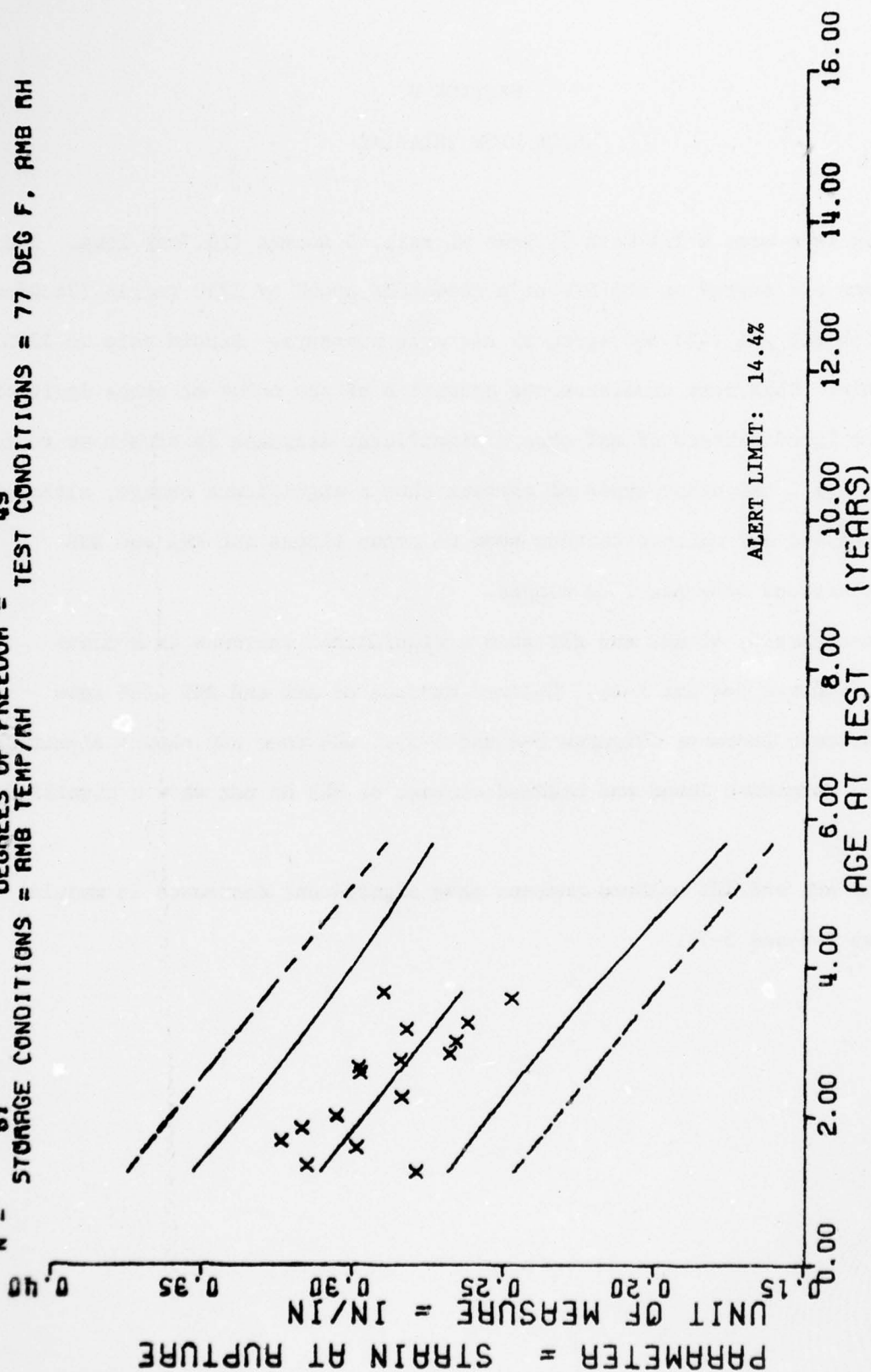
This test uses a 3/4 inch (1.9cm) GL rail, 5 inches (12.7cm) long. The specimens are tested on the MTS at a crosshead speed of 1750 in/min (74.08cm/sec) with 600 psi (421 860 kg/sq m) nitrogen pressure. Strain rate is 1000 in/in/min. This test simulates the condition of the motor at stage ignition.

Only lined cartons of ANT show a significant decrease in strain at rupture (Figure 5-1). No other types of cartons show a significant change, although ANB lined and ANT unlined cartons have negative slopes and ANA and ANB unlined cartons have positive slopes.

Lined cartons of ANB and ANT show a significant increase in maximum stress (Figures 5-2 and 5-3). Unlined cartons of ANB and ANT also show a significant increase (Figures 5-4 and 5-5). ANA does not show a significant change. Composite lined and unlined cartons of ANB do not show a significant change.

Only ANA and ANB unlined cartons show significant decreases in modulus (Figures 5-6 and 5-7).

$Y = ((+3.3503899E-01) + (-1.6148073E-03) \times X)$   
 $F = +2.1039668E+01$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = -5.4808435E-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +4.5869017E+00$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 61$  DEGREES OF FREEDOM = 49  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (ANT) TENSILE STN AT RUP, 1750 IN/MIN, 600 PSI, 77 DEG LINEO

Figure 5-1

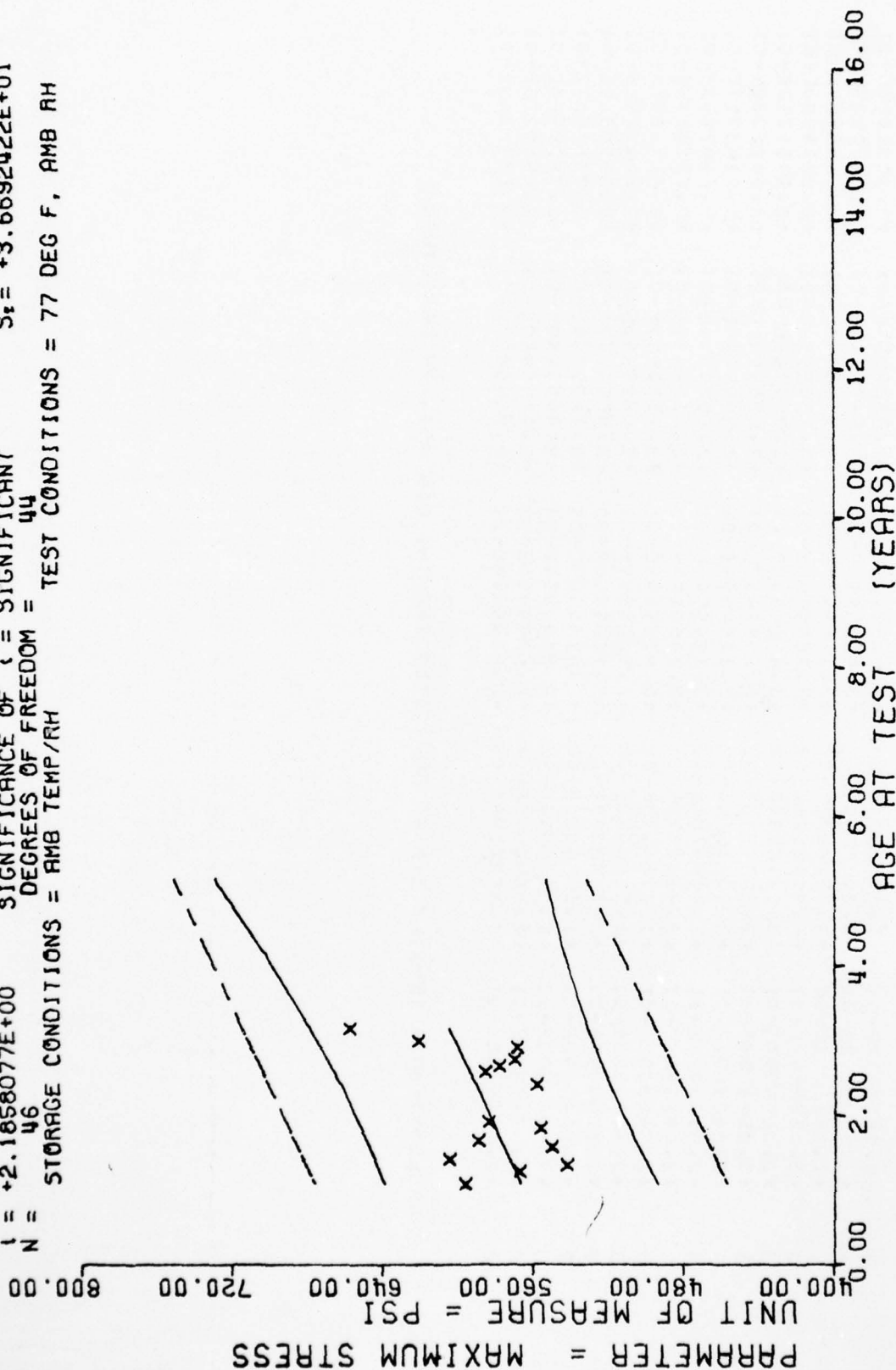
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+2.7516557E-01	+1.6851599E-03	+2.8059995E-01	+2.7729994E-01	+3.1081688E-01
16.0	3	+3.1836062E-01	+2.3002295E-02	+3.4029996E-01	+2.9479998E-01	+3.0920207E-01
19.0	3	+2.9886862E-01	+1.3737838E-02	+3.1469994E-01	+2.9009997E-01	+3.0435764E-01
20.0	3	+3.2386660E-01	+4.2998195E-03	+3.2639998E-01	+3.1989995E-01	+3.0274283E-01
22.0	3	+3.1699997E-01	+2.6190794E-02	+3.4229999E-01	+2.8999996E-01	+2.5951322E-01
24.0	3	+3.0546659E-01	+2.3479935E-02	+3.2959997E-01	+2.8269994E-01	+2.5628360E-01
27.0	6	+2.8403294E-01	+2.0303668E-02	+2.1209999E-01	+2.5999999E-01	+2.5143917E-01
31.0	3	+2.9779994E-01	+1.3194786E-02	+3.1299996E-01	+2.8929996E-01	+2.8497993E-01
32.0	3	+2.9823327E-01	+2.285772E-02	+3.1469994E-01	+2.7209997E-01	+2.8336513E-01
33.0	3	+2.8453332E-01	+1.8744433E-02	+3.0599999E-01	+2.7139997E-01	+2.8175032E-01
34.0	5	+2.6813983E-01	+1.5586370E-02	+2.5699999E-01	+2.4899995E-01	+2.8013551E-01
36.0	2	+2.6599997E-01	+7.0678377E-03	+2.7099996E-01	+2.6099997E-01	+2.7650589E-01
39.0	2	+2.8249996E-01	+1.3434932E-02	+2.9199999E-01	+2.7299994E-01	+2.7367627E-01
39.0	5	+2.6223963E-01	+1.6065810E-02	+2.8199994E-01	+2.4099999E-01	+2.7206146E-01
43.0	1	+2.4749994E-01	+2.5990955E-02	+2.6799994E-01	+2.2699999E-01	+2.6560223E-01
44.0	2	+2.8999996E-01	+1.4027190E-03	+2.9099994E-01	+2.8899997E-01	+2.6398742E-01

ANB 3065 PROPELLANT(ANT) TENSILE STN AT RUP. 1750 IN/MIN. 600 PSI. 77 DEG LINED

$Y = ((+5.4682293E+02) + (+1.5241589E+00) * X)$   
 $F = +4.777553E+00$  SIGNIFICANCE OF F = SIGNIFICANT  $G_1 = +3.8201554E+01$   
 $R = +3.1296880E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_1 = +6.9729783E-01$   
 $t = +2.1858077E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_2 = +3.6692422E+01$   
 $N = 46$  DEGREES OF FREEDOM = 44  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



ANB 3066 PROPELLANT (ANB) TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI, 77 DEG LINED

Figure 5-2



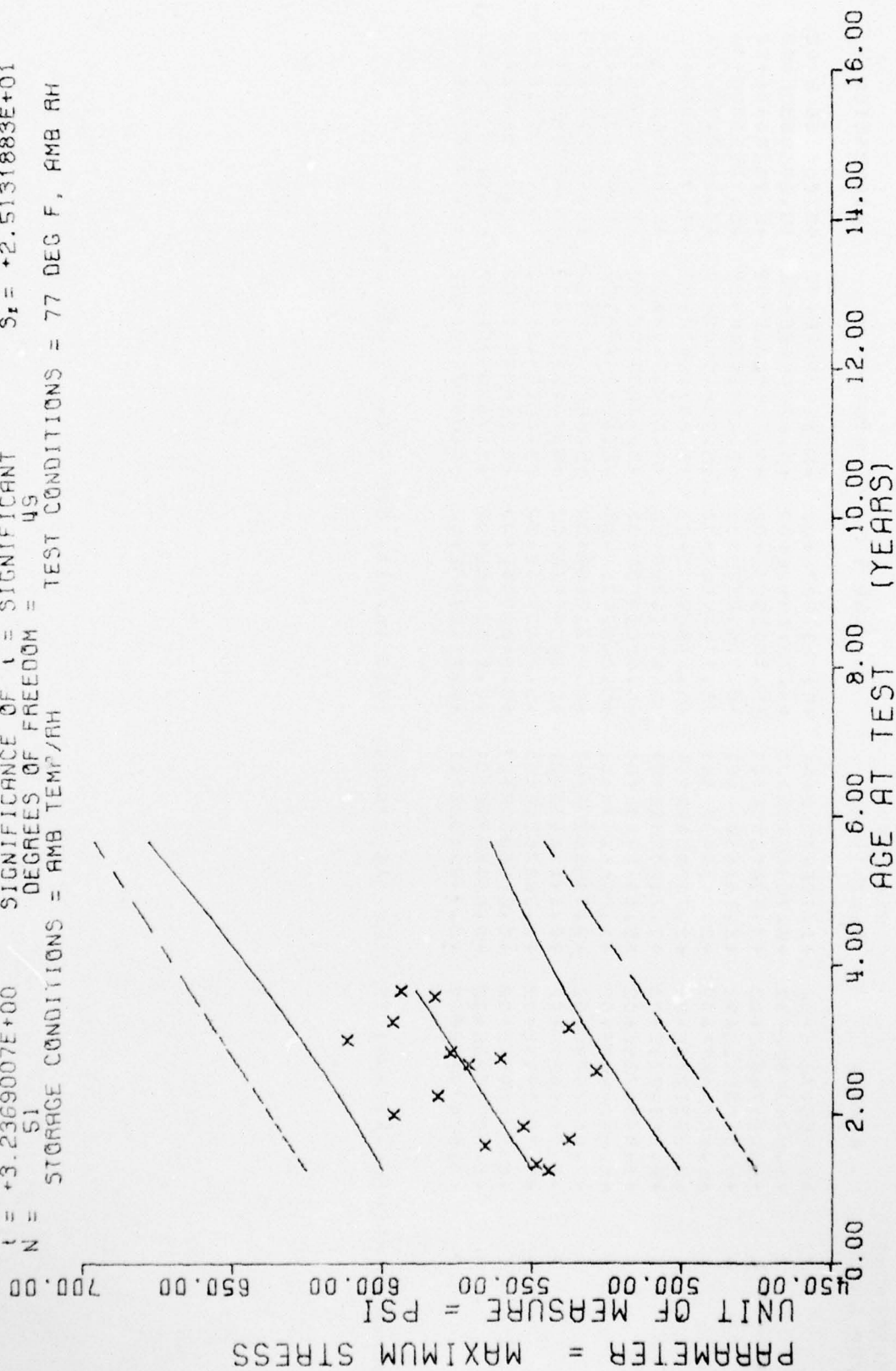
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	3	+5.9631733E+02	+1.2012212E+01	+6.0511987E+02	+5.8242588E+02	+5.8662656E+02
15.0	2	+5.6743481E+02	+6.7034040E+00	+5.7216992E+02	+5.6269995E+02	+5.6968530E+02
16.0	4	+5.4217480E+02	+3.6145055E+01	+5.7873995E+02	+4.9300000E+02	+5.7120947E+02
17.0	6	+6.0485131E+02	+2.1414104E+01	+6.3251977E+02	+5.6883564E+02	+5.7273339E+02
19.0	4	+5.5024487E+02	+2.2439493E+01	+5.7764960E+02	+5.3085560E+02	+5.7578173E+02
20.0	4	+5.8921225E+02	+2.7280547E+01	+6.2956982E+02	+5.6921957E+02	+5.7730590E+02
22.0	4	+5.5612231E+02	+3.7370281E+01	+5.9302978E+02	+5.0891952E+02	+5.8035424E+02
23.0	4	+5.8406225E+02	+5.1151913E+01	+6.4091992E+02	+5.2203979E+02	+5.8187841E+02
29.0	2	+5.5824487E+02	+1.5965147E+01	+5.6952978E+02	+5.4695556E+02	+5.9102343E+02
31.0	2	+5.8602978E+02	+2.7155030E+01	+6.0522998E+02	+5.6682983E+02	+5.9407177E+02
32.0	2	+5.7845487E+02	+1.1417652E+01	+5.8655581E+02	+5.7042593E+02	+5.9559594E+02
33.0	2	+5.7015991E+02	+1.3087656E+01	+5.7940991E+02	+5.6090991E+02	+5.9712011E+02
35.0	1	+5.6868994E+02	+0.000000E+27	+5.6868994E+02	+5.6868994E+02	+6.0016845E+02
36.0	4	+6.2093725E+02	+4.0345978E+01	+6.6350976E+02	+5.7050976E+02	+6.0169262E+02
38.0	2	+6.5747973E+02	+2.9492102E+01	+6.7832983E+02	+6.3662588E+02	+6.0474096E+02

ANB 3066 PROPELLANT(ANB) TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI, 77 DEG LINED

$Y = ((+5.3034254E+02) + ((+1.3378653E+00) * X)$   
 $F = +1.0477526E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G = +2.7410469E+01$   
 $R = +4.1971349E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_1 = +4.1331677E-01$   
 $t = +3.2369007E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_2 = +2.5131883E+01$   
 $N = 51$  DEGREES OF FREEDOM = 49  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



ANB 3066 PROPELLANT (ANT) TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI, 77 DEG LINED

Figure 5-3

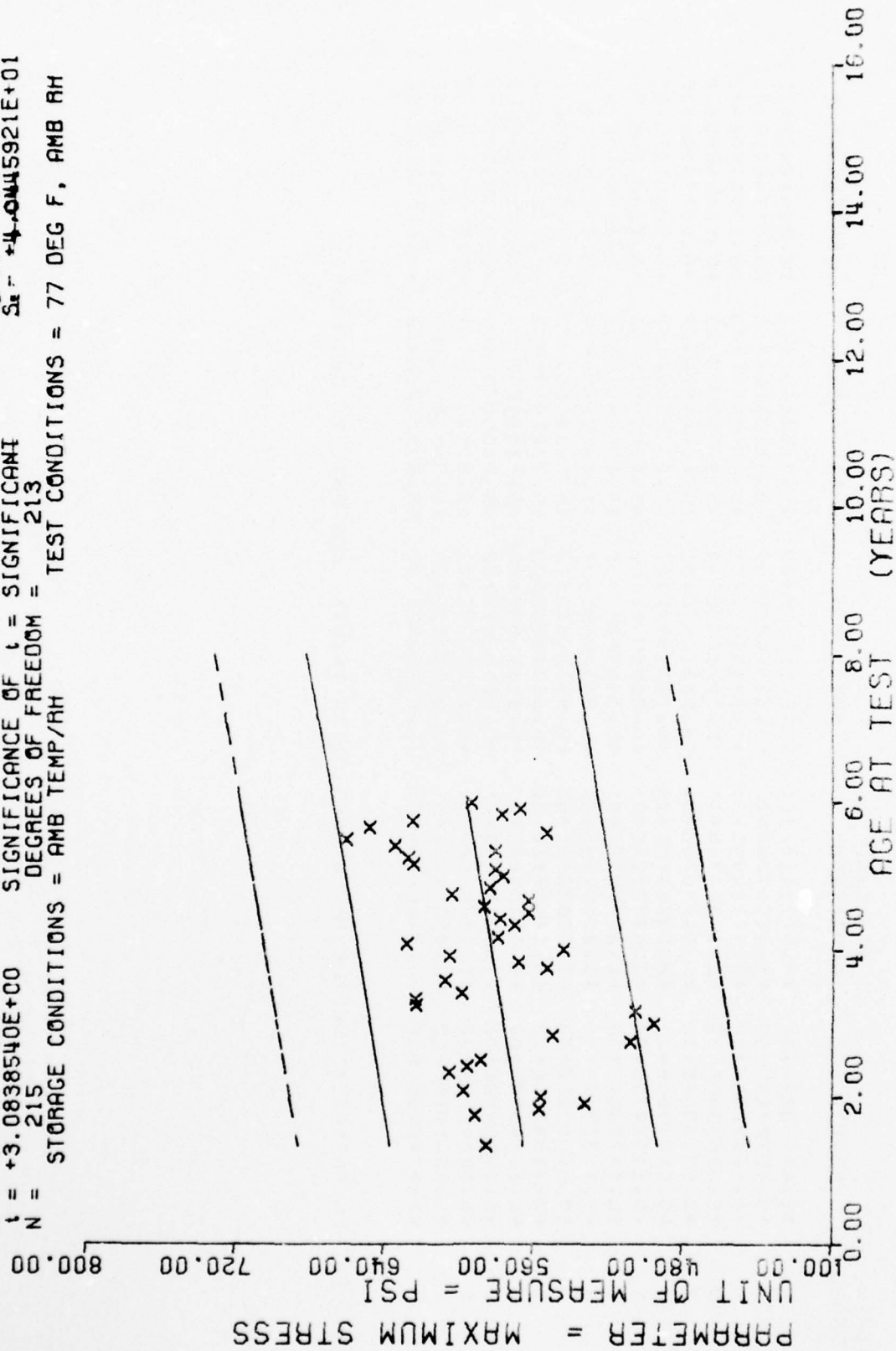
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+5.4463989E+02	+6.1073618E+00	+5.5085586E+02	+5.3866552E+02	+5.5041040E+02
16.0	3	+5.4878320E+02	+7.4891723E+00	+5.5734985E+02	+5.4355581E+02	+5.5174829E+02
19.0	3	+5.6592651E+02	+2.5032954E+01	+5.8417953E+02	+5.3244555E+02	+5.5576156E+02
20.0	3	+5.3783300E+02	+2.2058211E+01	+5.5227978E+02	+5.1244955E+02	+5.5709585E+02
22.0	3	+5.5314306E+02	+5.4148675E+00	+5.5690951E+02	+5.4694555E+02	+5.5977539E+02
24.0	3	+5.9634985E+02	+2.9398610E+01	+6.2001977E+02	+5.6343554E+02	+5.6245117E+02
27.0	6	+5.8172973E+02	+2.5837751E+01	+6.2500976E+02	+5.6240991E+02	+5.6646484E+02
31.0	3	+5.2870654E+02	+1.2377888E+01	+5.3587588E+02	+5.1540951E+02	+5.7181616E+02
32.0	3	+5.7121313E+02	+9.3305954E+00	+5.8114950E+02	+5.6265551E+02	+5.7315405E+02
33.0	3	+5.6060302E+02	+7.2003380E+00	+5.6516552E+02	+5.5231982E+02	+5.7449154E+02
34.0	5	+5.7734375E+02	+8.1456716E+00	+5.8877978E+02	+5.7026577E+02	+5.7582583E+02
36.0	2	+6.1184472E+02	+6.0425493E+00	+6.1605585E+02	+6.0758984E+02	+5.7850561E+02
38.0	2	+5.3790478E+02	+1.2247308E+01	+5.4655581E+02	+5.2925000E+02	+5.8118139E+02
39.0	5	+5.9664770E+02	+1.6580908E+01	+6.1726577E+02	+5.8262588E+02	+5.8251528E+02
43.0	2	+5.8244970E+02	+3.2008055E+01	+6.0507983E+02	+5.5581982E+02	+5.8767066E+02
44.0	2	+5.9392968E+02	+6.5516655E+00	+5.9856582E+02	+5.8928579E+02	+5.8920849E+02

ANB 3066 PROPELLANT(ANT) TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI, 77 DEG LINED

$F = +9.5101557E+00$   
 $R = +2.0673732E-01$   
 $t = +3.0838540E+00$   
 $N = 215$   
 $Y = (( +5.5589697E+02 ) + ( +5.5336914E-01 ) ) \cdot X$   
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM = 213  
 STORAGE CONDITIONS = AMB TEMP/AM  
 TEST CONDITIONS = 77 DEG F, AMB RH



ANB 3066 PROPELLANT (ANB) TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI, 77 DEG UNLND

Figure 5-4



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	8	+5.8472949E+02	+2.5755353E+01	+6.2000000E+02	+5.3979930E+02	+5.6475073E+02
21.0	2	+5.5045937E+02	+2.6774965E+01	+6.0979926E+02	+5.7193994E+02	+5.6751757E+02
22.0	2	+5.5638476E+02	+1.0820743E+01	+5.6402978E+02	+5.4873999E+02	+5.6807134E+02
23.0	2	+5.3182983E+02	+1.5388167E+01	+5.4270996E+02	+5.2094995E+02	+5.6862426E+02
24.0	2	+5.5563989E+02	+2.5738421E+01	+5.7457983E+02	+5.3669955E+02	+5.6917773E+02
25.0	2	+5.5723486E+02	+1.5529364E+01	+6.0820996E+02	+5.8625976E+02	+5.6973120E+02
28.0	6	+6.0484085E+02	+1.5506230E+01	+6.2038989E+02	+5.8370096E+02	+5.7139111E+02
29.0	2	+5.5525488E+02	+2.7530646E+01	+6.1471997E+02	+5.7578979E+02	+5.7194458E+02
30.0	4	+5.8786987E+02	+1.7224492E+01	+6.0767993E+02	+5.6721997E+02	+5.7249804E+02
33.0	2	+5.0750000E+02	+3.5355339E+00	+5.1000000E+02	+5.0500000E+02	+5.7415795E+02
34.0	6	+5.4916650E+02	+6.0861365E+01	+6.4500000E+02	+5.0500000E+02	+5.7471142E+02
36.0	2	+4.5500000E+02	+1.4142135E+01	+5.0500000E+02	+4.8500000E+02	+5.7581811E+02
38.0	1	+5.0500000E+02	+0.0000000E+00	+5.0500000E+02	+5.0500000E+02	+5.7692430E+02
39.0	4	+6.2250000E+02	+2.5000000E+01	+6.5000000E+02	+5.9000000E+02	+5.7747927E+02
40.0	2	+6.2294482E+02	+9.8293488E+00	+6.2989990E+02	+6.1598999E+02	+5.7803173E+02
41.0	6	+5.9792651E+02	+2.8804269E+01	+6.3590991E+02	+5.7000000E+02	+5.7858496E+02
43.0	2	+6.0702490E+02	+6.4302697E+00	+6.1155981E+02	+6.0248999E+02	+5.7969165E+02
45.0	7	+5.5229687E+02	+1.3038065E+01	+5.6931982E+02	+5.4097998E+02	+5.8079856E+02
46.0	7	+5.6742846E+02	+1.5733157E+01	+5.7643994E+02	+5.3000000E+02	+5.8135180E+02
47.0	2	+6.0458471E+02	+4.2464954E+00	+6.0755981E+02	+6.0160986E+02	+5.8190527E+02
48.0	4	+5.4333232E+02	+4.2273191E+01	+5.8395956E+02	+4.9000000E+02	+5.8245849E+02
49.0	2	+6.2750000E+02	+2.4748737E+01	+6.4500000E+02	+6.1000000E+02	+5.8301196E+02
50.0	4	+5.7475000E+02	+3.2755436E+01	+6.2000000E+02	+5.5000000E+02	+5.8356542E+02
52.0	5	+5.6987573E+02	+3.7071333E+01	+6.1541952E+02	+5.4039999E+02	+5.8467211E+02
53.0	9	+5.7757934E+02	+3.1751080E+01	+6.3804980E+02	+5.5025976E+02	+5.8522534E+02
54.0	16	+5.6214965E+02	+4.1428000E+01	+6.3451977E+02	+5.0500000E+02	+5.8577880E+02
55.0	12	+5.8590072E+02	+3.3847500E+01	+6.2000000E+02	+5.1276977E+02	+5.8633227E+02
56.0	8	+5.6229101E+02	+3.7268351E+01	+6.0815991E+02	+5.009985E+02	+5.8688549E+02
57.0	6	+6.0331494E+02	+4.7557310E+01	+6.4500000E+02	+5.3694995E+02	+5.8743896E+02
58.0	5	+5.8289575E+02	+3.6655740E+01	+6.2000000E+02	+5.3619955E+02	+5.8799213E+02
60.0	4	+5.7567993E+02	+3.6157913E+01	+6.1500000E+02	+5.2971997E+02	+5.8900912E+02

ANR 3066 PROPELLANT(ANR) TENSILE MAX STRESS, 1760 IN/MIN, 600 PSI, 77 DEG UNLND

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
61.0	2	+5.800000E+02	+1.4142135E+01	+5.9000000E+02	+5.7000000E+02	+5.2965234E+02
62.0	4	+6.2376730E+02	+8.5954070E+00	+6.3662385E+02	+6.1843994E+02	+5.9020581E+02
63.0	6	+6.2679467E+02	+4.1245974E+00	+6.3055981E+02	+6.2000000E+02	+5.5075903E+02
64.0	4	+5.8003222E+02	+7.6235632E+01	+6.7000000E+02	+5.0501977E+02	+5.5131250E+02
65.0	4	+6.3375000E+02	+1.1026778E+01	+6.4500000E+02	+6.2000000E+02	+5.9186596E+02
66.0	2	+6.6000000E+02	+7.0710678E+00	+6.6500000E+02	+6.5500000E+02	+5.5241918E+02
67.0	4	+5.5250000E+02	+1.8484227E+01	+5.8000000E+02	+5.4000000E+02	+5.9297265E+02
68.0	4	+6.4750000E+02	+1.1502380E+01	+6.6500000E+02	+6.4000000E+02	+5.9352587E+02
69.0	10	+6.2435571E+02	+2.1778190E+01	+6.5000000E+02	+5.8655081E+02	+5.5407934E+02
70.0	7	+5.7642846E+02	+3.5203490E+01	+6.2500000E+02	+5.4000000E+02	+5.5463281E+02
71.0	3	+5.6663305E+02	+2.6665253E+01	+5.9736987E+02	+5.4973999E+02	+5.9518603E+02
72.0	19	+5.9281360E+02	+3.7021402E+01	+6.6000000E+02	+5.3000000E+02	+5.5573950E+02

ANE 3066 PROPELLANT(ANB) TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI, 77 DEG UNLND

$Y = ((+5.8116822E+02) + (+6.9764555E-01) * X)$   
 $F = +1.4134526E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G = +3.3086524E+01$   
 $R = +2.8166685E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S = +1.8556419E-01$   
 $C = +3.7595915E+00$  SIGNIFICANCE OF C = SIGNIFICANT  $S = +3.1843373E+01$   
 $N = 166$  DEGREES OF FREEDOM = 164  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

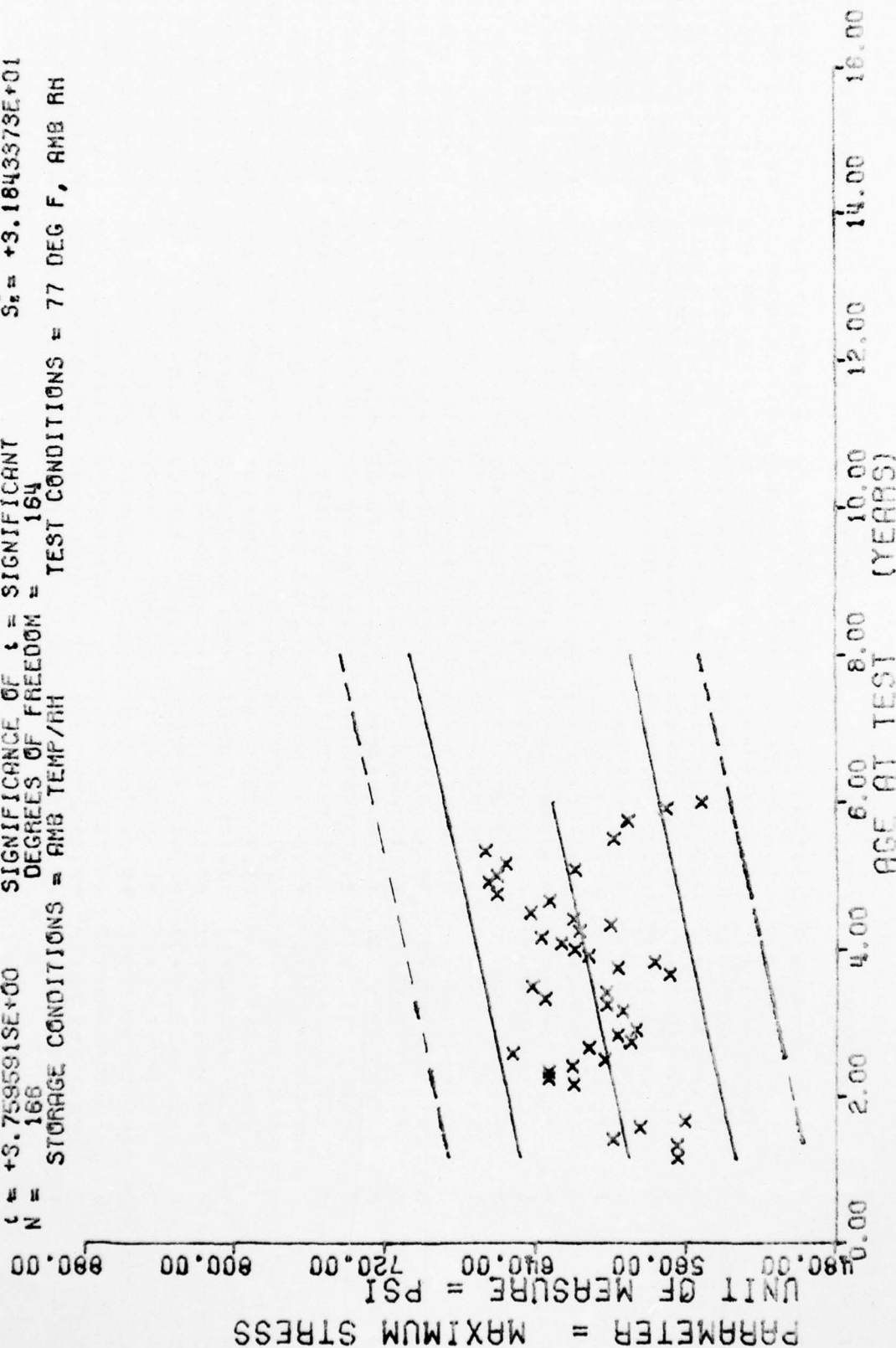


Figure 5-5

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF LINE SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
14.0	2	+5.645946E+02	+1.420330E+01	+5.7459884E+02	+5.5451977E+02	+5.5092505E+02
16.0	3	+5.6434943E+02	+1.2145975E+01	+5.7602570E+02	+5.5192954E+02	+5.5233032E+02
17.0	5	+5.6894772E+02	+1.7164894E+01	+6.1811992E+02	+5.7315992E+02	+5.9302507E+02
19.0	2	+5.8459976E+02	+2.1727169E+01	+5.9586987E+02	+5.6914990E+02	+5.9442333E+02
20.0	2	+5.6053491E+02	+4.0124323E+00	+5.6335986E+02	+5.5770956E+02	+5.5512109E+02
26.0	1	+5.1584085E+02	+0.000000E+00	+6.1984985E+02	+6.1984985E+02	+5.5930688E+02
27.0	2	+6.3314477E+02	+5.2326571E+00	+6.3668954E+02	+6.2956955E+02	+6.0000462E+02
28.0	1	+6.7310935E+02	+0.000000E+00	+6.7310935E+02	+6.7310935E+02	+6.0070214E+02
29.0	2	+5.2063980E+02	+1.7537262E+01	+6.3207923E+02	+6.0219955E+02	+6.0139990E+02
30.0	3	+6.0311645E+02	+4.2450181E+01	+6.3619955E+02	+5.5525000E+02	+6.0209741E+02
31.0	2	+6.5223486E+02	+5.5078841E+01	+6.9117993E+02	+6.1328979E+02	+6.0279516E+02
32.0	1	+6.1193986E+02	+0.000000E+00	+6.1185986E+02	+6.1185986E+02	+6.0349267E+02
33.0	2	+5.8546484E+02	+4.5202099E+00	+5.8291992E+02	+5.8503976E+02	+6.0419042E+02
34.0	1	+5.5609005E+02	+0.000000E+00	+5.5609005E+02	+5.5609005E+02	+6.0488793E+02
35.0	3	+5.8566067E+02	+1.2110063E+01	+5.9537988E+02	+5.7528979E+02	+6.0559559E+02
38.0	5	+5.9382983E+02	+7.4540201E+00	+6.0347998E+02	+5.8751977E+02	+6.0767871E+02
39.0	5	+6.0228784E+02	+1.7345633E+01	+6.1854980E+02	+5.8061987E+02	+6.0837622E+02
40.0	2	+6.3529971E+02	+7.2531863E+00	+6.4031982E+02	+6.3005585E+02	+6.0907397E+02
41.0	7	+5.0259537E+02	+1.1517630E+01	+6.1876977E+02	+5.8755981E+02	+6.0977148E+02
42.0	3	+6.4236640E+02	+4.5276195E+00	+6.4632683E+02	+6.3665991E+02	+6.1046923E+02
44.0	5	+5.6904814E+02	+2.5414654E+01	+5.9151977E+02	+5.3657983E+02	+6.1186450E+02
45.0	6	+5.5678908E+02	+1.3376974E+01	+6.1312988E+02	+5.7908924E+02	+6.1256225E+02
46.0	4	+5.7651479E+02	+1.7432863E+01	+6.0170996E+02	+5.6072953E+02	+6.1325976E+02
47.0	11	+6.1200503E+02	+3.1016174E+01	+6.4367993E+02	+5.7220956E+02	+6.1395751E+02
48.0	10	+6.1945068E+02	+2.2561757E+01	+6.5288989E+02	+5.8820980E+02	+6.1465502E+02
49.0	6	+6.2040820E+02	+1.4934233E+01	+6.4202978E+02	+6.0970956E+02	+6.1535278E+02
50.0	9	+6.3721777E+02	+1.5667499E+01	+6.5129980E+02	+6.1645956E+02	+6.1625029E+02
51.0	3	+6.1764321E+02	+1.2247862E+01	+6.2445956E+02	+6.0289900E+02	+6.1674804E+02
52.0	2	+6.0045483E+02	+8.5222648E+00	+6.0647958E+02	+5.9442953E+02	+6.1744555E+02
53.0	12	+6.1996118E+02	+2.3686816E+01	+6.5133984E+02	+5.9517993E+02	+6.1814331E+02
54.0	7	+6.6252302E+02	+1.1055956E+01	+6.5484085E+02	+6.2233984E+02	+6.1884106E+02

ANS-3000 PROPYLENE (ANI) TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI, 77 DEG UNLND



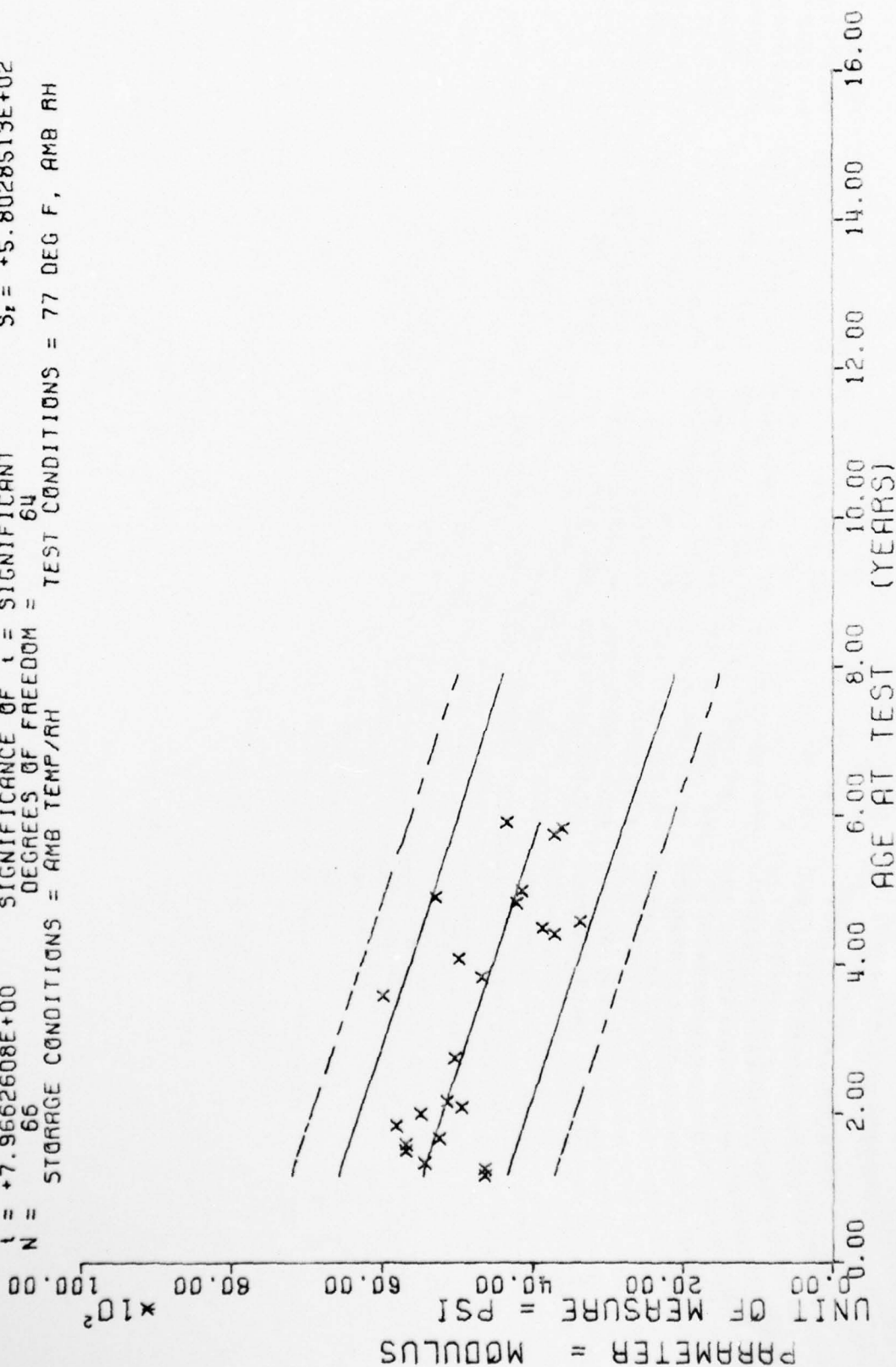
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
55.0	6	+1.3288813E+02	+3.6142994E+01	+6.8621957E+02	+5.0117953E+02	+6.2023632E+02
57.0	6	+6.6364457E+02	+3.4545907E+01	+6.8677976E+02	+6.0585956E+02	+6.2093383E+02
59.0	2	+1.6567393E+02	+1.6367922E+00	+6.6621657E+02	+6.6332054E+02	+6.2232910E+02
60.0	2	+6.6355981E+02	+5.8803076E+00	+6.6470950E+02	+6.5640951E+02	+6.2302685E+02
61.0	2	+6.1912988E+02	+5.6735277E+00	+6.2512588E+02	+6.1512588E+02	+6.2372436E+02
62.0	2	+6.5580453E+02	+4.0001125E+00	+6.5866992E+02	+6.5293994E+02	+6.2442211E+02
64.0	4	+6.6671972E+02	+2.2815007E+01	+6.9655985E+02	+6.4331922E+02	+6.2581738E+02
66.0	2	+5.6870280E+02	+5.5207915E+00	+6.3265955E+02	+5.5485955E+02	+6.2721264E+02
68.0	4	+5.4120433E+02	+7.5597975E+00	+5.6618964E+02	+5.7997958E+02	+6.2930566E+02
71.0	4	+5.7076435E+02	+2.4599734E+00	+5.7278979E+02	+5.6730981E+02	+6.3070092E+02
72.0	2	+5.5171997E+02	+9.9290157E+00	+5.5673999E+02	+5.4465955E+02	+6.3139868E+02

AND 3.66 PROPELLANT(T) TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI, 77 DEG UNLND

$Y = (1 + 5.8611089E+03) + (-2.7538323E+01) \times X$   
 $F = +6.3461311E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G_1 = +8.1259465E+02$   
 $R = -7.0561097E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_1 = +3.4568694E+00$   
 $t = +7.9662608E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_2 = +5.8028513E+02$   
 $N = 66$  DEGREES OF FREEDOM = 64  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (ANA) TENSILE MODULUS, 1750 IN/MIN, 600 PSI, 77 DEG UNLND

Figure 5-6

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIES POP GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
14.0	2	+4.6500000E+03	+7.0710078E+01	+4.7000000E+03	+4.6000000E+03	+5.4755703E+03
15.0	2	+4.6500000E+03	+3.5255339E+02	+4.9000000E+03	+4.4000000E+03	+5.4480312E+03
16.0	2	+5.4500000E+03	+7.7781745E+02	+6.0000000E+03	+4.9000000E+03	+5.4204921E+03
18.0	4	+5.7000000E+03	+1.4142135E+02	+5.8000000E+03	+5.6000000E+03	+5.3654179E+03
19.0	2	+5.7000000E+03	+1.4142135E+02	+5.8000000E+03	+5.6000000E+03	+5.3378789E+03
20.0	2	+5.2500000E+03	+4.3497474E+02	+5.6000000E+03	+4.9000000E+03	+5.3103398E+03
22.0	4	+5.4250000E+03	+6.3442887E+02	+6.6000000E+03	+5.1000000E+03	+5.2592666E+03
24.0	2	+5.5000000E+03	+1.4142135E+02	+5.6000000E+03	+5.4000000E+03	+5.2001879E+03
25.0	2	+4.9500000E+03	+3.5255339E+02	+5.2000000E+03	+4.7000000E+03	+5.1726484E+03
26.0	2	+5.1500000E+03	+3.5255339E+02	+5.4000000E+03	+4.9000000E+03	+5.1451093E+03
30.0	2	+5.6500000E+03	+2.1213203E+02	+5.2000000E+03	+4.9000000E+03	+4.9523437E+03
33.0	2	+5.0000000E+03	+0.0000000E+03	+6.0000000E+03	+6.0000000E+03	+4.6769609E+03
40.0	2	+4.6875000E+03	+1.4493964E+02	+4.7900000E+03	+4.5850000E+03	+4.5943437E+03
45.0	1	+5.0000000E+03	+0.0000000E+11	+5.0000000E+03	+5.0000000E+03	+4.5117304E+03
53.0	3	+3.7273332E+03	+3.2608792E+01	+3.7620000E+03	+3.6970000E+03	+4.4015742E+03
54.0	3	+3.8533332E+03	+1.4579055E+02	+4.0120000E+03	+3.7200000E+03	+4.3740390E+03
55.0	3	+3.3830000E+03	+1.1980819E+02	+3.5120000E+03	+3.2760000E+03	+4.3465000E+03
56.0	5	+4.2245000E+03	+4.0682145E+02	+4.7360000E+03	+3.7290000E+03	+4.2638828E+03
57.0	1	+5.3000000E+03	+0.0000000E+31	+5.3000000E+03	+5.3000000E+03	+4.2363476E+03
62.0	3	+4.1573320E+03	+3.0193537E+02	+4.4170000E+03	+3.8260000E+03	+4.2088085E+03
68.0	0	+3.7276665E+03	+1.6251974E+02	+3.9130000E+03	+3.4450000E+03	+3.5609645E+03
71.0	3	+3.6150000E+03	+2.5894014E+01	+3.6300000E+03	+3.5850000E+03	+3.9234262E+03
75.0	1	+4.2553320E+03	+3.1688720E+02	+4.8790000E+03	+3.9190000E+03	+3.9058879E+03

AGE 3000 POLYMERANT(ANA) TENSILE MODULUS, 1750 IN/MIN, 600 PSI, 77 DEG UNLND

AD-A043 656

OGDEN AIR LOGISTICS CENTER HILL AFB UTAH PROPELLANT L--ETC F/G 21/9.2  
PROPELLANT SURVEILLANCE REPORT MINUTEMAN III STAGE III, (U)

UNCLASSIFIED

JUL 77 E M DALABA  
MANCP-374(77)

NL

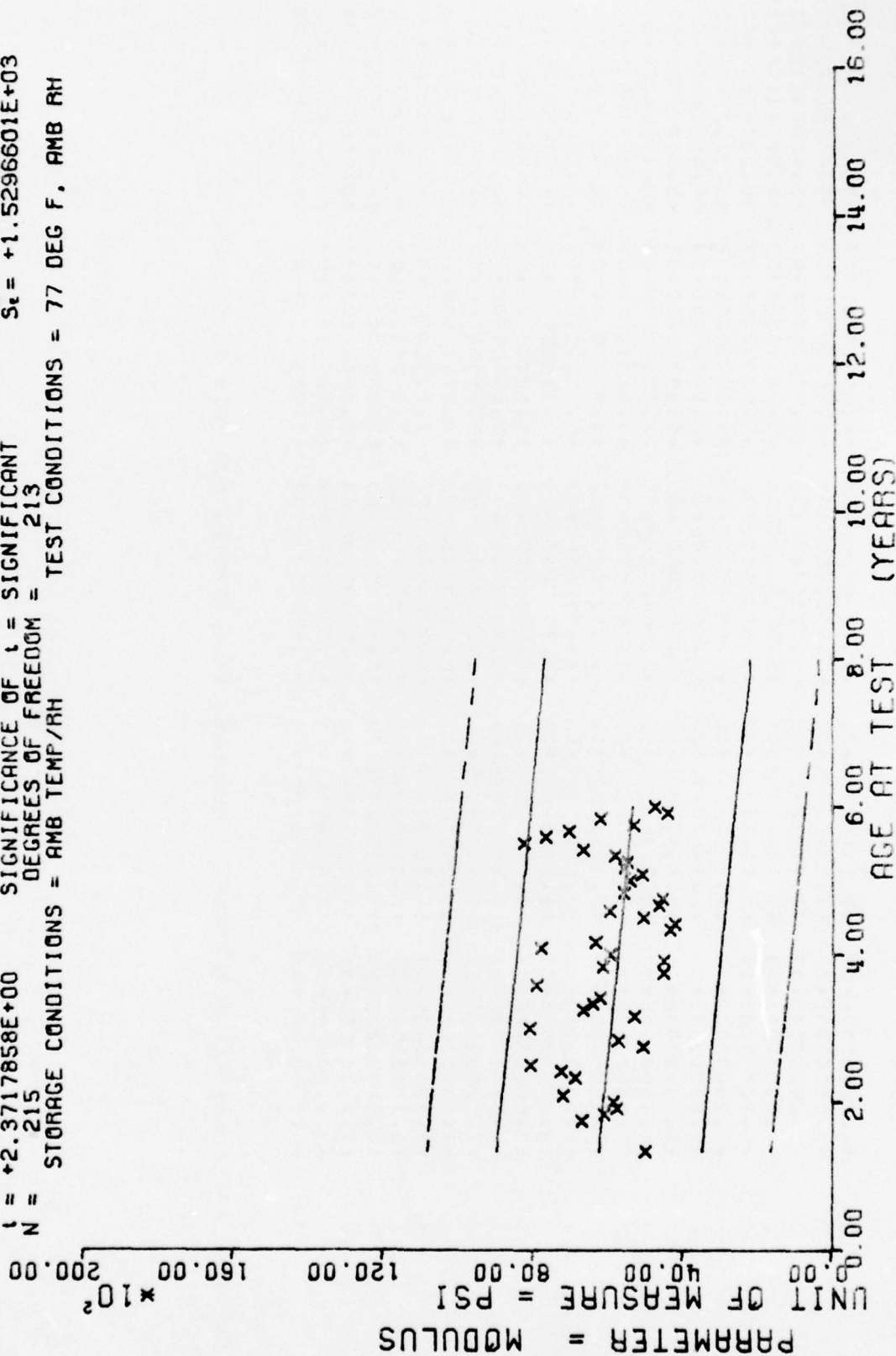
2 OF 3

AD  
A043656





$Y = ((+6.4929722E+03) + (-1.6095957E+01) * X)$   
 $F = +5.6253682E+00$  SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_1 = +1.5461026E+03$   
 $R = -1.6040769E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +6.7864294E+00$   
 $t = +2.3717858E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_t = +1.5296601E+03$   
 $N = 215$  DEGREES OF FREEDOM = 213  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH



ANB 3066 PROPELLANT (ANB) TENSILE MODULUS, 1750 IN/MIN, 600 PSI, 77 DEG F, UNLND

Figure 5-7

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	8	+4.5901250E+03	+1.8282999E+03	+7.5060000E+03	+3.1470000E+03	+6.2354335E+03
21.0	2	+6.7000000E+03	+2.8284271E+02	+6.9000000E+03	+6.5000000E+03	+6.1540570E+03
22.0	2	+6.1000000E+03	+2.8284271E+02	+6.3000000E+03	+5.9000000E+03	+6.1388593E+03
23.0	2	+5.7500000E+03	+2.1213203E+02	+5.9000000E+03	+5.6000000E+03	+6.1227617E+03
24.0	2	+5.8500000E+03	+4.9497474E+02	+6.2000000E+03	+5.5000000E+03	+6.1066679E+03
25.0	2	+7.2000000E+03	+8.4852813E+02	+7.8000000E+03	+6.6000000E+03	+6.0905703E+03
28.0	6	+6.8833330E+03	+7.5078490E+02	+7.6000000E+03	+5.7000000E+03	+6.0422851E+03
29.0	2	+7.2500000E+03	+7.7781745E+02	+7.8000000E+03	+6.7000000E+03	+6.0261875E+03
30.0	4	+8.0750000E+03	+1.1176612E+03	+9.2000000E+03	+6.8000000E+03	+6.0100895E+03
33.0	2	+5.0500000E+03	+3.8355339E+02	+5.3600000E+03	+4.8600000E+03	+5.5618046E+03
34.0	6	+5.7166640E+03	+6.8239773E+02	+6.6000000E+03	+5.0000000E+03	+5.5457070E+03
36.0	2	+8.1000000E+03	+2.8284271E+02	+8.3000000E+03	+7.9000000E+03	+5.5135156E+03
38.0	1	+5.3000000E+03	+0.0000000E+03	+5.3000000E+03	+5.3000000E+03	+5.8813242E+03
39.0	4	+6.6750000E+03	+1.5261607E+03	+8.4000000E+03	+5.2000000E+03	+5.8652265E+03
40.0	2	+6.4100000E+03	+8.6267027E+02	+7.0200000E+03	+5.8000000E+03	+5.9491328E+03
41.0	0	+6.2076640E+03	+8.2744901E+02	+7.1000000E+03	+4.9000000E+03	+5.8330351E+03
42.0	2	+7.9195000E+03	+4.3075515E+01	+7.9500000E+03	+7.8890000E+03	+5.8008437E+03
45.0	7	+4.5314257E+03	+1.6618149E+03	+7.1000000E+03	+3.4360000E+03	+5.7686523E+03
46.0	7	+6.1602851E+03	+1.7611238E+03	+8.9000000E+03	+3.8780000E+03	+5.7525546E+03
47.0	2	+4.5210000E+03	+2.4039550E+02	+4.6510000E+03	+4.3510000E+03	+5.7364609E+03
48.0	4	+5.9500000E+03	+5.4467115E+02	+6.7000000E+03	+5.5000000E+03	+5.7203632E+03
49.0	2	+7.8000000E+03	+1.4142135E+02	+7.9000000E+03	+7.7000000E+03	+5.7042695E+03
50.0	4	+6.3500000E+03	+1.5545631E+03	+8.0000000E+03	+4.7000000E+03	+5.6881718E+03
52.0	5	+4.3470000E+03	+1.7056596E+02	+4.5790000E+03	+4.1120000E+03	+5.6559804E+03
53.0	9	+4.2291093E+03	+2.3252058E+02	+4.5240000E+03	+3.7970000E+03	+5.6398828E+03
54.0	16	+5.0713125E+03	+1.5062636E+03	+8.3000000E+03	+2.6400000E+03	+5.6237890E+03
55.0	12	+5.5760000E+03	+1.8956542E+03	+8.6000000E+03	+3.1000000E+03	+5.6076914E+03
56.0	8	+4.6466250E+03	+1.1056623E+03	+6.6000000E+03	+3.6000000E+03	+5.5915976E+03
57.0	6	+4.5623320E+03	+1.3823006E+03	+6.3000000E+03	+3.3380000E+03	+5.5755000E+03
58.0	5	+5.5923984E+03	+1.9349542E+03	+7.9000000E+03	+3.9640000E+03	+5.5594062E+03
60.0	4	+5.4225000E+03	+9.2269008E+02	+6.8000000E+03	+4.9000000E+03	+5.5272109E+03

ANS 3006 PROPELLANT(ANS) TENSILE MODULUS, 1750 IN/MIN, 600 PSI, 77 DEG F + UMLND

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
61.0	2	+5.1000000E+03	+1.4142135E+02	+5.2000000E+03	+5.0000000E+03	+5.5111171E+03
62.0	4	+5.5790000E+03	+1.0672700E+03	+6.6000000E+03	+4.6120000E+03	+5.4950195E+03
63.0	6	+5.4961000E+03	+1.6465000E+03	+7.9000000E+03	+4.2710000E+03	+5.4789257E+03
64.0	4	+5.8250000E+03	+4.9244289E+02	+6.4000000E+03	+5.2000000E+03	+5.4628281E+03
65.0	4	+6.6750000E+03	+1.3022416E+03	+7.9000000E+03	+5.5000000E+03	+5.4467343E+03
66.0	2	+8.2500000E+03	+7.7781745E+02	+8.8000000E+03	+7.7000000E+03	+5.4306367E+03
67.0	4	+7.6750000E+03	+3.5939764E+02	+8.2000000E+03	+7.4000000E+03	+5.4145429E+03
68.0	4	+7.0500000E+03	+1.6256331E+03	+8.8000000E+03	+5.3000000E+03	+5.3984453E+03
69.0	10	+5.3167968E+03	+1.0727970E+03	+6.4000000E+03	+3.0550000E+03	+5.3823476E+03
70.0	7	+6.2142851E+03	+9.2452036E+02	+7.5000000E+03	+5.2000000E+03	+5.3662539E+03
71.0	3	+4.4210000E+03	+4.9076521E+02	+4.9650000E+03	+4.0220000E+03	+5.3501562E+03
72.0	19	+4.7586289E+03	+1.2444507E+03	+7.7000000E+03	+3.3100000E+03	+5.3340625E+03

ANS 3066 PROPELLANT(ANS) TENSILE MODULUS, 1750 IN/MIN, 600 PSI, 77 DEG F, UNLND

## SECTION VI

### STRESS RELAXATION

An end-bonded 1/2" x 1/2" x 4" (1.27 x 1.27 x 10.16cm) is used on the Stress Relaxometer. The specimens are tested at seven different temperatures to derive a master stress relaxation curve.

A strain of 1% at 77°F (25.0°C) was not introduced into the program until Phase 3 of Minuteman III testing and Phase B Series 2 for Minuteman II which has resulted in a relatively short time frame for analysis. Prior to that time strains of 3% and/or 5% were used to form the data base.

ANA unlined cartons show a significant increase in relaxation modulus (Figures 6-1 and 6-2). ANB unlined cartons do not show a significant change at 10 sec. but do at 1000 sec. (Figures 6-3 and 6-4). ANT unlined cartons do not show a significant change.

When ANA and ANB unlined cartons are combined, there is no significant change (Figures 6-5 and 6-6).

There is no significant change for ANB lined cartons. There is a significant increase in relaxation modulus for ANT lined cartons (Figures 6-7 and 6-8). When all ANB is combined there is a significant increase in relaxation modulus (Figures 6-9 and 6-10). The increase in relaxation modulus is consistent with the increase in uniaxial tensile modulus and 10 sec hardness exhibited by this propellant.

Master stress relaxation curves include lined and unlined cartons. The curves are shown in Figures 6-11, 6-12 and 6-13. There is better agreement between ANB and ANT than between ANB and ANA. At lower test temperatures differences are accentuated.



Gradient stress relaxation was run on mini-stress relaxation specimens (0.1 x 0.5 x 2" specimens) at 1% strain and 77°F. Minimum stress relaxation modulus is reached at 2.2 inches from the bond line (Figures 6-14 and 6-15). It is apparent from the graphs that there is a sharp drop in modulus between the first and second specimens. Several cartons had liner which penetrated several samples which caused much disparity in the data.

$Y = ((-6.317270E+01) + (1.2525010E+01) * X)$   
 F = +1.2202670E+01 SIGNIFICANCE OF F = SIGNIFICANT  $G_1 = +1.8875880E+02$   
 R = +5.5093453E-01 SIGNIFICANCE OF R = SIGNIFICANT  $S_1 = +3.5855075E+00$   
 t = +3.4932321E+00 SIGNIFICANCE OF t = SIGNIFICANT  $S_t = +1.6031669E+02$   
 N = 30 DEGREES OF FREEDOM = 28  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

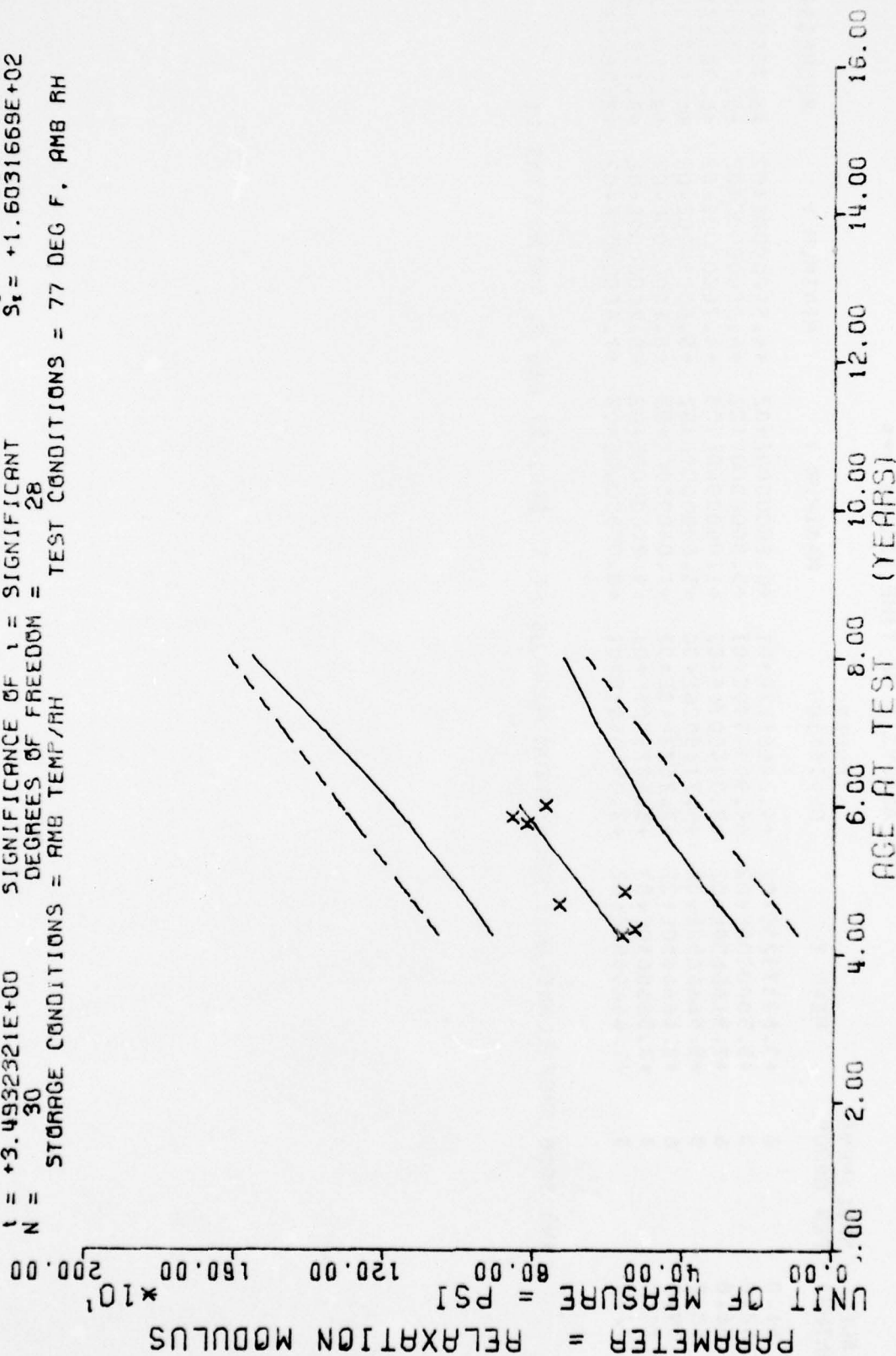


Figure 6-1

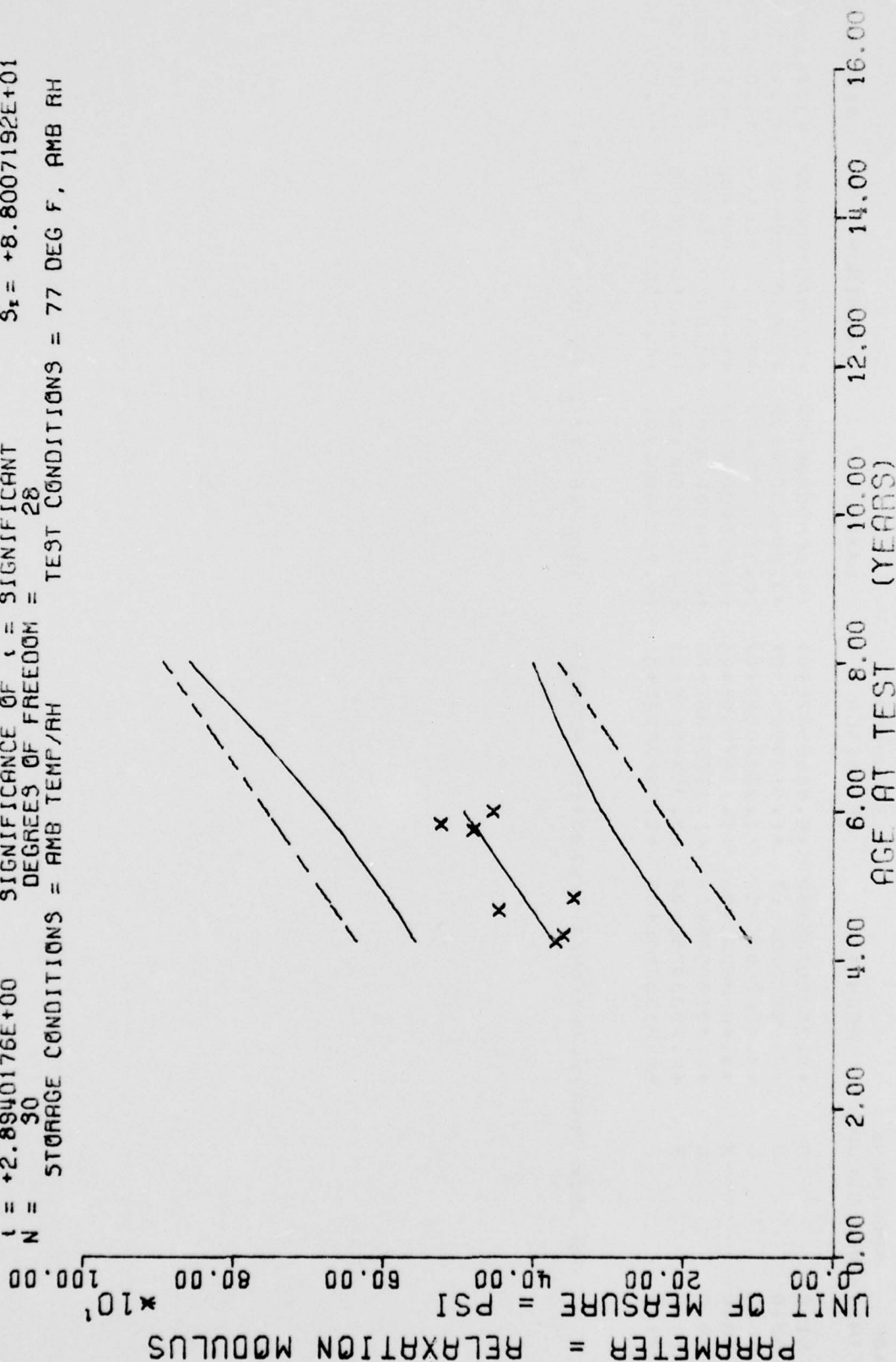
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
51.0	6	+5.6333325E+02	+9.2448183E+01	+6.8000000E+02	+4.5000000E+02	+5.7559814E+02
52.0	3	+5.3000000E+02	+4.9999999E+01	+5.8000000E+02	+4.8000000E+02	+5.8812304E+02
56.0	6	+7.3166650E+02	+2.3945076E+02	+1.0400000E+03	+4.7000000E+02	+6.3822314E+02
58.0	3	+5.5666650E+02	+5.7735026E+00	+5.6000000E+02	+5.5000000E+02	+6.6327319E+02
69.0	6	+8.1666650E+02	+2.2677448E+02	+1.0400000E+03	+6.1000000E+02	+8.0104833E+02
70.0	3	+8.5666650E+02	+5.5075705E+01	+9.2000000E+02	+8.2000000E+02	+8.1357324E+02
72.0	3	+7.6666650E+02	+3.0550504E+01	+8.0000000E+02	+7.4000000E+02	+8.3862329E+02

ANB 3066 PROPELLANT(ANA) RELAXATION MODULUS AT 10 SEC, 77 DEG F, UNLND CYNs 18

$Y = ((+8.3611444E+01) + (+5.6962785E+00) \times X)$   
 $F = +8.3753379E+00$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = +4.7984132E-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +2.8940176E+00$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 30$  DEGREES OF FREEDOM = 28  
 STORAGE CONDITIONS = AMB TEMP/AH TEST CONDITIONS = 77 DEG F, AMB RH



ANB 3066 PROPELLANT (ANA) RELAXATION MODULUS AT 1000 SEC 77 DEG F UNLND CTNS 1X

Figure 6-2



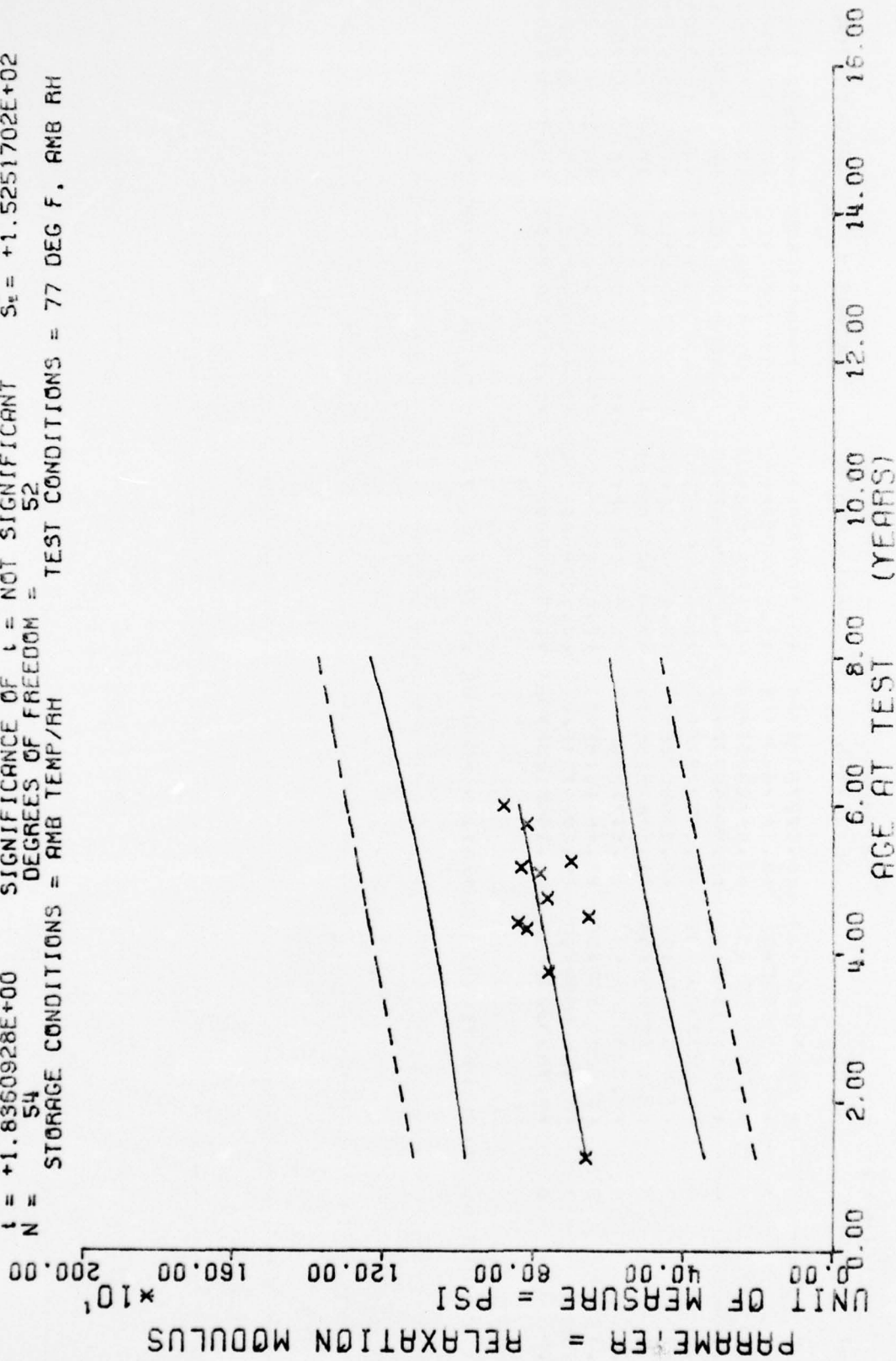
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
51.0	6	+3.700000E+02	+5.6568542E+01	+4.4000000E+02	+3.1000000E+02	+3.7412158E+02
52.0	3	+3.600000E+02	+1.9592999E+01	+3.8000000E+02	+3.4000000E+02	+3.7981787E+02
56.0	6	+4.4666650E+02	+1.2242004E+02	+6.1000000E+02	+3.1000000E+02	+4.0260302E+02
58.0	3	+3.4666650E+02	+1.1547005E+01	+3.6000000E+02	+3.4000000E+02	+4.1399536E+02
69.0	6	+4.800000E+02	+1.3175735E+02	+6.1000000E+02	+3.5000000E+02	+4.7665454E+02
70.0	3	+5.2333325E+02	+2.3094010E+01	+5.5000000E+02	+5.1000000E+02	+4.8235083E+02
72.0	7	+4.5333325E+02	+1.5275252E+01	+4.7000000E+02	+4.4000000E+02	+4.5374340E+02

AND 3066 PROPELLANT(ANA) RELAXATION MODULUS AT 1000 SEC 77 DEG F UNLND CTNS 1X

$F = +3.3712370E+00$   
 $R = +2.4674737E-01$   
 $t = +1.8360928E+00$   
 $N = 54$   
 STORAGE CONDITIONS = AMB TEMP/RH  
 DEGREES OF FREEDOM = 52  
 $Y = ((+6.1544231E+02) + (+3.1055993E+00) * X)$   
 SIGNIFICANCE OF F = NOT SIGNIFICANT  
 SIGNIFICANCE OF R = NOT SIGNIFICANT  
 SIGNIFICANCE OF t = NOT SIGNIFICANT  
 $\alpha = +1.5589152E+02$   
 $S_e = +1.6914173E+00$   
 $S_t = +1.5251702E+02$   
 TEST CONDITIONS = 77 DEG F, AMB RH



AMB 3066 PROPELLANT (AMB) RELAXATION MODULUS AT 10 SEC, 77 DEG F, UNLND CINS 1X

Figure 6-3

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+6.600000E+02	+6.0827625E+01	+7.3600000E+02	+5.2000000E+02	+6.6202612E+02
45.0	3	+7.6000000E+02	+5.5677643E+01	+8.1000000E+02	+7.0000000E+02	+7.5519409E+02
52.0	9	+8.1666650E+02	+1.5570385E+02	+1.1700000E+03	+4.9000000E+02	+7.7693334E+02
53.0	9	+8.411108E+02	+1.5855877E+02	+1.0400000E+03	+6.4000000E+02	+7.6003906E+02
54.0	6	+6.5333325E+02	+1.1552777E+02	+8.0000000E+02	+5.4000000E+02	+7.8314453E+02
57.0	3	+7.6333325E+02	+6.8068592E+01	+8.4000000E+02	+7.1000000E+02	+7.5246142E+02
61.0	3	+7.8333325E+02	+1.1547005E+01	+7.9000000E+02	+7.7000000E+02	+8.0488378E+02
62.0	6	+8.3333325E+02	+2.5271855E+02	+1.0900000E+03	+6.0000000E+02	+8.0798925E+02
63.0	3	+7.0000000E+02	+3.4641016E+01	+7.4000000E+02	+6.8000000E+02	+8.1109497E+02
69.0	3	+8.1666650E+02	+8.6216781E+01	+9.1000000E+02	+7.4000000E+02	+8.2972851E+02
72.0	6	+8.7833325E+02	+1.1540128E+02	+1.0100000E+03	+7.1000000E+02	+8.3904541E+02

AND 3065 PROPELLANT(AN3) RELAXATION MODULUS AT 10 SEC, 77 DEG F, UNLND CINS 1%

$F = +4.1675817E+00$  SIGNIFICANCE OF F =  $(+3.6913866E+02)$  +  $(+2.1200505E+00)$  \* X)  
 $R = +2.7239504E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $G_1 = +9.6399906E+01$   
 $t = +2.0414655E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_1 = +1.0384943E+00$   
 $N = 54$  DEGREES OF FREEDOM = 52  $S_2 = +9.3642216E+01$   
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

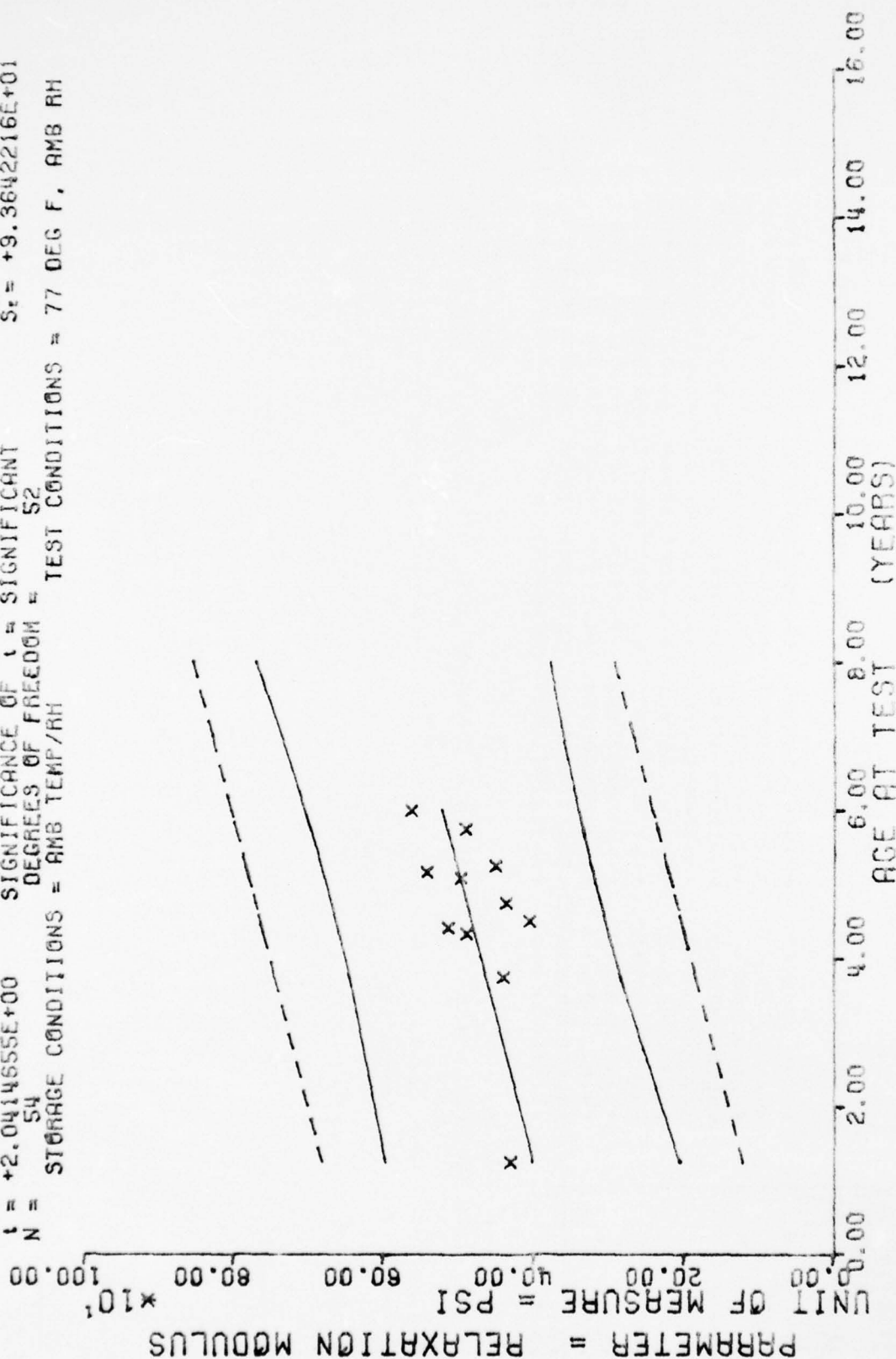


Figure 6-4



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

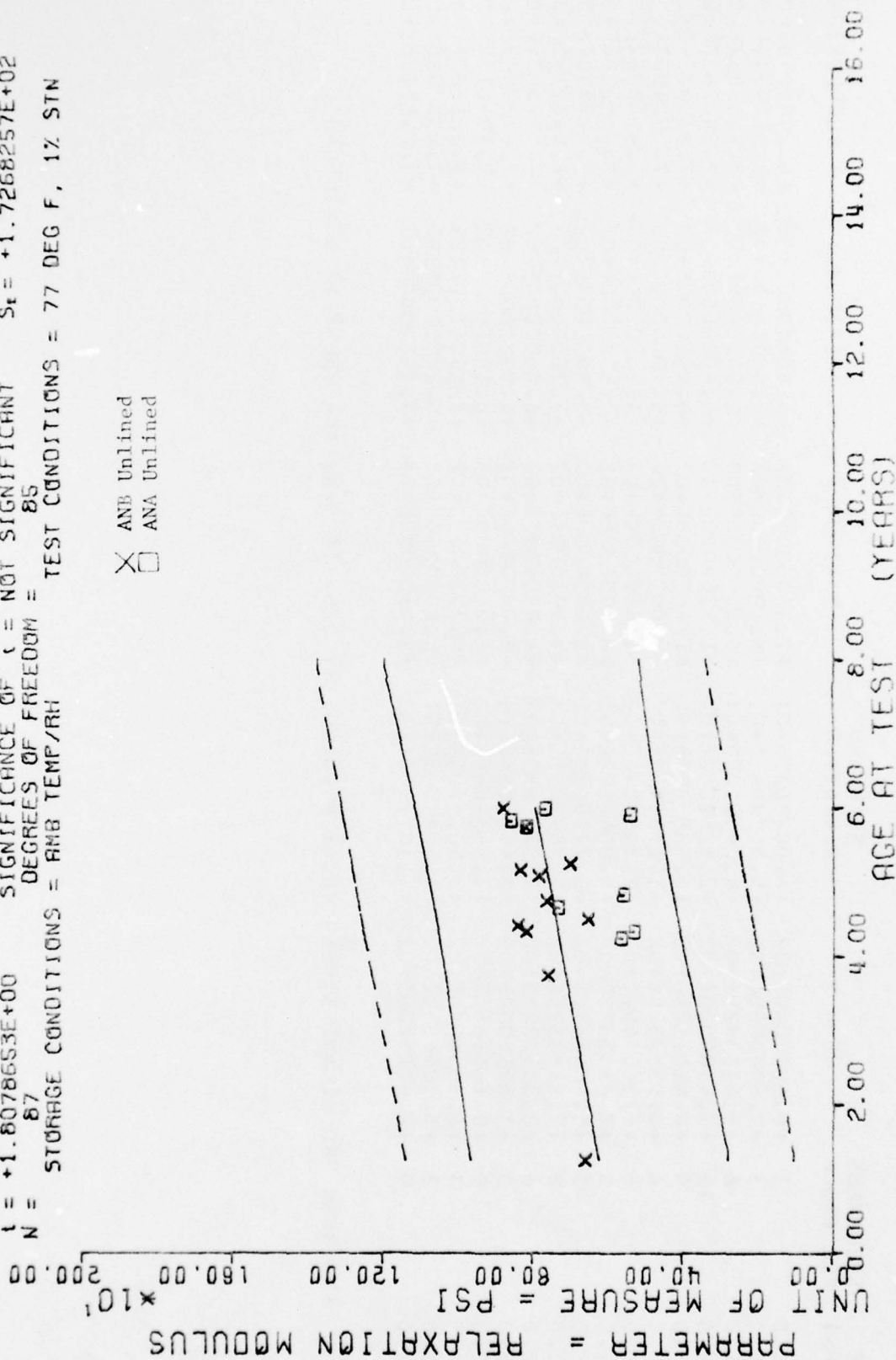
\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+4.300000E+02	+3.464101E+01	+4.700000E+02	+4.100000E+02	+4.0093920E+02
45.0	3	+4.400000E+02	+2.567513E+01	+4.600000E+02	+4.100000E+02	+4.6454077E+02
52.0	9	+4.680000E+02	+1.163807E+02	+6.500000E+02	+2.800000E+02	+4.7938110E+02
53.0	0	+5.1323325E+02	+9.1651913E+01	+6.300000E+02	+3.700000E+02	+4.8159122E+02
54.0	6	+4.050000E+02	+4.7644516E+01	+4.700000E+02	+3.600000E+02	+4.8362133E+02
57.0	3	+4.3666650E+02	+4.7258150E+01	+4.900000E+02	+4.000000E+02	+4.8958144E+02
61.0	4	+4.9666650E+02	+1.5278252E+01	+5.100000E+02	+4.800000E+02	+4.9846166E+02
62.0	0	+5.4166650E+02	+1.7803557E+02	+7.200000E+02	+3.800000E+02	+5.0056178E+02
63.0	3	+4.500000E+02	+1.7220508E+01	+4.600000E+02	+4.300000E+02	+5.0270166E+02
69.0	3	+4.500000E+02	+6.0827625E+01	+5.600000E+02	+4.500000E+02	+5.1342211E+02
72.0	6	+5.6166650E+02	+2.4832774E+01	+5.900000E+02	+5.400000E+02	+5.2176222E+02

AGE 30.60 PRECIPITANT(AMB) RELAXATION MODULUS AT 1000 SEC 77 DEG F UNLNE CYS 1%

$F = +3.2683769E+00$  SIGNIFICANCE OF F =  $(+5.7564219E+02)$  +  $(+2.9612427E+00)$  \* XJ  
 $R = +1.9242588E-01$  SIGNIFICANCE OF R = NOT SIGNIFICANT  $G_1 = +1.7494513E+02$   
 $t = +1.8078653E+00$  SIGNIFICANCE OF t = NOT SIGNIFICANT  $S_2 = +1.6379775E+00$   
 $N = 87$  DEGREES OF FREEDOM = 85  $S_t = +1.7268257E+02$   
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, 1% STN

X ANB Unlined  
 □ ANA Unlined



ANB 3066 PROPELLANT STRESS RELAX MODULUS, 77 DEG, 1% STN, ANA UNLND VS ANB UNLND  
 10 Sec

Figure 6-5

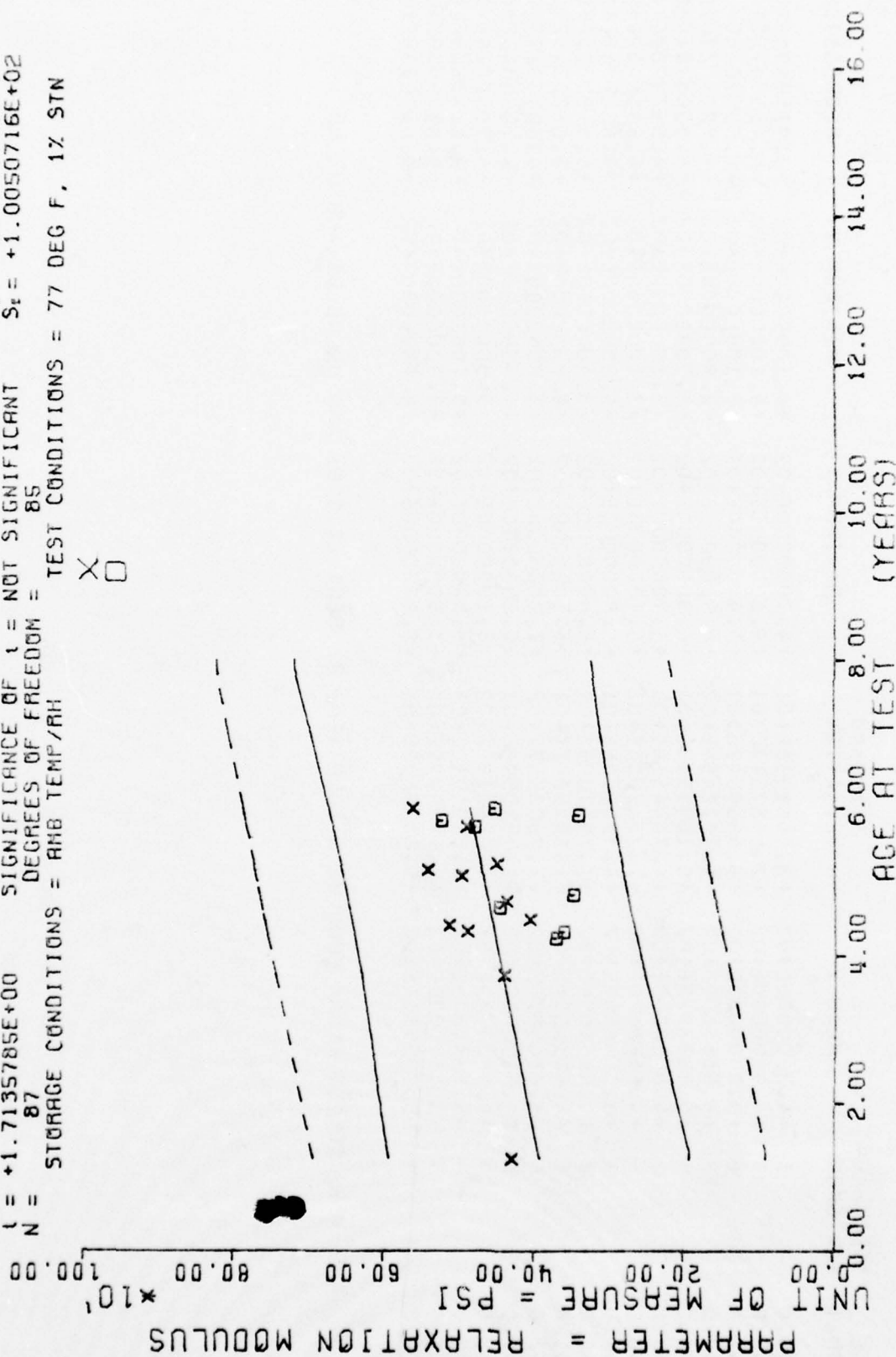
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+6.600000E+02	+6.0827625E+01	+7.3000000E+02	+6.2000000E+02	+6.2006079E+02
45.0	3	+7.6000000E+02	+5.5677643E+01	+8.1000000E+02	+7.0000000E+02	+7.0889794E+02
51.0	6	+5.6333325E+02	+9.2448183E+01	+6.8000000E+02	+4.5000000E+02	+7.2666552E+02
52.0	12	+7.4500000E+02	+2.1241040E+02	+1.1700000E+03	+4.8000000E+02	+7.2962670E+02
53.0	9	+8.4111108E+02	+1.5885877E+02	+1.0400000E+03	+6.4000000E+02	+7.3258789E+02
54.0	6	+6.5333325E+02	+1.1552777E+02	+8.0000000E+02	+5.4000000E+02	+7.3554907E+02
56.0	6	+7.3166650E+02	+2.3945076E+02	+1.0400000E+03	+4.7000000E+02	+7.4147167E+02
57.0	3	+7.6333325E+02	+6.8068592E+01	+8.4000000E+02	+7.1000000E+02	+7.4443286E+02
58.0	3	+5.5666650E+02	+5.7735026E+00	+5.6000000E+02	+5.5000000E+02	+7.4739404E+02
61.0	3	+7.8333325E+02	+1.1547005E+01	+7.9000000E+02	+7.7000000E+02	+7.5627783E+02
62.0	6	+8.3333325E+02	+2.5271855E+02	+1.0900000E+03	+6.0000000E+02	+7.5923901E+02
63.0	3	+7.0000000E+02	+3.4641016E+01	+7.4000000E+02	+6.8000000E+02	+7.6220043E+02
69.0	9	+8.1666650E+02	+1.8439088E+02	+1.0400000E+03	+6.1000000E+02	+7.7996777E+02
70.0	3	+8.5666650E+02	+5.5075705E+01	+9.2000000E+02	+8.2000000E+02	+7.8292895E+02
71.0	3	+5.3666650E+02	+1.1547005E+01	+5.5000000E+02	+5.3000000E+02	+7.8589038E+02
72.0	9	+8.4111108E+02	+1.1072990E+02	+1.0100000E+03	+7.1000000E+02	+7.8885156E+02

ANB 3066 PROPELLANT STRESS RELAX MODULUS, 77 DEG, 1% STN, ANA UNLND VS ANB UNLND

$\gamma = (1 + 3.6708023E+02) + (1.6336553E+00) * X$   
 $F = +2.9363514E+00$  SIGNIFICANCE OF F = NOT SIGNIFICANT  $G = +1.0163235E+02$   
 $R = +1.8273418E-01$  SIGNIFICANCE OF R = NOT SIGNIFICANT  $S = +9.5335890E-01$   
 $L = +1.7135785E+00$  SIGNIFICANCE OF L = NOT SIGNIFICANT  $S_t = +1.0050716E+02$   
 $N = 87$  DEGREES OF FREEDOM = 85  
 STORAGE CONDITIONS = ANB TEMP/RH TEST CONDITIONS = 77 DEG F, 1% STN



ANB 3066 STRESS RELAX MODULUS @ 1000 SEC, 77 DEG, 1% STN, ANB UNLND VS ANB UNLND

Figure 6-6



\*\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	3	+4.3000000E+02	+3.4641016E+01	+4.7000000E+02	+4.1000000E+02	+3.9158496E+02
45.0	3	+4.4000000E+02	+2.6457513E+01	+4.6000000E+02	+4.1000000E+02	+4.4059472E+02
51.0	6	+3.7000000E+02	+5.6568542E+01	+4.4000000E+02	+3.1000000E+02	+4.5039648E+02
52.0	12	+4.5666650E+02	+1.1578454E+02	+6.9000000E+02	+2.8000000E+02	+4.5203027E+02
53.0	9	+5.1333325E+02	+9.1651513E+01	+6.3000000E+02	+3.7000000E+02	+4.5366381E+02
54.0	6	+4.0500000E+02	+4.7644516E+01	+4.7000000E+02	+3.6000000E+02	+4.5529760E+02
56.0	6	+4.4666650E+02	+1.2242004E+02	+6.1000000E+02	+3.1000000E+02	+4.5856469E+02
57.0	3	+4.3666650E+02	+4.7258156E+01	+4.9000000E+02	+4.0000000E+02	+4.6019848E+02
58.0	3	+3.4666650E+02	+1.1547005E+01	+3.6000000E+02	+3.4000000E+02	+4.6183203E+02
61.0	3	+4.9666650E+02	+1.5275252E+01	+5.1000000E+02	+4.8000000E+02	+4.6673315E+02
62.0	6	+5.4166650E+02	+1.7803557E+02	+7.2000000E+02	+3.8000000E+02	+4.6836669E+02
63.0	3	+4.5000000E+02	+1.7320508E+01	+4.6000000E+02	+4.3000000E+02	+4.7000048E+02
69.0	9	+4.8333325E+02	+1.0862780E+02	+6.1000000E+02	+3.5000000E+02	+4.7980224E+02
70.0	3	+5.2333325E+02	+2.3094010E+01	+5.5000000E+02	+5.1000000E+02	+4.8143603E+02
71.0	3	+3.4000000E+02	+9.9999999E+00	+3.5000000E+02	+3.3000000E+02	+4.8306958E+02
72.0	9	+5.2555541E+02	+5.8118652E+01	+5.9000000E+02	+4.4000000E+02	+4.8470336E+02

ANB 3066 STRESS RELAX MODULUS @ 1000 SEC, 77 DEG; 1% STN, ANA UNLND VS ANB UNLND

$Y = (1 + 4.6438564E+02) + (1 + 7.5895256E+00) \times X1$   
 $F = +1.9043898E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G_1 = +1.2304944E+02$   
 $R = +5.0714632E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_0 = +1.7391486E+00$   
 $t = +4.9639314E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_1 = +1.0701114E+02$   
 $N = 57$  DEGREES OF FREEDOM = 55  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

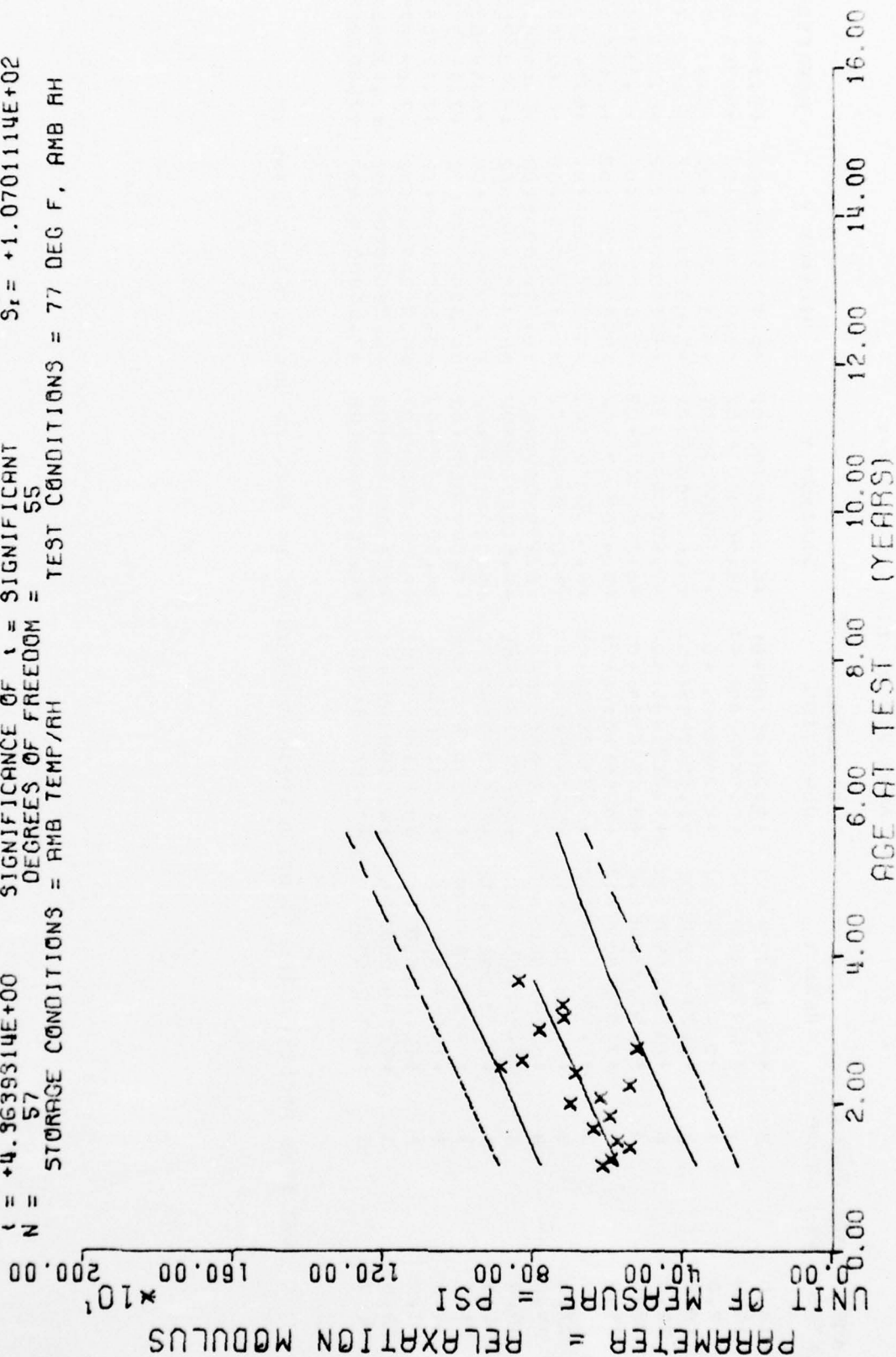


Figure 6-7

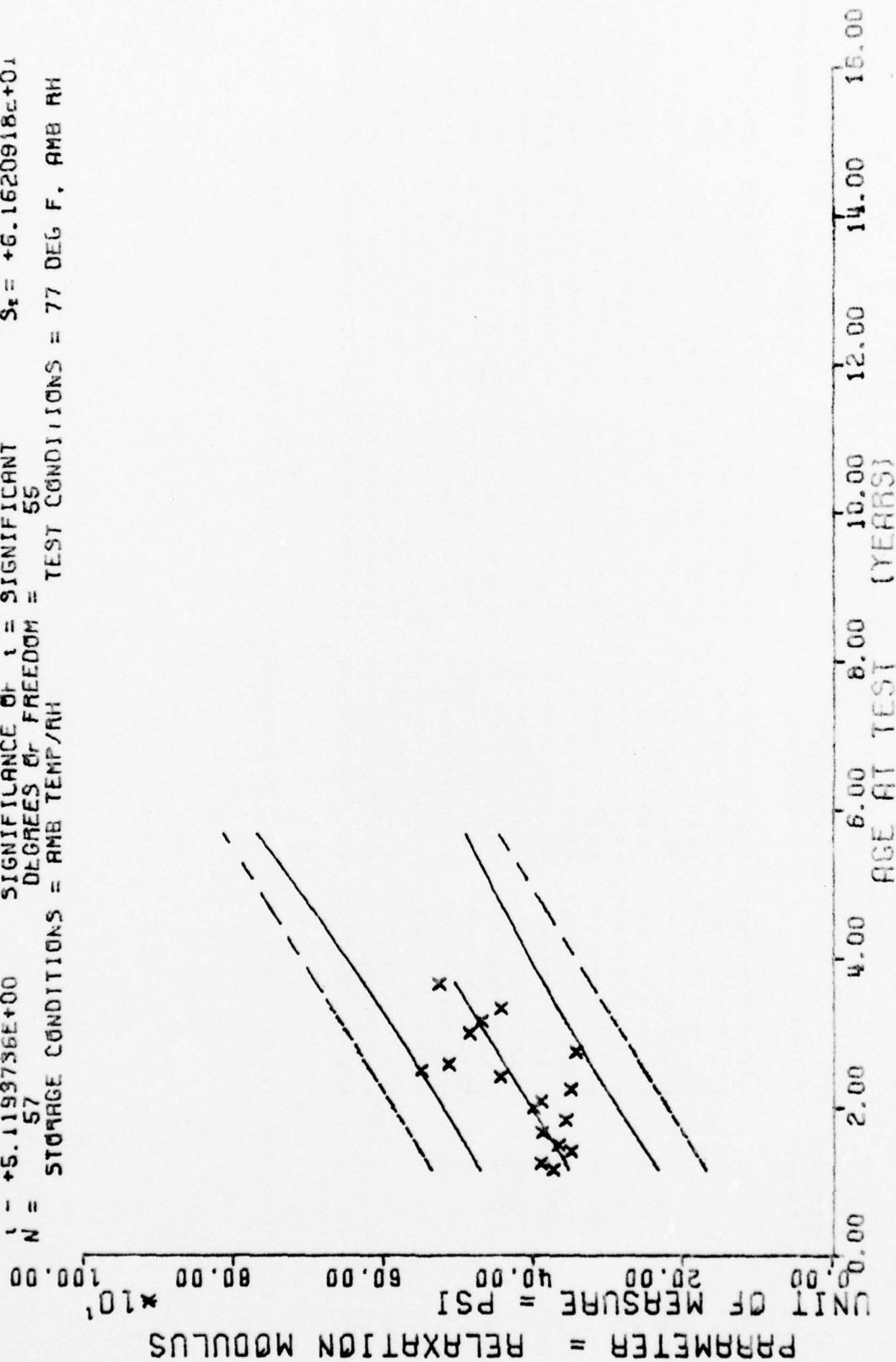
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
14.0	3	+5.1333325E+02	+4.0414518E+01	+6.5000000E+02	+5.7000000E+02	+5.7063851E+02
15.0	1	+5.9000000E+02	+0.0000000E+02	+5.9000000E+02	+5.9000000E+02	+5.7822851E+02
17.0	3	+5.4000000E+02	+4.3588589E+01	+5.9000000E+02	+5.1000000E+02	+5.5340747E+02
18.0	3	+5.7333325E+02	+1.1547005E+01	+5.8000000E+02	+5.6000000E+02	+6.0099707E+02
20.0	6	+6.3666650E+02	+1.2027745E+02	+7.5000000E+02	+5.1000000E+02	+6.1617602E+02
22.0	3	+5.9333325E+02	+3.0550504E+01	+6.2000000E+02	+5.6000000E+02	+6.3135458E+02
24.0	3	+7.0000000E+02	+3.4641016E+01	+7.4000000E+02	+5.8000000E+02	+6.4653417E+02
25.0	3	+5.2000000E+02	+4.3588589E+01	+6.5000000E+02	+5.7000000E+02	+6.5412377E+02
27.0	3	+5.4333325E+02	+5.7735026E+00	+5.5000000E+02	+5.4000000E+02	+6.6930273E+02
29.0	8	+6.8525000E+02	+1.0568653E+02	+8.2000000E+02	+5.3000000E+02	+6.8448168E+02
30.0	3	+8.8666650E+02	+6.0277137E+01	+9.5000000E+02	+8.3000000E+02	+6.9207128E+02
31.0	3	+8.3000000E+02	+6.5574385E+01	+9.0000000E+02	+7.7000000E+02	+6.9966038E+02
33.0	3	+5.2333325E+02	+1.5207950E+02	+7.0000000E+02	+4.3000000E+02	+7.1493984E+02
36.0	3	+7.8333325E+02	+3.5118845E+01	+8.2000000E+02	+7.5000000E+02	+7.3760835E+02
38.0	3	+7.1666650E+02	+3.5118845E+01	+7.5000000E+02	+6.8000000E+02	+7.5278759E+02
40.0	3	+7.2000000E+02	+4.9599999E+01	+7.7000000E+02	+6.7000000E+02	+7.6796655E+02
44.0	3	+8.3666650E+02	+7.7674534E+01	+9.0000000E+02	+7.5000000E+02	+7.9832470E+02

AND 3066 PROPELLANT(ANT) RELAXATION MODULUS AT 10 SEC, 77 DEG F, LINED CINS 1%

$Y = ((+2.8090470E+02) + (+5.1268743E+00) * X)$   
 $F = +2.6207986E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $G = +7.4205060E+01$   
 $R = +5.6808041E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +1.0014651E+00$   
 $t = +5.1193736E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_t = +6.1620918E+01$   
 $N = 57$  DEGREES OF FREEDOM = 55  
 STORAGE CONDITIONS = AMB TEMP/AM TEST CONDITIONS = 77 DEG F, AMB RH



AMS 3066 PROPELLANT (ANT) RELAXATION MODULUS AT 1000 SEC, 77 DEG F, LND CTNS 1X



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF THE SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
14.0	3	+7.7333333E+02	+3.0550504E+01	+4.0000000E+02	+2.4000000E+02	+3.5263000E+02
15.0	1	+4.0000000E+02	+0.0000000E+00	+3.0000000E+02	+3.0000000E+02	+3.5740761E+02
17.0	3	+3.5000000E+02	+2.0000000E+01	+3.5000000E+02	+2.0000000E+02	+3.5906152E+02
18.0	3	+3.6566666E+02	+5.7235026E+00	+3.7000000E+02	+3.6000000E+02	+3.7318823E+02
20.0	6	+3.8973325E+02	+4.4007675E+01	+4.4000000E+02	+3.4000000E+02	+3.8344217E+02
22.0	3	+3.5866666E+02	+1.5275252E+01	+3.7000000E+02	+3.4000000E+02	+3.9360580E+02
24.0	3	+4.0000000E+02	+1.0000000E+01	+4.0000000E+02	+3.8000000E+02	+4.0304246E+02
25.0	3	+3.6000000E+02	+2.6457513E+01	+4.1000000E+02	+3.6000000E+02	+4.007641E+02
27.0	3	+3.5000000E+02	+0.0000000E+00	+3.5000000E+02	+3.5000000E+02	+4.1033007E+02
29.0	3	+4.0375000E+02	+6.9680392E+01	+5.0000000E+02	+3.5000000E+02	+4.2058398E+02
30.0	3	+5.5000000E+02	+2.0999999E+01	+5.8000000E+02	+5.2000000E+02	+4.3471093E+02
31.0	3	+5.1333325E+02	+4.5002407E+01	+5.6000000E+02	+4.7000000E+02	+4.7983764E+02
33.0	3	+2.4333333E+02	+1.0115093E+02	+4.0000000E+02	+2.8000000E+02	+4.5009155E+02
35.0	3	+4.5666666E+02	+2.5156114E+01	+5.1000000E+02	+4.6000000E+02	+4.6547216E+02
37.0	3	+4.7000000E+02	+1.0900000E+01	+4.9000000E+02	+4.6000000E+02	+4.7572587E+02
40.0	2	+4.0333325E+02	+3.0550504E+01	+4.7000000E+02	+4.1000000E+02	+4.8597940E+02
44.0	3	+5.2666666E+02	+5.1316014E+01	+5.7000000E+02	+4.7000000E+02	+5.0648706E+02

AGE 30.66 DOUBLE ANT(ANT) RELAXATION MODULUS AT 1000 SEC. 77 DEG F. 1ND CTNS 1%

$F = +2.0907284E+01$   
 $R = +2.8253680E-01$   
 $t = +4.5724484E+00$   
 $N = 243$   
 $Y = (1 + 6.0808140E+02) + (1.7436554E+00) * X$   
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM = 241  
 STORAGE CONDITIONS = AMB TEMP/RH  
 TEST CONDITIONS = 77 DEG F, AMB RH

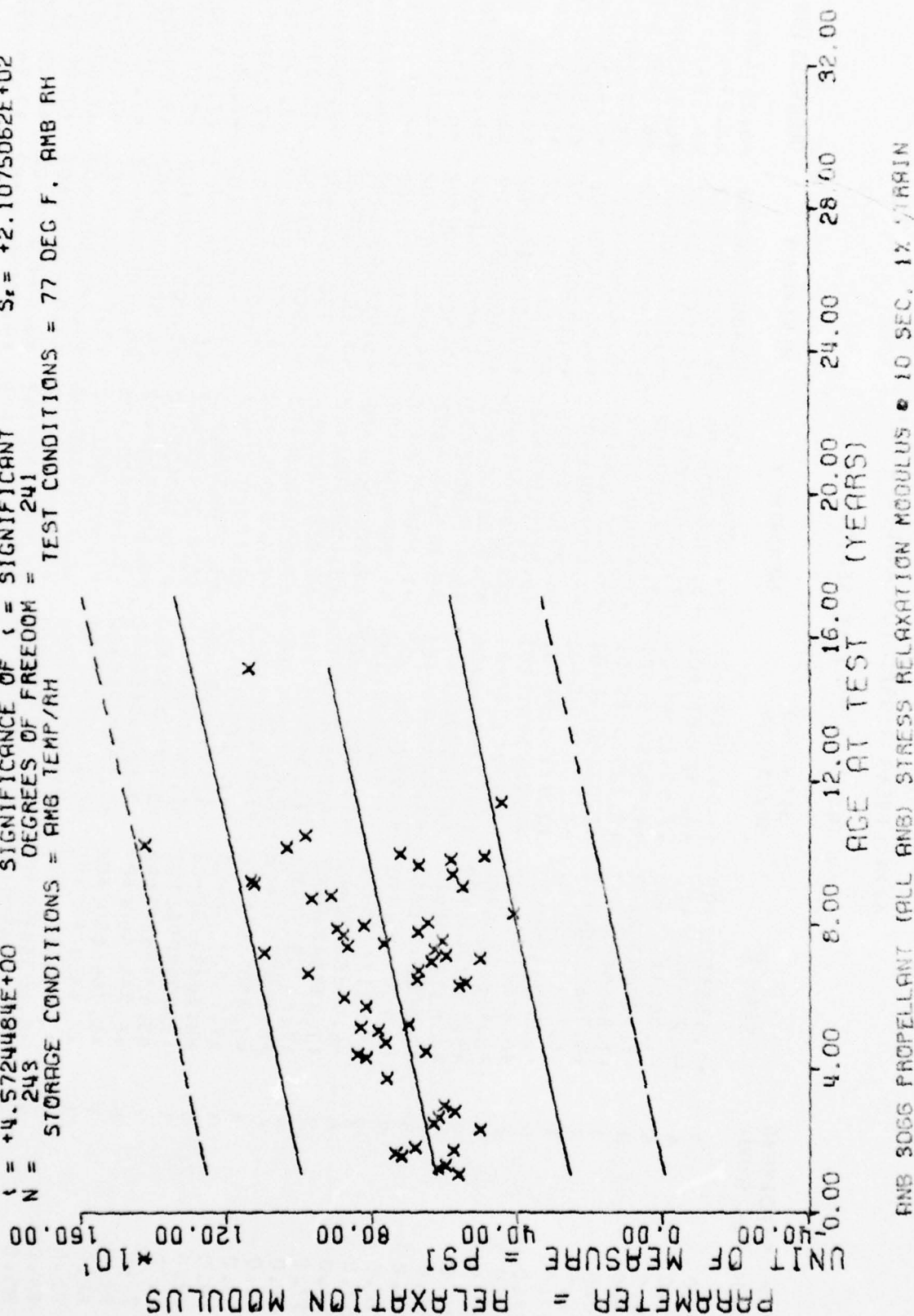


Figure 6-9

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	3	+5.5333325E+02	+4.1633319E+01	+6.1000000E+02	+5.3000000E+02	+6.2574877E+02
15.0	6	+6.2000000E+02	+5.9329587E+01	+7.3000000E+02	+5.7000000E+02	+6.2923608E+02
16.0	6	+5.98333325E+02	+7.9351533E+01	+7.0000000E+02	+5.1000000E+02	+6.3097973E+02
19.0	3	+7.2000000E+02	+4.5825756E+01	+7.7000000E+02	+6.8000000E+02	+6.3621069E+02
20.0	3	+7.3666650E+02	+3.7859388E+01	+7.8000000E+02	+7.1000000E+02	+6.3795434E+02
21.0	3	+5.7666650E+02	+2.0816659E+01	+6.0000000E+02	+5.6000000E+02	+6.3969799E+02
22.0	3	+6.2333325E+02	+2.0816659E+01	+7.0000000E+02	+6.6000000E+02	+6.4144165E+02
28.0	6	+5.0333325E+02	+7.7373552E+01	+6.2000000E+02	+4.1000000E+02	+6.5190356E+02
30.0	6	+6.3166650E+02	+4.7081489E+01	+6.9000000E+02	+5.7000000E+02	+6.5539086E+02
32.0	6	+6.1666650E+02	+7.3120904E+01	+7.2000000E+02	+5.1000000E+02	+6.5887817E+02
34.0	3	+5.7333325E+02	+1.5275252E+01	+5.9000000E+02	+5.6000000E+02	+6.6236547E+02
36.0	3	+6.0333325E+02	+8.0208062E+01	+6.8000000E+02	+5.2000000E+02	+6.6585278E+02
45.0	3	+7.6000000E+02	+5.5677643E+01	+8.1000000E+02	+7.0000000E+02	+6.8154589E+02
52.0	9	+8.1666650E+02	+1.9570395E+02	+1.1700000E+03	+4.9000000E+02	+6.9375146E+02
53.0	9	+8.4111108E+02	+1.5885377E+02	+1.0400000E+03	+6.4000000E+02	+6.9549511E+02
54.0	6	+6.5333325E+02	+1.1552777E+02	+8.0000000E+02	+5.4000000E+02	+6.5723876E+02
57.0	3	+7.6333325E+02	+6.8068592E+01	+8.4000000E+02	+7.1000000E+02	+7.0246972E+02
61.0	3	+7.8333325E+02	+1.1547005E+01	+7.9000000E+02	+7.7000000E+02	+7.0944433E+02
62.0	6	+8.3333325E+02	+2.5271855E+02	+1.0900000E+03	+6.0000000E+02	+7.1118798E+02
63.0	3	+7.0000000E+02	+3.4641016E+01	+7.4000000E+02	+6.8000000E+02	+7.1293164E+02
69.0	3	+8.1666650E+02	+3.6216781E+01	+9.1000000E+02	+7.4000000E+02	+7.2339355E+02
72.0	6	+8.7833325E+02	+1.1940128E+02	+1.0100000E+03	+7.1000000E+02	+7.2862451E+02
76.0	3	+5.6000000E+02	+1.9999999E+01	+5.8000000E+02	+5.4000000E+02	+7.3559912E+02
77.0	3	+5.4333325E+02	+5.7735026E+00	+5.5000000E+02	+5.4000000E+02	+7.3734277E+02
78.0	6	+6.7666650E+02	+2.0655911E+01	+7.1000000E+02	+6.5000000E+02	+7.3908642E+02
80.0	3	+9.7666650E+02	+1.1590225E+02	+1.1100000E+03	+9.0000000E+02	+7.4257373E+02
81.0	3	+6.7333325E+02	+8.1445278E+01	+7.3000000E+02	+5.9000000E+02	+7.4431738E+02
84.0	3	+6.3666650E+02	+3.0550504E+01	+6.7000000E+02	+6.1000000E+02	+7.4954833E+02
85.0	3	+5.0333325E+02	+2.3094010E+01	+5.3000000E+02	+4.9000000E+02	+7.5129199E+02
86.0	3	+5.9666650E+02	+5.5075705E+01	+6.5000000E+02	+5.4000000E+02	+7.5303564E+02
87.0	3	+1.0966665E+03	+1.6072751E+02	+1.2800000E+03	+9.8000000E+02	+7.5477929E+02

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

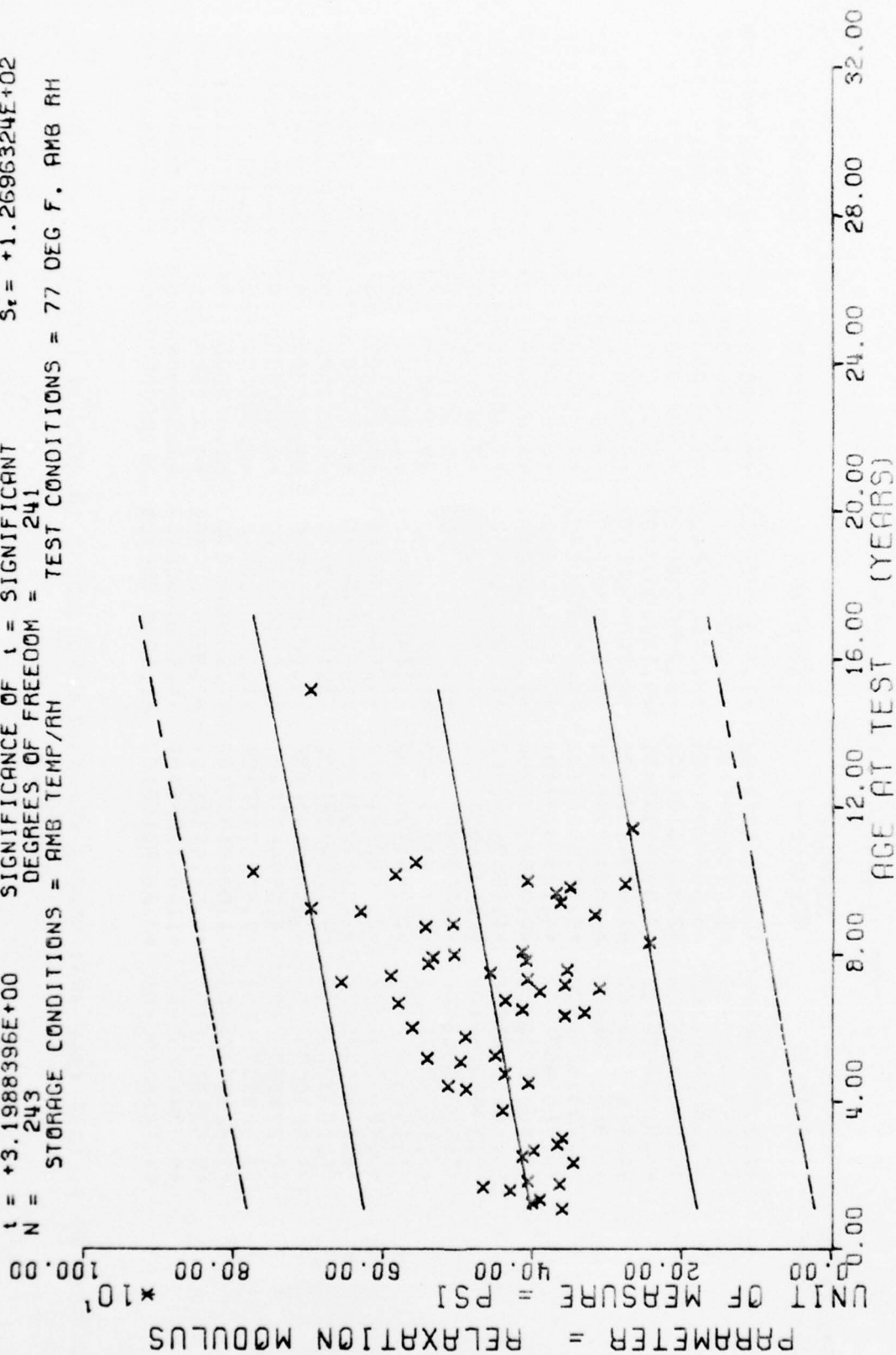
\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
88.0	9	+6.2777758E+02	+2.3215177E+02	+1.1300000E+03	+4.6000000E+02	+7.5652294E+02
89.0	6	+8.6833325E+02	+1.0796604E+02	+9.9000000E+02	+7.0000000E+02	+7.5826660E+02
90.0	3	+7.6666650E+02	+5.5075705E+01	+8.3000000E+02	+7.3000000E+02	+7.6001025E+02
91.0	3	+6.0666650E+02	+2.3094010E+01	+6.2000000E+02	+5.8000000E+02	+7.6175390E+02
93.0	3	+8.8000000E+02	+2.9999999E+01	+9.1000000E+02	+8.5000000E+02	+7.6524121E+02
94.0	9	+6.7444433E+02	+1.0794803E+02	+8.1000000E+02	+5.2000000E+02	+7.6698486E+02
95.0	3	+8.9666650E+02	+5.0332229E+01	+9.5000000E+02	+8.5000000E+02	+7.6872851E+02
96.0	6	+8.2333325E+02	+3.5023801E+01	+8.7000000E+02	+7.7000000E+02	+7.7047216E+02
97.0	3	+6.4666650E+02	+4.163319E+01	+6.8000000E+02	+6.0000000E+02	+7.7221582E+02
100.0	3	+4.1000000E+02	+9.999999E+00	+4.2000000E+02	+4.0000000E+02	+7.7744677E+02
105.0	6	+9.6666650E+02	+1.9469634E+02	+1.2000000E+03	+7.1000000E+02	+7.8616503E+02
106.0	3	+9.1333325E+02	+2.1221058E+02	+1.1500000E+03	+7.4000000E+02	+7.8790869E+02
109.0	3	+5.5000000E+02	+0.000000E+02	+5.5000000E+02	+5.5000000E+02	+7.9313964E+02
110.0	3	+1.1233332E+03	+1.7387735E+02	+1.3200000E+03	+9.9000000E+02	+7.9488330E+02
111.0	6	+1.1316665E+03	+1.7904375E+02	+1.4300000E+03	+9.3000000E+02	+7.9662695E+02
113.0	12	+5.7833325E+02	+2.3482424E+02	+1.0000000E+03	+3.7000000E+02	+8.0011425E+02
116.0	6	+6.7166650E+02	+1.8411047E+02	+9.9000000E+02	+4.9000000E+02	+8.0534521E+02
118.0	3	+5.8333325E+02	+3.7859388E+01	+6.1000000E+02	+5.4000000E+02	+8.0883251E+02
119.0	3	+4.9000000E+02	+9.999999E+00	+5.0000000E+02	+4.8000000E+02	+8.1057617E+02
120.0	3	+7.2333325E+02	+5.8594652E+01	+7.9000000E+02	+6.8000000E+02	+8.1231982E+02
122.0	3	+1.0333332E+03	+7.5718777E+01	+1.1200000E+03	+9.8000000E+02	+8.1580737E+02
123.0	3	+1.4233332E+03	+1.0969655E+02	+1.5500000E+03	+1.3600000E+03	+8.1755102E+02
126.0	3	+9.8333325E+02	+4.0414518E+01	+1.0200000E+03	+9.4000000E+02	+8.2278198E+02
137.0	3	+4.4333325E+02	+1.1547005E+01	+4.5000000E+02	+4.3000000E+02	+8.4196215E+02
162.0	3	+1.1366665E+03	+2.2810816E+02	+1.4000000E+03	+1.0000000E+03	+9.2042651E+02

ANR 3046 PROPELLANT (ALL ANB) STRESS RELAXATION MODULUS @ 10 SEC, 1% STRAIN



$Y = ((+3.9373020E+02) + (+7.3487501E-01) * X)$   
 $F = +1.0232575E+01$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = +2.0181548E-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +3.1988396E+00$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 243$  DEGREES OF FREEDOM = 241  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F. AMB RH



ANB 3066 PROPELLANT (ALL ANB) STRESS RELAXATION MODULUS • 1000 SEC. 1% STRAIN

Figure 6-10

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	3	+3.600000E+02	+1.7320508E+01	+3.8000000E+02	+3.5000000E+02	+4.0328344E+02
15.0	6	+4.0000000E+02	+4.2895221E+01	+4.7000000E+02	+3.5000000E+02	+4.0475317E+02
16.0	6	+3.9000000E+02	+4.1472882E+01	+4.4000000E+02	+3.5000000E+02	+4.0548803E+02
19.0	3	+4.3000000E+02	+1.7320508E+01	+4.5000000E+02	+4.2000000E+02	+4.0769262E+02
20.0	3	+4.6666650E+02	+2.8867513E+01	+5.0000000E+02	+4.5000000E+02	+4.0842749E+02
21.0	3	+3.6333325E+02	+2.3094010E+01	+3.9000000E+02	+3.5000000E+02	+4.0916235E+02
22.0	3	+4.0666650E+02	+1.5275252E+01	+4.2000000E+02	+3.9000000E+02	+4.0989721E+02
28.0	6	+3.4500000E+02	+4.3243496E+01	+4.1000000E+02	+2.9000000E+02	+4.1430664E+02
30.0	6	+4.1333325E+02	+2.7325202E+01	+4.4000000E+02	+3.8000000E+02	+4.1577636E+02
32.0	6	+3.9833325E+02	+4.8751068E+01	+4.7000000E+02	+3.3000000E+02	+4.1724609E+02
34.0	3	+3.6666650E+02	+2.5166114E+01	+3.9000000E+02	+3.4000000E+02	+4.1871582E+02
36.0	3	+3.6000000E+02	+6.2449979E+01	+4.3000000E+02	+3.1000000E+02	+4.2018554E+02
45.0	3	+4.4000000E+02	+2.6457513E+01	+4.6000000E+02	+4.1000000E+02	+4.2679956E+02
52.0	3	+4.8888867E+02	+1.1689075E+02	+6.9000000E+02	+2.8000000E+02	+4.2194360E+02
53.0	3	+5.1333325E+02	+9.1651513E+01	+6.3000000E+02	+3.7000000E+02	+4.3267846E+02
54.0	6	+4.0500000E+02	+4.7644516E+01	+4.7000000E+02	+3.6000000E+02	+4.3341333E+02
57.0	3	+4.3666650E+02	+4.7258156E+01	+4.9000000E+02	+4.0000000E+02	+4.3561791E+02
61.0	3	+4.9666650E+02	+1.5275252E+01	+5.1000000E+02	+4.8000000E+02	+4.3855737E+02
62.0	6	+5.4166650E+02	+1.7803557E+02	+7.2000000E+02	+3.8000000E+02	+4.3929223E+02
63.0	3	+4.5000000E+02	+1.7320508E+01	+4.6000000E+02	+4.3000000E+02	+4.4002709E+02
69.0	3	+4.9000000E+02	+6.0827625E+01	+5.6000000E+02	+4.5000000E+02	+4.4443652E+02
72.0	6	+5.6166650E+02	+2.4832774E+01	+5.9000000E+02	+5.4000000E+02	+4.4664111E+02
76.0	3	+3.5666650E+02	+1.5275252E+01	+3.7000000E+02	+3.4000000E+02	+4.4958056E+02
77.0	3	+3.3000000E+02	+0.0000000E+95	+3.3000000E+02	+3.3000000E+02	+4.5031542E+02
78.0	6	+4.1333325E+02	+8.1649658E+00	+4.2000000E+02	+4.0000000E+02	+4.5105029E+02
80.0	3	+5.8000000E+02	+7.8102496E+01	+6.7000000E+02	+5.3000000E+02	+4.5252001E+02
81.0	3	+4.3666650E+02	+6.0277137E+01	+5.0000000E+02	+3.8000000E+02	+4.5325488E+02
84.0	3	+3.9000000E+02	+9.9999999E+00	+4.0000000E+02	+3.8000000E+02	+4.5545947E+02
85.0	3	+3.1000000E+02	+9.9999999E+00	+3.2000000E+02	+3.0000000E+02	+4.5619458E+02
86.0	3	+3.5666650E+02	+3.2145502E+01	+3.8000000E+02	+3.2000000E+02	+4.5692944E+02
87.0	3	+6.5666650E+02	+8.9628864E+01	+7.6000000E+02	+6.0000000E+02	+4.5766430E+02

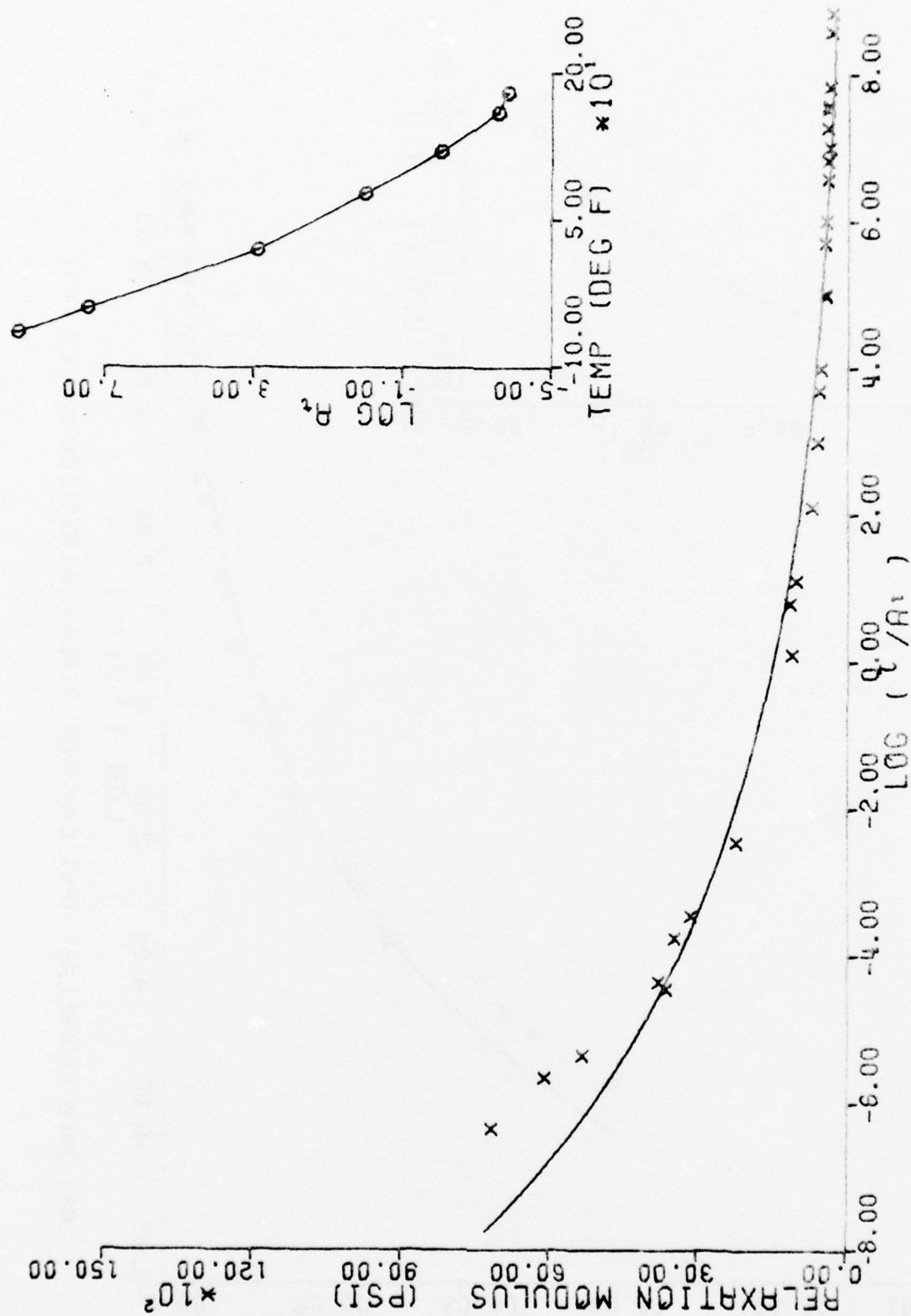
ANB 3066 PROPELLANT (ALL ANB) STRESS RELAXATION MODULUS @ 1000 SEC, 1% STRAIN

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
88.0	9	+4.0666650E+02	+2.1071307E+02	+8.8000000E+02	+2.7000000E+02	+4.5839916E+02
89.0	6	+5.9000000E+02	+5.7965506E+01	+6.5000000E+02	+5.2000000E+02	+4.5913403E+02
90.0	3	+4.5666650E+02	+2.0816659E+01	+4.8000000E+02	+4.4000000E+02	+4.5986889E+02
91.0	3	+3.5333325E+02	+1.1547005E+01	+3.6000000E+02	+3.4000000E+02	+4.6060375E+02
93.0	3	+5.4000000E+02	+1.9999999E+01	+5.6000000E+02	+5.2000000E+02	+4.6207348E+02
94.0	9	+4.0777758E+02	+6.0781941E+01	+4.8000000E+02	+3.2000000E+02	+4.6280834E+02
95.0	3	+5.3333325E+02	+2.3094010E+01	+5.6000000E+02	+5.2000000E+02	+4.6354321E+02
96.0	6	+5.0500000E+02	+2.8809720E+01	+5.5000000E+02	+4.7000000E+02	+4.6427807E+02
97.0	3	+4.1333325E+02	+5.7735026E+00	+4.2000000E+02	+4.1000000E+02	+4.6501293E+02
100.0	3	+2.4333332E+02	+1.1547005E+01	+2.5000000E+02	+2.3000000E+02	+4.6721752E+02
105.0	6	+5.4333325E+02	+1.1724617E+02	+6.9000000E+02	+3.8000000E+02	+4.7089184E+02
106.0	3	+5.0666650E+02	+1.1590225E+02	+6.4000000E+02	+4.3000000E+02	+4.7162695E+02
109.0	3	+3.1666650E+02	+5.7735026E+00	+3.2000000E+02	+3.1000000E+02	+4.7383154E+02
110.0	3	+6.3000000E+02	+1.1269427E+02	+7.6000000E+02	+5.6000000E+02	+4.7456640E+02
111.0	6	+6.9666650E+02	+1.3952299E+02	+9.3000000E+02	+5.3000000E+02	+4.7530126E+02
113.0	12	+3.6250000E+02	+1.2700214E+02	+5.9000000E+02	+2.5000000E+02	+4.7677099E+02
116.0	6	+3.6333325E+02	+9.8268340E+01	+5.5000000E+02	+2.8000000E+02	+4.7897558E+02
118.0	3	+3.5000000E+02	+1.7320508E+01	+3.6000000E+02	+3.3000000E+02	+4.8044531E+02
119.0	3	+2.7666650E+02	+5.7735026E+00	+2.8000000E+02	+2.7000000E+02	+4.8118017E+02
120.0	3	+4.0666650E+02	+2.8867513E+01	+4.4000000E+02	+3.9000000E+02	+4.8191503E+02
122.0	3	+5.8333325E+02	+4.9328828E+01	+6.4000000E+02	+5.5000000E+02	+4.8338476E+02
123.0	3	+7.7333325E+02	+4.9328828E+01	+8.3000000E+02	+7.4000000E+02	+4.8411962E+02
126.0	3	+5.5666650E+02	+4.0414518E+01	+6.0000000E+02	+5.2000000E+02	+4.8632421E+02
137.0	3	+2.6666650E+02	+5.7735026E+00	+2.7000000E+02	+2.6000000E+02	+4.9440795E+02
182.0	3	+6.9666650E+02	+1.5885003E+02	+8.8000000E+02	+6.0000000E+02	+5.2747729E+02

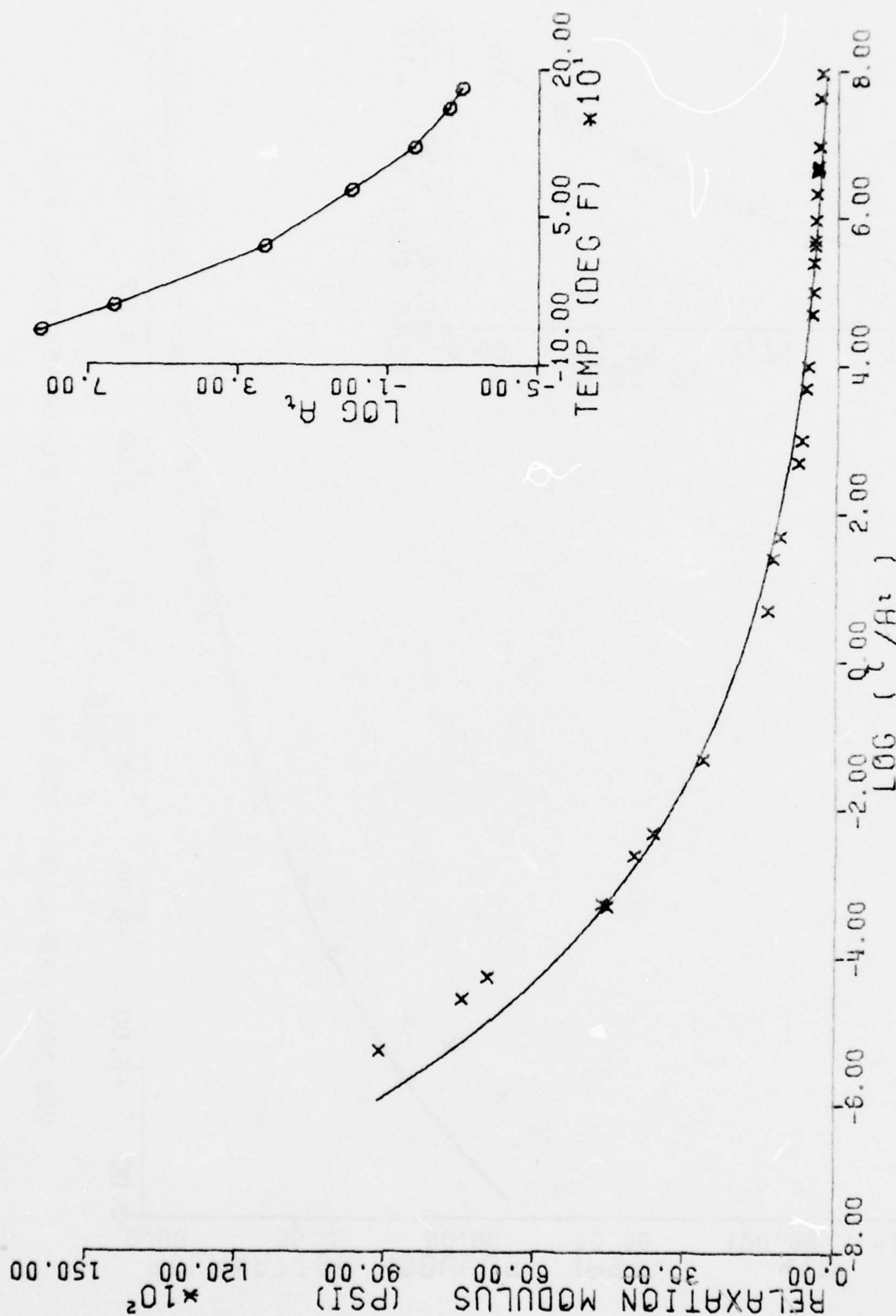
ANB-3066-PROPELLANT (ALL ANB) STRESS RELAXATION MODULUS @ 1000 SEC; 1% STRAIN



ANB 3066 PROPELLANT (ANB CARTONS) STRESS RELAXATION MASTER PLOT

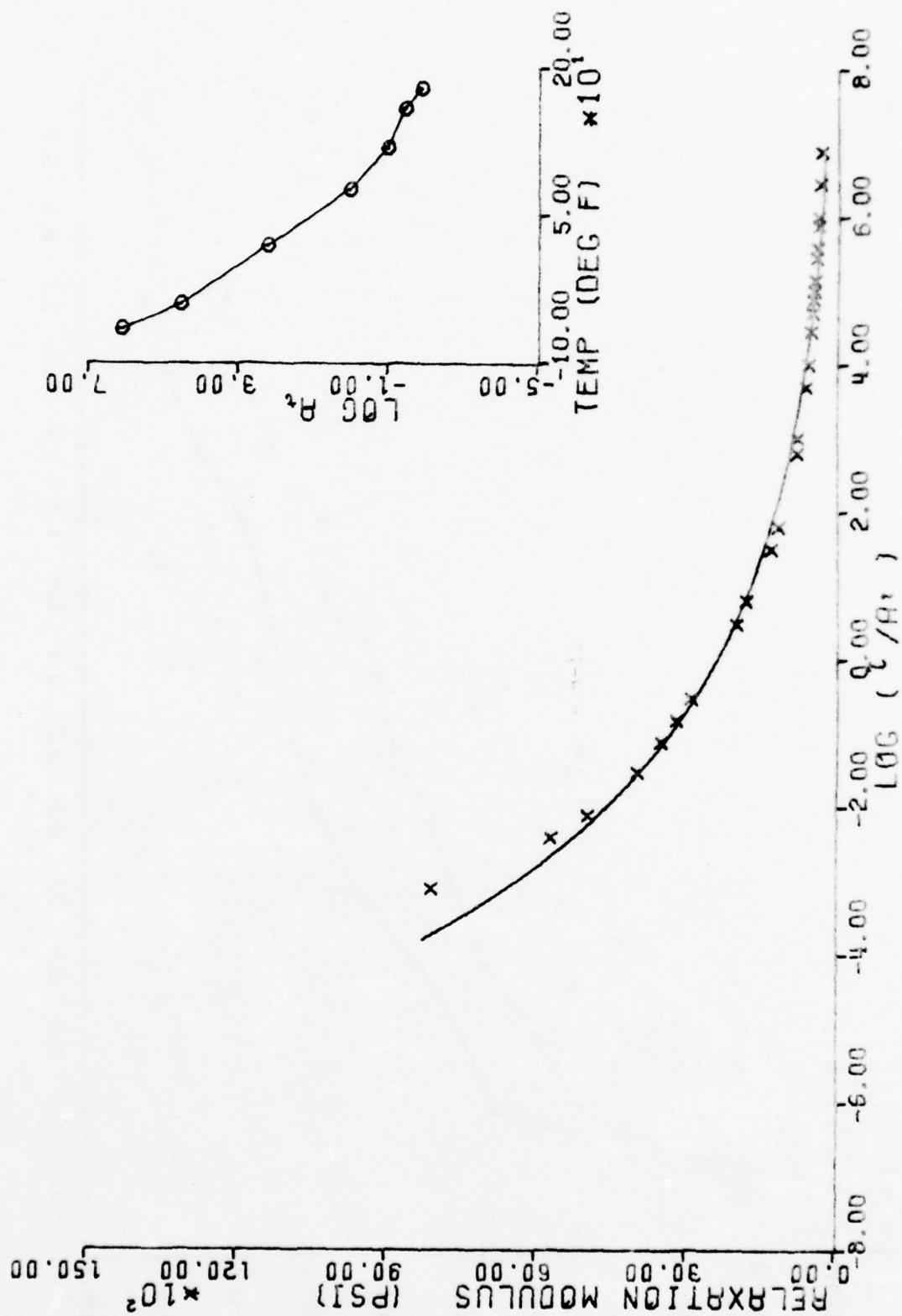
Figure 6-11





ANB 3066 PROPELLANT (ANT CARBONS) STRESS RELAXATION MASTER PLOT

Figure 6-12



ANB 3066 PROPELLANT (ANA CARTONS) STRESS RELAXATION MASTER PLOT

Figure 6-13

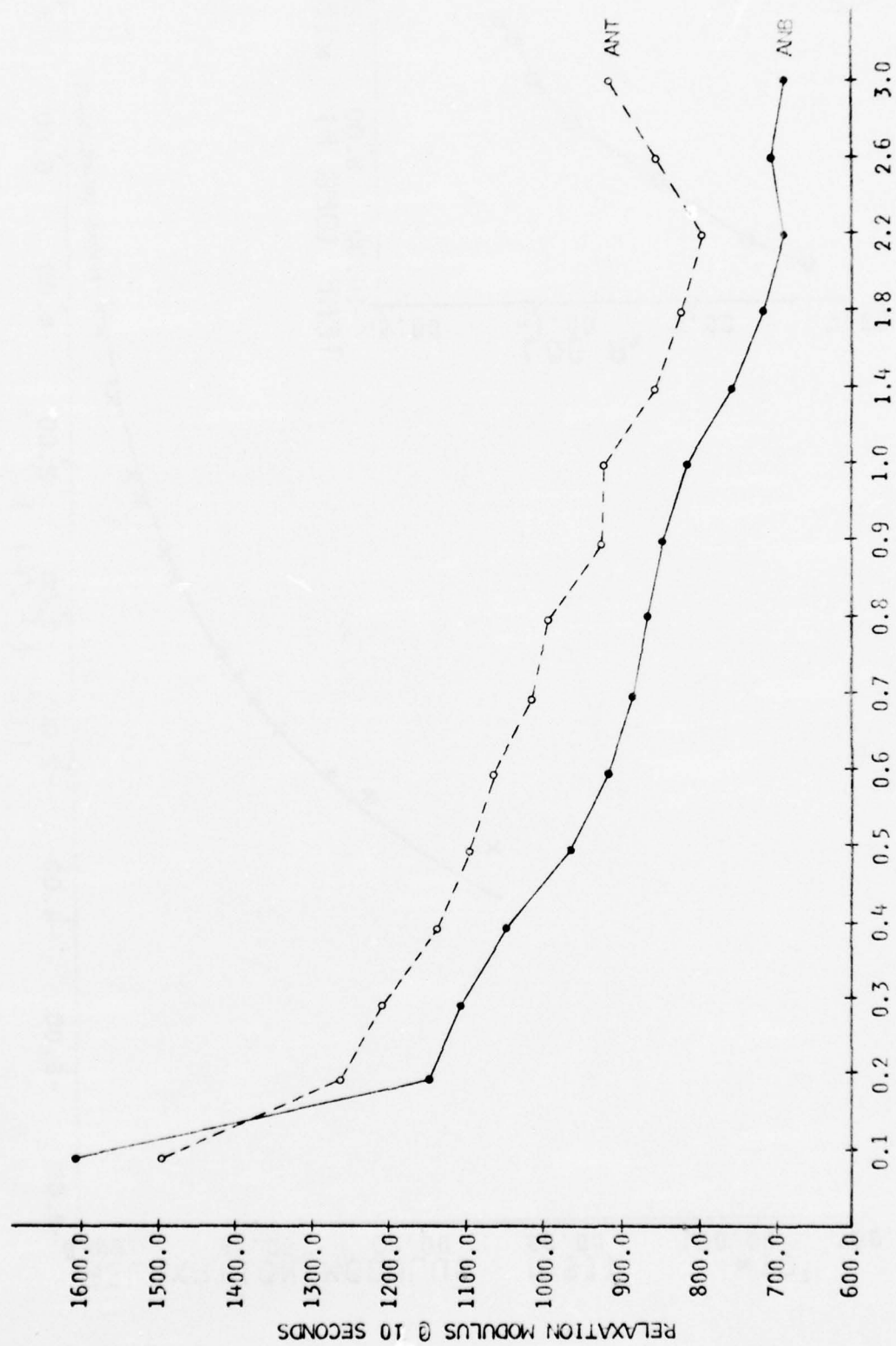


Figure 6-14

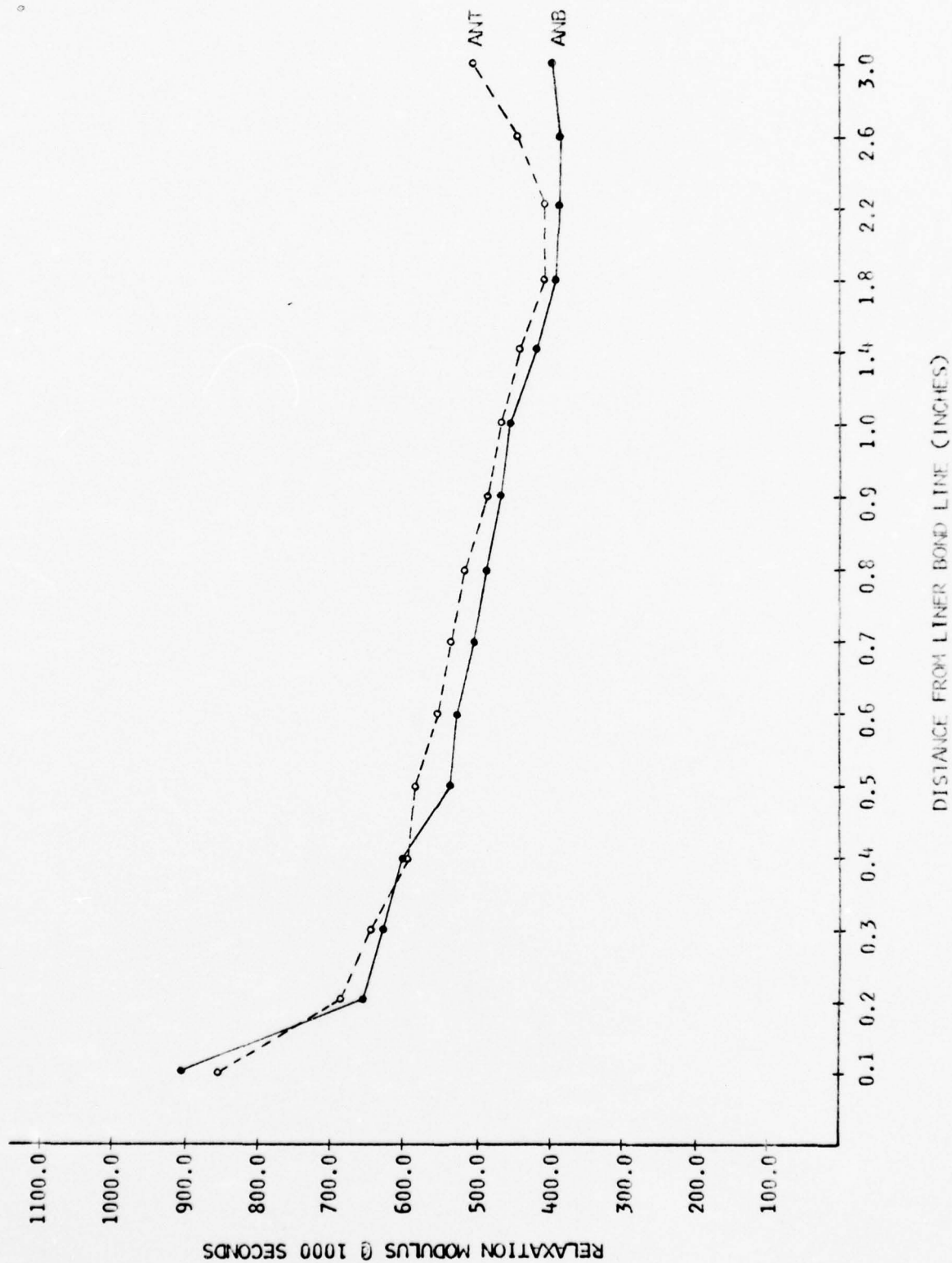


Figure 6-15



## SECTION VII

### Thermal Coefficient of Linear Expansion

Thermal coefficient of linear expansion (TCLE) is run using an expansion probe on the DuPont 990 TMA. The specimen is a 0.200" wafer (.508cm) which is cooled to  $-110^{\circ}\text{C}$  with liquid nitrogen then heated at  $5^{\circ}\text{C}/\text{min}$ . The glass point ( $T_g$ ) and TCLE above glass point, (over the range  $-110^{\circ}\text{C}$  to  $+40^{\circ}\text{C}$ ) is determined. TCLE below glass point is not considered to be of value in stress analysis.

ANA does not show a significant change in glass point, but has a significant increase in TCLE above glass point (Figure 7-1).

Data on ANB lined cartons was limited but TCLE above  $T_g$  showed a significant increase (Figure 7-5).

ANT lined cartons show a significant decrease in glass point (Figure 7-6) and a significant increase in TCLE below  $T_g$  (Figure 7-7).

All ANB shows a significant decrease in glass point (Figure 7-8) and a significant decrease in TCLE below  $T_g$  (Figure 7-9).

It is apparent that there is much variation in the data but as the data base expands there should be greater consistency.

$Y = (1 + 6.1658614E-05) + ( + 6.0259811E-07 ) \times X$   
 $F = +1.4669861E+02$  SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_1 = +1.5246758E-05$   
 $R = +7.7427859E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $\sigma_2 = +4.9752482E-08$   
 $t = +1.2111920E+01$  SIGNIFICANCE OF t = SIGNIFICANT  $\sigma_3 = +9.6979368E-06$   
 $N = 100$  DEGREES OF FREEDOM = 98  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

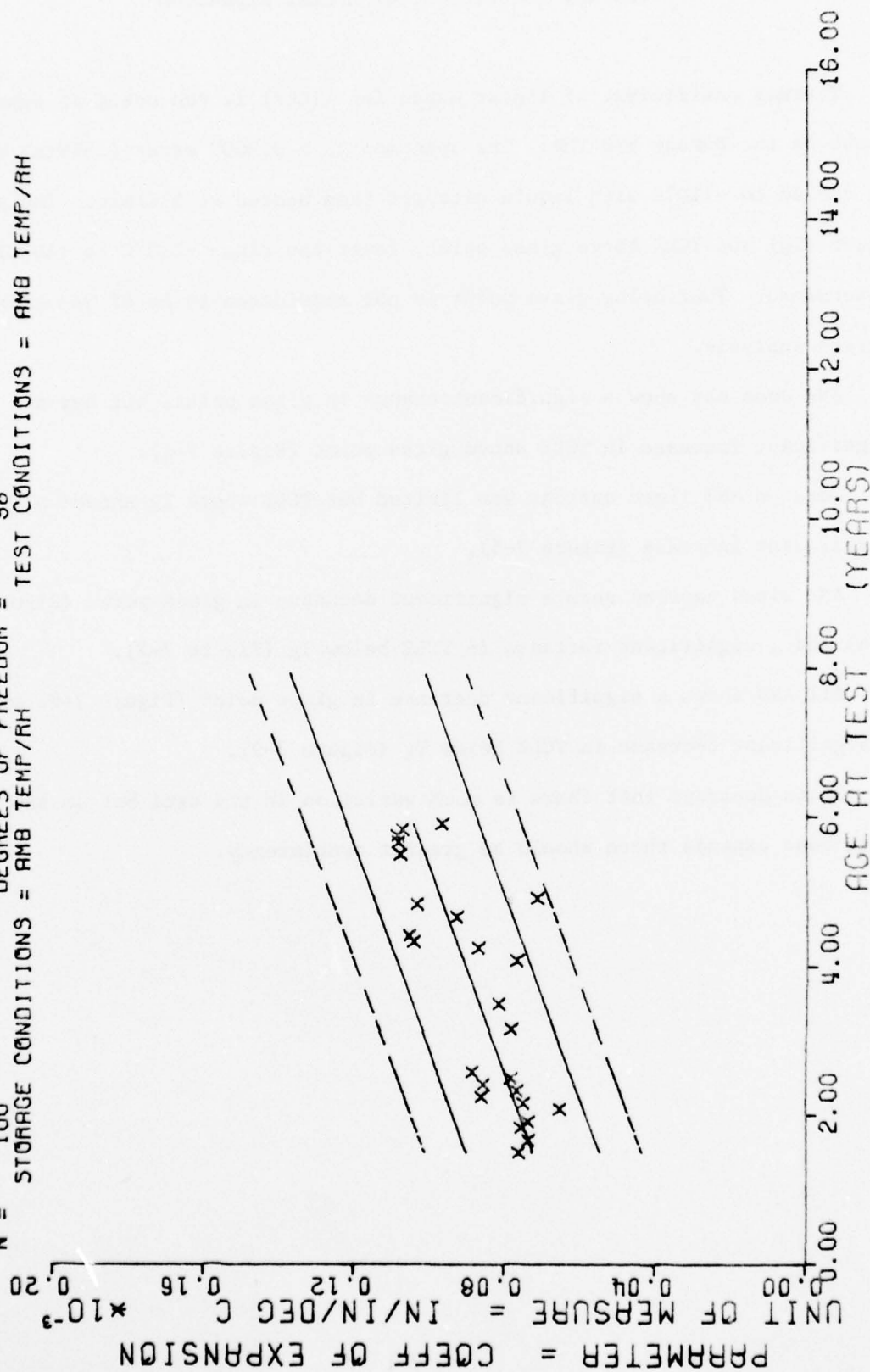


Figure 7-1

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	6	-7.9166656E+01	+1.3291601E+00	-7.8000000E+01	-8.1000000E+01	-7.6201766E+01
16.0	3	-7.8666656E+01	+3.2145502E+00	-7.5000000E+01	-8.1000000E+01	-7.6105834E+01
17.0	6	-7.6833328E+01	+1.4715601E+00	-7.5000000E+01	-7.9000000E+01	-7.6073852E+01
21.0	3	-7.5333328E+01	+5.7735026E-01	-7.5000000E+01	-7.6000000E+01	-7.5945938E+01
22.0	3	-7.7000000E+01	+0.0000000E+00	-7.7000000E+01	-7.7000000E+01	-7.5913955E+01
23.0	3	-7.6666656E+01	+1.5275252E+00	-7.5000000E+01	-7.8000000E+01	-7.5881988E+01
24.0	3	-7.2000000E+01	+0.0000000E+00	-7.2000000E+01	-7.2000000E+01	-7.5850006E+01
27.0	3	-7.7000000E+01	+1.0000000E+00	-7.6000000E+01	-7.8000000E+01	-7.5754074E+01
28.0	6	-7.1833328E+01	+2.2286019E+00	-7.0000000E+01	-7.5000000E+01	-7.5722051E+01
29.0	3	-7.5666656E+01	+2.0816659E+00	-7.8000000E+01	-8.2000000E+01	-7.5690109E+01
30.0	3	-7.3000000E+01	+2.4457513E+00	-7.1000000E+01	-7.6000000E+01	-7.5658126E+01
31.0	6	-7.5333328E+01	+1.8618986E+00	-7.2000000E+01	-7.7000000E+01	-7.5626159E+01
33.0	5	-7.4759987E+01	+3.5637059E+00	-7.0000000E+01	-7.8000000E+01	-7.5562194E+01
34.0	4	-7.6500000E+01	+3.4156502E+00	-7.2000000E+01	-8.0000000E+01	-7.5530212E+01
35.0	4	-7.6500000E+01	+2.4457513E+00	-7.4000000E+01	-8.0000000E+01	-7.5458245E+01
36.0	6	-7.7500000E+01	+2.0736441E+00	-7.4000000E+01	-7.9000000E+01	-7.5466262E+01
37.0	4	-7.6250000E+01	+5.0000000E-01	-7.6000000E+01	-7.7000000E+01	-7.5434280E+01
38.0	6	-7.2833328E+01	+5.8452259E+00	-6.2000000E+01	-7.8000000E+01	-7.5402297E+01
39.0	3	-7.9333328E+01	+1.1547005E+00	-7.8000000E+01	-8.0000000E+01	-7.5370330E+01
41.0	3	-7.8000000E+01	+1.0000000E+00	-7.7000000E+01	-7.9000000E+01	-7.5306365E+01
42.0	1	-7.4000000E+01	+0.0000000E+00	-7.4000000E+01	-7.4000000E+01	-7.5274383E+01
43.0	3	-7.6333328E+01	+1.1547005E+00	-7.5000000E+01	-7.7000000E+01	-7.5242416E+01
45.0	1	-7.6000000E+01	+0.0000000E+00	-7.6000000E+01	-7.6000000E+01	-7.5178451E+01
47.0	4	-6.9750000E+01	+5.6789083E+00	-6.2000000E+01	-7.4000000E+01	-7.5114501E+01
48.0	3	-7.6000000E+01	+1.9999999E+00	-7.4000000E+01	-7.8000000E+01	-7.5082519E+01
49.0	6	-7.1500000E+01	+5.6480084E+00	-6.6000000E+01	-8.1000000E+01	-7.5050537E+01
50.0	3	-7.8000000E+01	+2.6457513E+00	-7.5000000E+01	-8.0000000E+01	-7.5018554E+01
51.0	3	-7.4333328E+01	+2.0616659E+00	-7.2000000E+01	-7.6000000E+01	-7.4986587E+01
52.0	6	-7.7500000E+01	+5.2544415E+00	-7.1000000E+01	-8.3000000E+01	-7.4954605E+01
53.0	13	-7.2384613E+01	+4.3691811E+00	-6.5000000E+01	-7.9000000E+01	-7.4922622E+01
54.0	16	-7.1875000E+01	+4.2720018E+00	-6.5000000E+01	-7.8000000E+01	-7.4890640E+01

ANG 3066 PROPELLANT(ANG) GLASS POINT, UNLND CARTONS

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
18.0	3	+7.6333322E-05	+1.3316666E-05	+9.0999994E-05	+6.4999995E-05	+7.2505368E-05
20.0	6	+7.3666597E-05	+8.5014700E-06	+8.5999985E-05	+6.3999952E-05	+7.3710572E-05
22.0	3	+7.5666655E-05	+1.1060424E-05	+8.5999985E-05	+6.3999952E-05	+7.4915762E-05
23.0	3	+7.3666655E-05	+5.0333250E-06	+7.8999990E-05	+6.8999986E-05	+7.5518357E-05
25.0	3	+6.5333311E-05	+6.6583222E-06	+7.0999987E-05	+5.7999990E-05	+7.6723561E-05
26.0	3	+7.4999989E-05	+9.5999258E-06	+8.4999992E-05	+6.4999985E-05	+7.7326156E-05
27.0	3	+8.6333282E-05	+9.8662062E-06	+9.2999995E-05	+7.4999989E-05	+7.7928751E-05
28.0	3	+7.6666643E-05	+7.7674876E-06	+8.2999991E-05	+6.7999993E-05	+7.8531360E-05
29.0	3	+8.5666615E-05	+5.0341705E-06	+9.0999994E-05	+8.0999991E-05	+7.5133955E-05
30.0	3	+7.8333323E-05	+7.7674328E-06	+8.6999993E-05	+7.1999995E-05	+7.5736550E-05
31.0	3	+8.8666638E-05	+6.8071157E-06	+9.3999988E-05	+8.0999991E-05	+8.0339144E-05
38.0	3	+7.8333323E-05	+8.6215917E-06	+8.5999985E-05	+6.8999986E-05	+8.4557337E-05
42.0	3	+8.1733247E-05	+3.0887480E-06	+8.3899998E-05	+7.8199995E-05	+8.6967731E-05
49.0	3	+7.6766649E-05	+2.2675458E-06	+7.8499986E-05	+7.4199997E-05	+9.1185909E-05
51.0	3	+9.6965581E-05	+7.2077137E-07	+8.7599997E-05	+8.6199986E-05	+9.2391113E-05
52.0	3	+1.0429997E-04	+5.8500866E-06	+1.1109998E-04	+1.0079999E-04	+9.2993708E-05
53.0	3	+1.0539994E-04	+3.6364810E-05	+1.0639995E-04	+1.0229999E-04	+9.3596303E-05
55.0	6	+9.2849906E-05	+4.2835984E-06	+9.7999989E-05	+8.8799992E-05	+9.5404102E-05
58.0	3	+1.0343329E-04	+3.1271457E-06	+1.0629999E-04	+1.0009999E-04	+9.6609292E-05
59.0	1	+7.1299989E-05	+0.000000E+47	+7.1299989E-05	+7.1299989E-05	+9.7211901E-05
56.0	3	+1.0773329E-04	+1.9878465E-06	+1.0989999E-04	+1.0599999E-04	+1.0143007E-04
68.0	3	+1.0829992E-04	+2.4289512E-06	+1.1109998E-04	+1.0689999E-04	+1.0263528E-04
69.0	9	+1.0845540E-04	+9.1640605E-06	+1.2219999E-04	+9.7199995E-05	+1.0323787E-04
70.0	9	+1.0721097E-04	+8.6214201E-06	+1.1809999E-04	+9.1599998E-05	+1.0384047E-04
71.0	12	+9.6558258E-05	+9.3611732E-06	+1.0599999E-04	+8.2999991E-05	+1.0444306E-04

ANG 3066 PROPELLANT(ANA) TOL ABOVE GLASS POINT, UNLND CARTONS



$F = +4.2254093E+00$  SIGNIFICANCE OF F =  $+3.1978639E-02$  \* X)  
 $R = +1.2192785E-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +2.0555800E+00$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 282$  DEGREES OF FREEDOM = 280  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

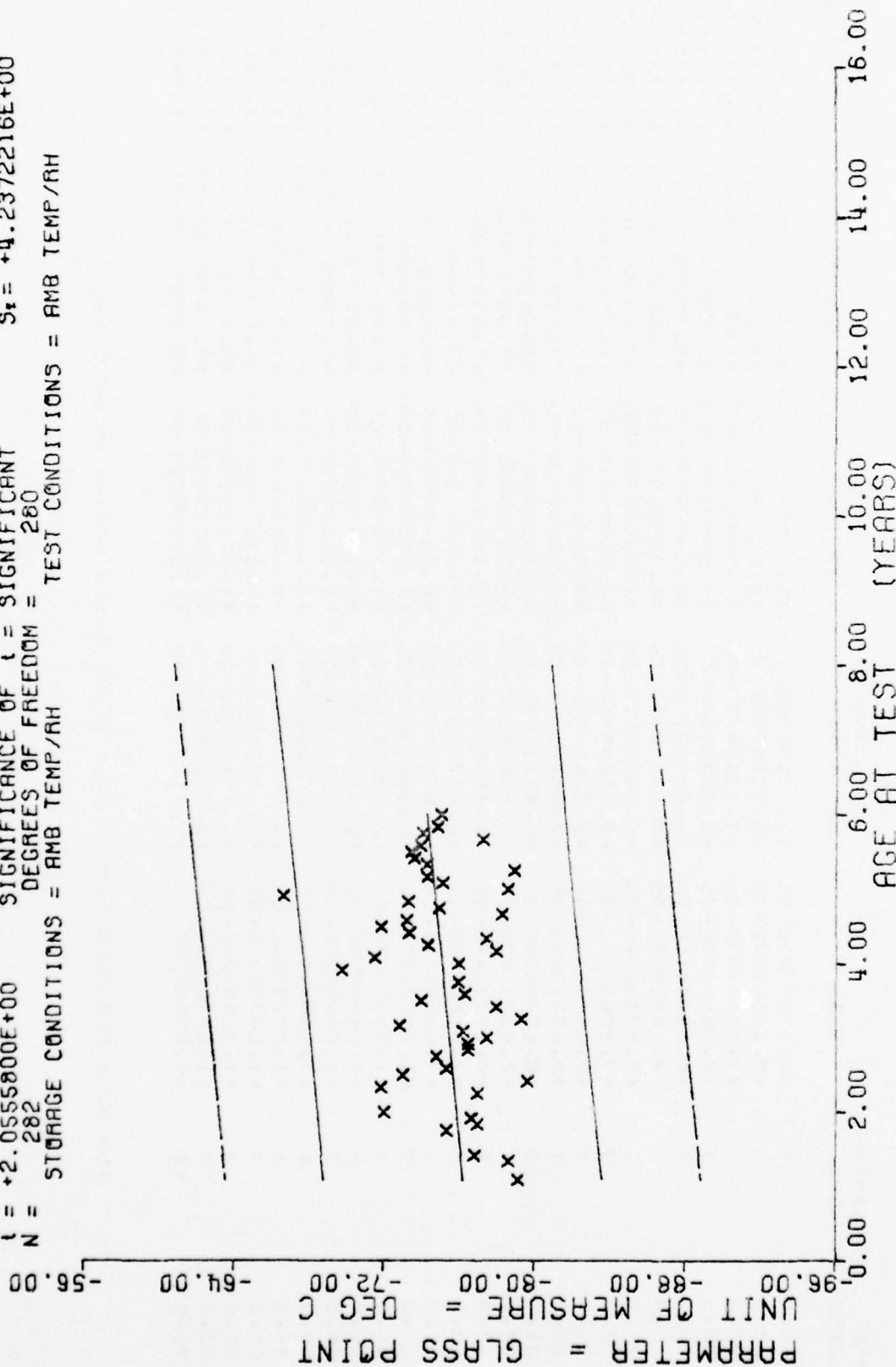


Figure 7-2

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	6	-7.9166656E+01	+1.3291601E+00	-7.8000000E+01	-8.1000000E+01	-7.6201766E+01
16.0	3	-7.8666656E+01	+3.2145502E+00	-7.5000000E+01	-8.1000000E+01	-7.6105834E+01
17.0	6	-7.6833328E+01	+1.4715601E+00	-7.5000000E+01	-7.9000000E+01	-7.6073852E+01
21.0	3	-7.5333328E+01	+5.7735026E-01	-7.5000000E+01	-7.6000000E+01	-7.5945938E+01
22.0	3	-7.7000000E+01	+0.0000000E+00	-7.7000000E+01	-7.7000000E+01	-7.5913955E+01
23.0	3	-7.6666656E+01	+1.5275252E+00	-7.5000000E+01	-7.8000000E+01	-7.5881988E+01
24.0	3	-7.2000000E+01	+0.0000000E+00	-7.2000000E+01	-7.2000000E+01	-7.5850006E+01
27.0	3	-7.7000000E+01	+1.0000000E+00	-7.6000000E+01	-7.8000000E+01	-7.5754074E+01
28.0	6	-7.1833328E+01	+2.2286019E+00	-7.0000000E+01	-7.5000000E+01	-7.5722091E+01
29.0	3	-7.9666656E+01	+2.0816659E+00	-7.8000000E+01	-8.2000000E+01	-7.5690109E+01
30.0	3	-7.3000000E+01	+2.4457513E+00	-7.1000000E+01	-7.6000000E+01	-7.5658126E+01
31.0	6	-7.5333328E+01	+1.8618986E+00	-7.2000000E+01	-7.7000000E+01	-7.5626159E+01
33.0	5	-7.4799987E+01	+3.5637059E+00	-7.0000000E+01	-7.8000000E+01	-7.5562194E+01
34.0	4	-7.6500000E+01	+3.4156502E+00	-7.2000000E+01	-8.0000000E+01	-7.5530212E+01
35.0	4	-7.6500000E+01	+2.4457513E+00	-7.4000000E+01	-8.0000000E+01	-7.5458245E+01
36.0	6	-7.7500000E+01	+2.0736441E+00	-7.4000000E+01	-7.9000000E+01	-7.5466262E+01
37.0	4	-7.6250000E+01	+5.0000000E-01	-7.6000000E+01	-7.7000000E+01	-7.5434280E+01
38.0	6	-7.2833328E+01	+5.8452259E+00	-6.2000000E+01	-7.8000000E+01	-7.5402297E+01
39.0	3	-7.9333328E+01	+1.1547005E+00	-7.8000000E+01	-8.0000000E+01	-7.5370330E+01
41.0	3	-7.8000000E+01	+1.0000000E+00	-7.7000000E+01	-7.9000000E+01	-7.5306365E+01
42.0	1	-7.4000000E+01	+0.0000000E+00	-7.4000000E+01	-7.4000000E+01	-7.5274383E+01
43.0	3	-7.6333328E+01	+1.1547005E+00	-7.5000000E+01	-7.7000000E+01	-7.5242416E+01
45.0	1	-7.6000000E+01	+0.0000000E+00	-7.6000000E+01	-7.6000000E+01	-7.5178451E+01
47.0	4	-6.9750000E+01	+5.6789083E+00	-6.2000000E+01	-7.4000000E+01	-7.5114501E+01
48.0	3	-7.6000000E+01	+1.9599999E+00	-7.4000000E+01	-7.8000000E+01	-7.5082519E+01
49.0	6	-7.1500000E+01	+5.6480084E+00	-6.6000000E+01	-8.1000000E+01	-7.5050537E+01
50.0	3	-7.8000000E+01	+2.6457513E+00	-7.5000000E+01	-8.0000000E+01	-7.5018554E+01
51.0	3	-7.4333328E+01	+2.0616659E+00	-7.2000000E+01	-7.6000000E+01	-7.4986587E+01
52.0	6	-7.7500000E+01	+5.2544415E+00	-7.1000000E+01	-8.3000000E+01	-7.4954605E+01
53.0	13	-7.2384613E+01	+4.3691811E+00	-6.5000000E+01	-7.9000000E+01	-7.4922622E+01
54.0	16	-7.1875000E+01	+4.2720018E+00	-6.5000000E+01	-7.8000000E+01	-7.4890640E+01

ANG 3066 PROPELLANT(ANG) GLASS POINT, UNLND CARTONS

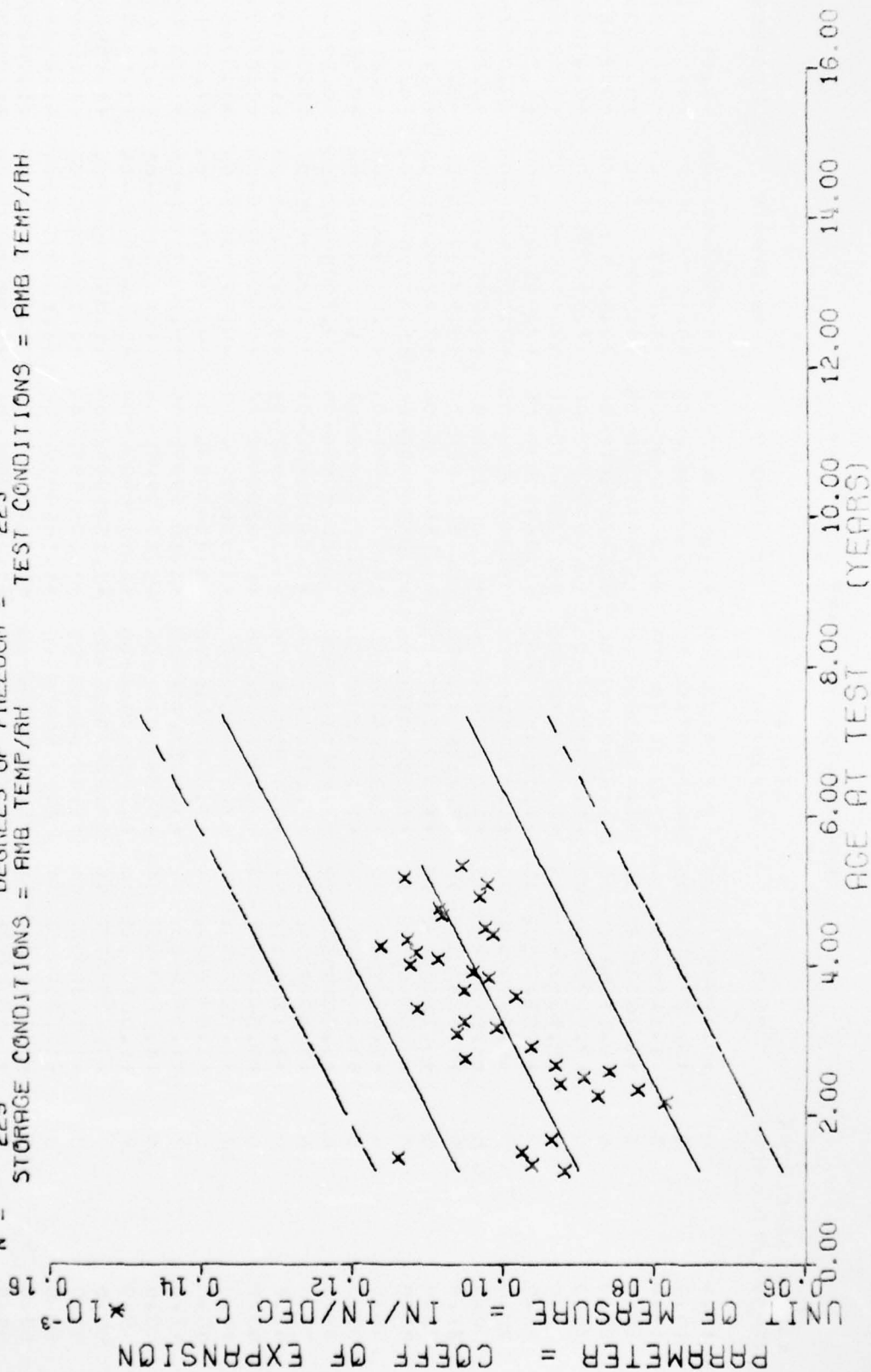
\*\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MCNTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
55.0	13	-7.3230758E+01	+4.4376015E+00	-6.7000000E+01	-8.1000000E+01	-7.4858673E+01
56.0	6	-7.83333328E+01	+1.7511900E+00	-7.7000000E+01	-8.1000000E+01	-7.4326690E+01
57.0	6	-7.5000000E+01	+1.6732200E+00	-7.3000000E+01	-7.7000000E+01	-7.4794708E+01
58.0	12	-7.33333328E+01	+4.1633319E+00	-6.2000000E+01	-7.8000000E+01	-7.4762725E+01
59.0	3	-6.6666656E+01	+5.0322229E+00	-6.2000000E+01	-7.2000000E+01	-7.4730758E+01
60.0	9	-7.8666656E+01	+1.9599999E+00	-7.5000000E+01	-8.1000000E+01	-7.4698776E+01
61.0	11	-7.5181808E+01	+4.8552667E+00	-6.9000000E+01	-8.4000000E+01	-7.4666793E+01
62.0	9	-7.43333328E+01	+2.8722813E+00	-6.8000000E+01	-7.9000000E+01	-7.4634811E+01
63.0	9	-7.5000000E+01	+2.1794454E+00	-7.6000000E+01	-8.2000000E+01	-7.4602844E+01
64.0	3	-7.43333328E+01	+1.5275252E+00	-7.3000000E+01	-7.6000000E+01	-7.4570861E+01
65.0	3	-7.3666656E+01	+2.0816659E+00	-7.2000000E+01	-7.6000000E+01	-7.4538879E+01
66.0	4	-7.3500000E+01	+3.4156502E+00	-6.9000000E+01	-7.7000000E+01	-7.4506896E+01
67.0	1	-7.4000000E+01	+0.0000000E+99	-7.4000000E+01	-7.4000000E+01	-7.4474529E+01
68.0	3	-7.73333328E+01	+1.1547005E+00	-7.6000000E+01	-7.8000000E+01	-7.4442947E+01
69.0	18	-7.4111099E+01	+3.3235149E+00	-6.8000000E+01	-8.0000000E+01	-7.4410964E+01
70.0	12	-7.4916656E+01	+5.5670839E+00	-5.8000000E+01	-7.8000000E+01	-7.4378582E+01
72.0	18	-7.5111099E+01	+6.1058206E+00	-5.6000000E+01	-8.1000000E+01	-7.4315032E+01

ANB 3066 PROPELLANT (ANE) GLASS POINT, UNLND CARTONS

$Y = ((+8.3728688E-05) + (+4.2582805E-07) \times X)$   
 $F = +8.6131029E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_1 = +1.0609479E-05$   
 $R = +5.2784755E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +4.5883277E-08$   
 $t = +9.2806804E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_r = +9.0312278E-06$   
 $N = 225$  DEGREES OF FREEDOM = 223  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



AMS 3066 PROPELLANT (ANT) TCLE ABOVE GLASS POINT, UNLND CARTONS

Figure 7-3



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
15.0	9	+9.1588826E-05	+8.6174133E-06	+1.0565998E-04	+8.0999991E-05	+9.0116096E-05
16.0	3	+9.6299918E-05	+4.0660779E-06	+9.9399985E-05	+9.1659999E-05	+9.0541929E-05
17.0	3	+1.1409996E-04	+1.7790578E-06	+1.1549999E-04	+1.1209999E-04	+9.0967761E-05
18.0	3	+9.7633252E-05	+1.4219385E-06	+9.8499993E-05	+9.5999988E-05	+9.1393580E-05
20.0	6	+9.3766604E-05	+1.8830867E-06	+9.6299991E-05	+9.1399997E-05	+9.2245245E-05
26.0	6	+7.8599929E-05	+4.2594216E-06	+8.6899992E-05	+7.4799989E-05	+9.4800212E-05
27.0	9	+8.7533262E-05	+2.6093874E-06	+9.1399997E-05	+8.4199986E-05	+9.5226045E-05
28.0	3	+8.2259957E-05	+4.7154872E-06	+8.7699998E-05	+7.8999990E-05	+9.5551863E-05
29.0	3	+9.2569919E-05	+1.4787416E-06	+9.3499998E-05	+9.0999993E-05	+9.6077696E-05
30.0	6	+8.9449924E-05	+1.0527747E-05	+1.0009999E-04	+7.5899995E-05	+9.6503528E-05
31.0	6	+8.6033251E-05	+2.7629441E-06	+8.9899986E-05	+8.2299986E-05	+9.6929346E-05
32.0	6	+9.3166629E-05	+1.2791331E-05	+1.0549998E-04	+7.7299991E-05	+9.7355179E-05
33.0	3	+1.0516664E-04	+1.2505075E-06	+1.0639999E-04	+1.0389999E-04	+9.7781012E-05
35.0	6	+9.6399919E-05	+1.5786459E-05	+1.1359999E-04	+7.9099991E-05	+9.8632663E-05
37.0	6	+1.0623324E-04	+1.2294309E-06	+1.0809999E-04	+1.0459999E-04	+9.9484313E-05
38.0	6	+1.0099995E-04	+3.4346154E-06	+1.0539998E-04	+9.7099997E-05	+9.9910146E-05
39.0	6	+1.0529994E-04	+2.5826376E-06	+1.0819999E-04	+1.0209999E-04	+1.0033597E-04
41.0	9	+1.1162211E-04	+6.4895022E-06	+1.1859998E-04	+9.6699994E-05	+1.0118763E-04
43.0	6	+9.8449949E-05	+2.7158588E-06	+1.0229999E-04	+9.5599995E-05	+1.0203928E-04
44.0	12	+1.0537491E-04	+7.2526654E-06	+1.1869998E-04	+9.8999997E-05	+1.0246511E-04
46.0	6	+1.0208322E-04	+7.6238781E-06	+1.1049999E-04	+9.2999995E-05	+1.0331676E-04
47.0	12	+1.0419986E-04	+5.4777777E-06	+1.1029999E-04	+9.2899994E-05	+1.0374259E-04
48.0	6	+1.1249995E-04	+5.3865976E-06	+1.1799999E-04	+1.0619999E-04	+1.0416842E-04
49.0	9	+1.0879991E-04	+4.7381994E-06	+1.1739999E-04	+1.0309999E-04	+1.0459424E-04
50.0	6	+1.1168877E-04	+2.2042982E-06	+1.1549999E-04	+1.0819999E-04	+1.0502008E-04
51.0	3	+1.1679995E-04	+5.3854444E-06	+1.2259998E-04	+1.1289998E-04	+1.0544591E-04
52.0	3	+1.1289995E-04	+2.1395029E-06	+1.1459999E-04	+1.1049999E-04	+1.0587173E-04
53.0	15	+1.0152655E-04	+1.0195688E-05	+1.1379999E-04	+8.6899992E-05	+1.0629756E-04
54.0	9	+1.0257767E-04	+8.6287359E-06	+1.1609999E-04	+9.3899987E-05	+1.0672339E-04
56.0	12	+1.0829158E-04	+3.0766848E-06	+1.1289998E-04	+1.0249999E-04	+1.0757504E-04
57.0	6	+1.0868724E-04	+7.7215675E-06	+1.1799999E-04	+9.7279998E-05	+1.0800088E-04

AGE 3066 PROPELLANT(IANT) TGLF ABOVE GLASS POINT, UNLND CAPTIONS

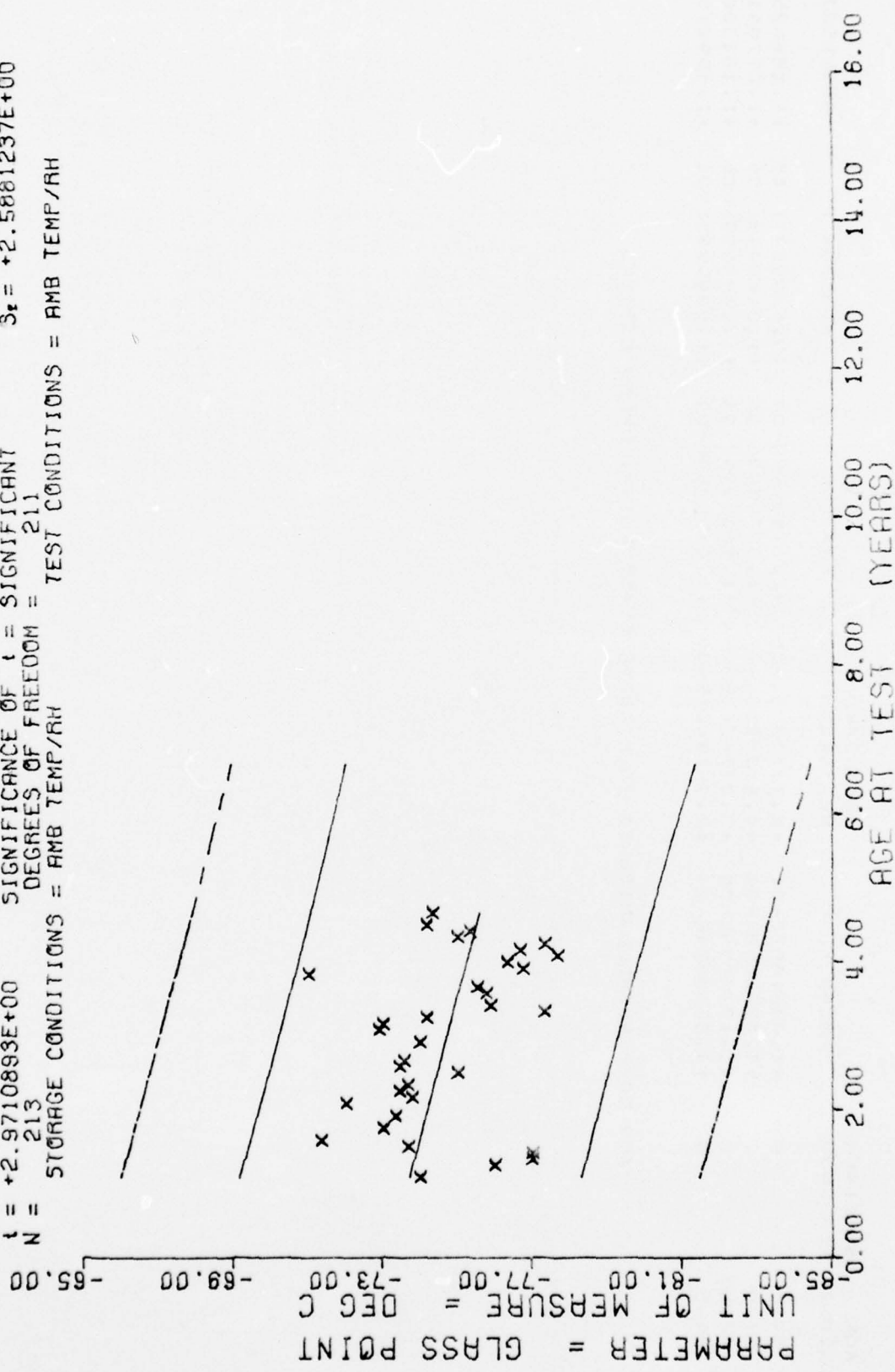
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
59.0	6	+1.0331557E-04	+4.1770335E-06	+1.0749998E-04	+9.6399991E-05	+1.0885253E-04
61.0	3	+1.0226653E-04	+6.5538058E-07	+1.0279999E-04	+1.0149958E-04	+1.0970419E-04
62.0	3	+1.1726659E-04	+3.0174066E-06	+1.1609999E-04	+1.1009999E-04	+1.1013001E-04
64.0	6	+1.0563324E-04	+2.0919901E-06	+1.0749998E-04	+1.0249999E-04	+1.1098168E-04

ANB 3066 PROPELLANT(ANT) TCLE ABOVE GLASS POINT, UNLND CARTRONS

$F = +8.8273719E+00$  SIGNIFICANCE OF  $F =$  SIGNIFICANT  $\sigma_1 = +2.6354694E+00$   
 $R = -2.0038943E-01$  SIGNIFICANCE OF  $R =$  SIGNIFICANT  $\sigma_2 = +1.4770050E-02$   
 $t = +2.9710893E+00$  SIGNIFICANCE OF  $t =$  SIGNIFICANT  $\sigma_3 = +2.5881237E+00$   
 $N = 213$  DEGREES OF FREEDOM = 211  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



ANB 3066 PROPELLANT (ANT) GLASS POINT, UNLND CARTONS

Figure 7-4

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MCNTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	3	-7.4000000E+01	+1.0000000E+00	-7.3000000E+01	-7.5000000E+01	-7.2725631E+01
15.0	9	-7.6000000E+01	+4.5244289E+00	-6.7000000E+01	-8.2000000E+01	-7.3813400E+01
16.0	3	-7.7000000E+01	+1.0000000E+00	-7.6000000E+01	-7.8000000E+01	-7.3857284E+01
17.0	3	-7.7000000E+01	+1.0000000E+00	-7.6000000E+01	-7.8000000E+01	-7.3901153E+01
18.0	3	-7.3666656E+01	+1.5275252E+00	-7.2000000E+01	-7.5000000E+01	-7.3945037E+01
19.0	3	-7.1333328E+01	+5.7735026E-01	-7.1000000E+01	-7.2000000E+01	-7.3968922E+01
21.0	3	-7.3000000E+01	+1.7320508E+00	-7.1000000E+01	-7.4000000E+01	-7.4076690E+01
23.0	3	-7.3333328E+01	+5.7735026E-01	-7.3000000E+01	-7.4000000E+01	-7.4164459E+01
25.0	3	-7.2000000E+01	+1.0000000E+00	-7.1000000E+01	-7.3000000E+01	-7.4252227E+01
26.0	9	-7.3777770E+01	+2.1081851E+00	-7.1000000E+01	-7.7000000E+01	-7.4296112E+01
27.0	9	-7.3444442E+01	+1.3333333E+00	-7.2000000E+01	-7.6000000E+01	-7.4339996E+01
28.0	6	-7.3666656E+01	+2.2509257E+00	-7.0000000E+01	-7.6000000E+01	-7.4383880E+01
30.0	6	-7.5000000E+01	+1.2649110E+00	-7.4000000E+01	-7.7000000E+01	-7.4471633E+01
31.0	9	-7.3444442E+01	+1.4240000E+00	-7.0000000E+01	-7.5000000E+01	-7.4515518E+01
32.0	9	-7.3555541E+01	+2.1278575E+00	-7.0000000E+01	-7.6000000E+01	-7.4559402E+01
35.0	6	-7.4000000E+01	+1.0554451E+00	-7.2000000E+01	-7.5000000E+01	-7.4691055E+01
37.0	9	-7.2888885E+01	+2.2607766E+00	-6.9000000E+01	-7.5000000E+01	-7.4778823E+01
38.0	3	-7.3000000E+01	+1.0000000E+00	-7.2000000E+01	-7.4000000E+01	-7.4822708E+01
39.0	6	-7.4166656E+01	+3.1251666E+00	-7.1000000E+01	-7.7000000E+01	-7.4866592E+01
40.0	3	-7.7333328E+01	+1.5275252E+00	-7.6000000E+01	-7.9000000E+01	-7.4910476E+01
41.0	9	-7.5888885E+01	+2.5712081E+00	-7.1000000E+01	-7.9000000E+01	-7.4954360E+01
43.0	9	-7.5777770E+01	+1.9660625E+00	-7.3000000E+01	-7.9000000E+01	-7.5042114E+01
44.0	15	-7.5533325E+01	+2.6149751E+00	-7.1000000E+01	-7.9000000E+01	-7.5085998E+01
46.0	6	-7.1000000E+01	+2.0576176E+00	-6.9000000E+01	-7.5000000E+01	-7.5173767E+01
47.0	12	-7.6750000E+01	+2.843577E+00	-6.9000000E+01	-7.9000000E+01	-7.5217651E+01
48.0	6	-7.6333329E+01	+1.0327955E+00	-7.5000000E+01	-7.8000000E+01	-7.5261535E+01
49.0	9	-7.7666656E+01	+2.5495057E+00	-7.3000000E+01	-8.0000000E+01	-7.5305419E+01
50.0	9	-7.6666656E+01	+1.2247448E+00	-7.5000000E+01	-7.9000000E+01	-7.5349304E+01
51.0	3	-7.7333328E+01	+5.7735026E-01	-7.7000000E+01	-7.8000000E+01	-7.5393188E+01
52.0	3	-7.5000000E+01	+1.0000000E+00	-7.4000000E+01	-7.6000000E+01	-7.5437072E+01
53.0	9	-7.5333328E+01	+2.260679E+00	-7.3000000E+01	-7.9000000E+01	-7.5480957E+01

ANB 3066 PROPELLANT(ANT) GLASS POINT, UNLAD CARTONS



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
54.0	6	-7.4166656E+01	+2.768739E+00	-7.2000000E+01	-7.9000000E+01	-7.5524841E+01
56.0	9	-7.4333328E+01	+1.4142135E+00	-7.2000000E+01	-7.6000000E+01	-7.5612609E+01

ANB 3066 PROPELLANT(ANT) CLASS POINT, UNLND CARTONS

$F = +2.5868187E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_1 = +1.6369753E-05$   
 $R = +5.1251170E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +3.3036961E-07$   
 $t = +4.8855079E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_r = +1.4160893E-05$   
 $N = 69$  DEGREES OF FREEDOM = 67  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH

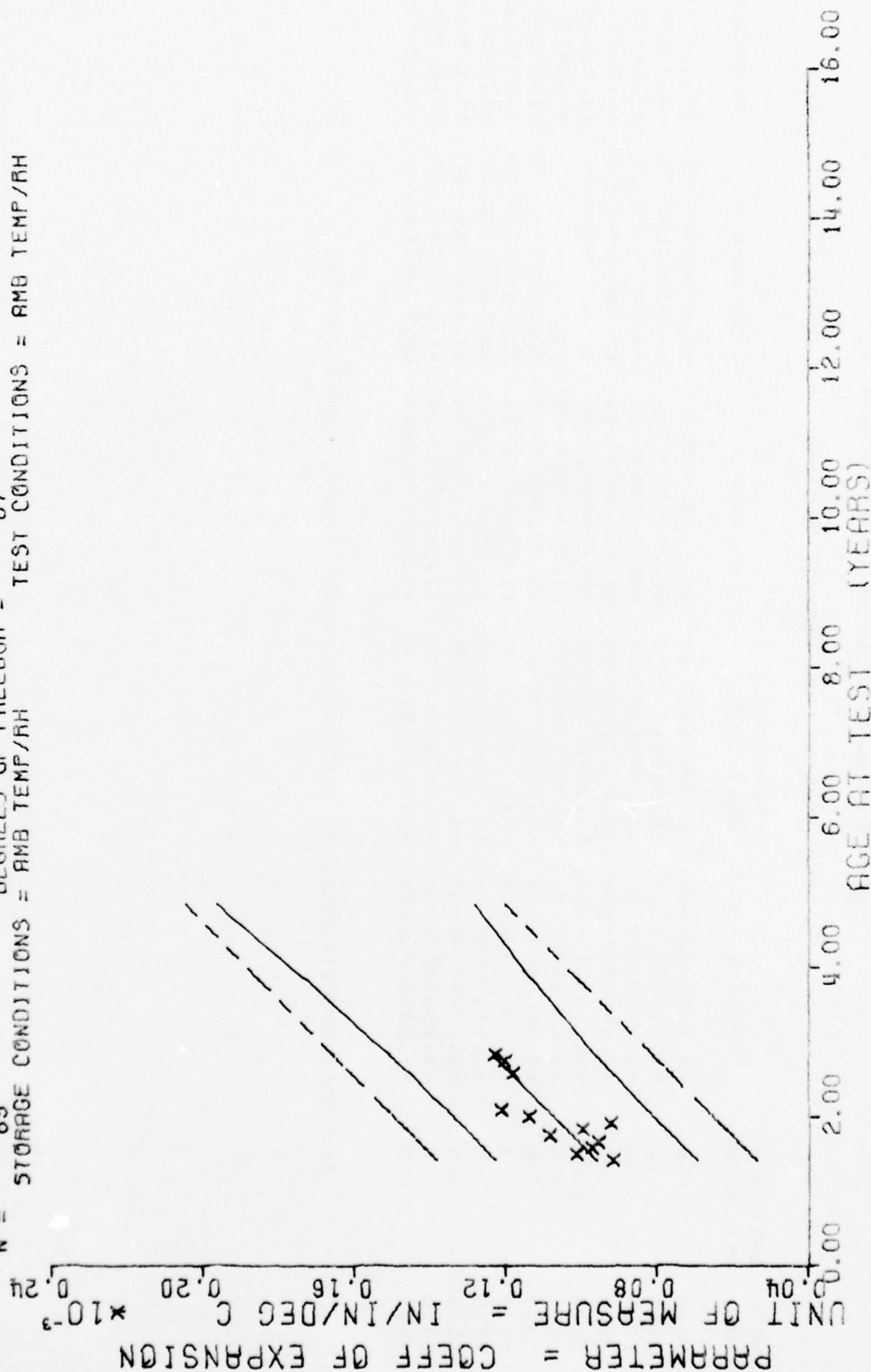


Figure 7-5

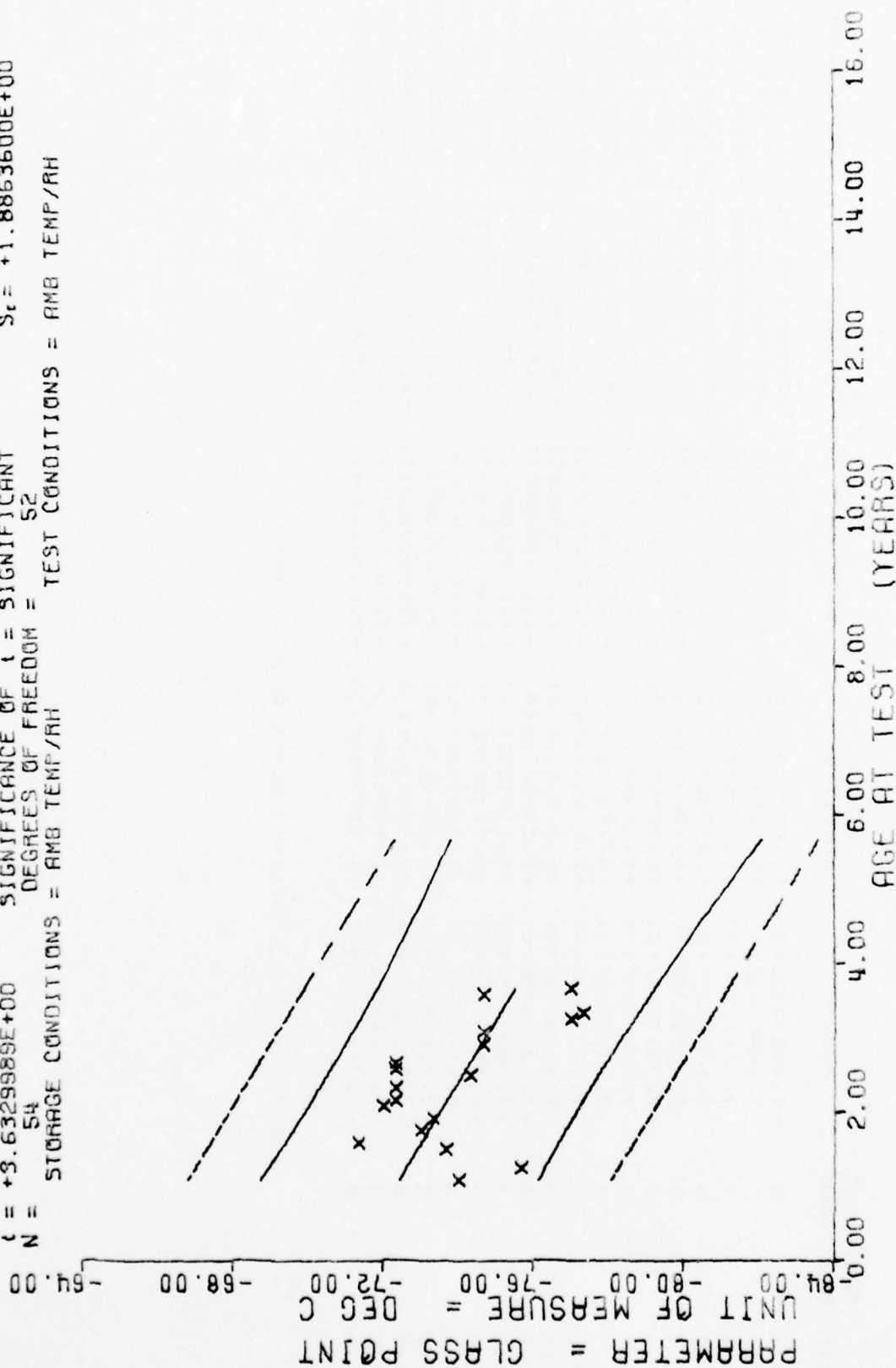
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
17.0	5	+9.1699912E-05	+2.3152340E-05	+1.1439999E-04	+6.6393996E-05	+9.6173127E-05
18.0	12	+1.0143325E-04	+1.6756297E-05	+1.2139999E-04	+7.8999990E-05	+9.7787153E-05
19.0	3	+5.7333293E-05	+2.1589535E-07	+9.7595586E-05	+9.6999996E-05	+9.5401178E-05
20.0	6	+9.5599942E-05	+2.2333148E-05	+1.1959999E-04	+7.4899993E-05	+1.0101520E-04
21.0	9	+1.0852213E-04	+1.1510048E-05	+1.1979999E-04	+8.6399998E-05	+1.0262923E-04
22.0	6	+9.5816548E-05	+1.3012790E-05	+1.1239999E-04	+8.5199993E-05	+1.0424325E-04
23.0	6	+9.2266549E-05	+4.0345313E-06	+9.6999996E-05	+8.5299994E-05	+1.0585726E-04
24.0	3	+1.1393325E-04	+2.5868962E-06	+1.1589999E-04	+1.1049999E-04	+1.0747129E-04
25.0	6	+1.2119994E-04	+3.1863258E-06	+1.2549999E-04	+1.1699995E-04	+1.0908531E-04
31.0	3	+1.1796658E-04	+4.0798634E-06	+1.2249998E-04	+1.1459995E-04	+1.1876945E-04
23.0	6	+1.2024995E-04	+1.2155534E-06	+1.2149999E-04	+1.1819999E-04	+1.2199750E-04
34.0	3	+1.2283329E-04	+3.5656881E-06	+1.2619998E-04	+1.1909999E-04	+1.2361153E-04

ANB 3066 PROPELLANT(ANB) ICLE ABOVE GLASS POINT, LINED CARTONS

$F = +1.9198681E+01$   
 $R = -4.4993095E-01$   
 $t = +3.6329989E+00$   
 $N = 54$   
 $Y = ((-7.1106455E+01) + (-1.0035381E-01) * X)$   
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM = 52  
 STORAGE CONDITIONS = AMB TEMP/RH  
 TEST CONDITIONS = AMB TEMP/RH



AMB 3066 PROPELLANT (ANT) GLASS POINT, LINED CARTONS

Figure 7-6



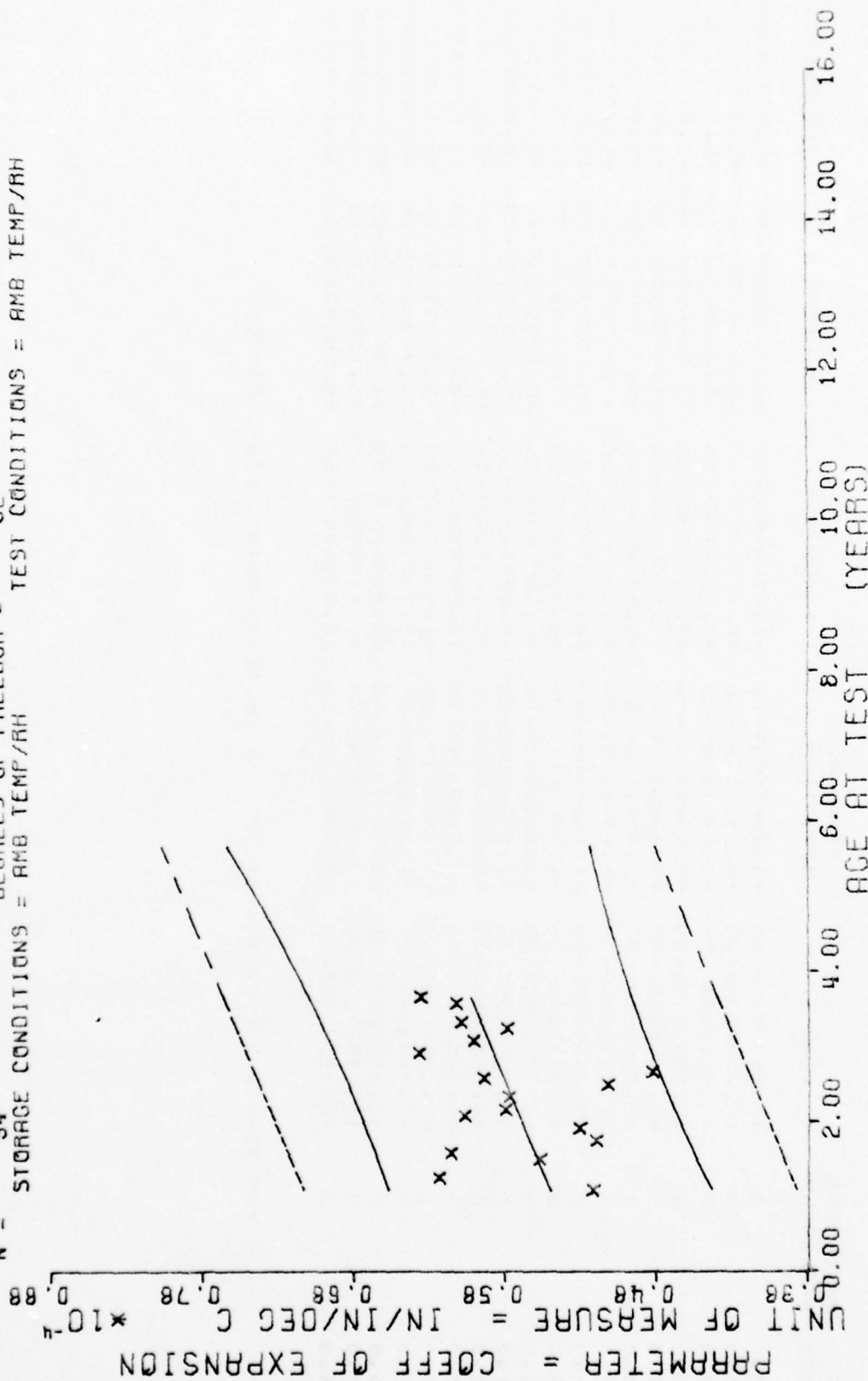
\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	3	-7.400000E+01	+1.000000E+00	-7.3000000E+01	-7.5000000E+01	-7.2411956E+01
15.0	3	-7.566666E+01	+1.527525E+00	-7.4000000E+01	-7.7000000E+01	-7.2611770E+01
18.0	3	-7.366666E+01	+1.527525E+00	-7.2000000E+01	-7.5000000E+01	-7.2912826E+01
19.0	3	-7.133332E+01	+5.773502E-01	-7.1000000E+01	-7.2000000E+01	-7.3013183E+01
21.0	3	-7.300000E+01	+1.732050E+00	-7.1000000E+01	-7.4000000E+01	-7.2213882E+01
23.0	3	-7.233332E+01	+5.773502E-01	-7.3000000E+01	-7.4000000E+01	-7.3414596E+01
25.0	3	-7.200000E+01	+1.000000E+00	-7.1000000E+01	-7.3000000E+01	-7.3615295E+01
26.0	3	-7.233332E+01	+5.773502E-01	-7.2000000E+01	-7.3000000E+01	-7.3715652E+01
28.0	3	-7.233332E+01	+2.516114E+00	-7.0000000E+01	-7.5000000E+01	-7.3916366E+01
30.0	3	-7.433332E+01	+5.773502E-01	-7.4000000E+01	-7.5000000E+01	-7.4117065E+01
31.0	3	-7.233332E+01	+2.081665E+00	-7.0000000E+01	-7.4000000E+01	-7.4217422E+01
32.0	3	-7.233332E+01	+1.527525E+00	-7.1000000E+01	-7.4000000E+01	-7.4317779E+01
35.0	3	-7.466666E+01	+5.773502E-01	-7.4000000E+01	-7.5000000E+01	-7.4618835E+01
37.0	3	-7.466666E+01	+5.773502E-01	-7.4000000E+01	-7.5000000E+01	-7.4819549E+01
39.0	3	-7.700000E+01	+0.000000E+01	-7.7000000E+01	-7.7000000E+01	-7.5020263E+01
40.0	3	-7.733332E+01	+1.527525E+00	-7.6000000E+01	-7.9000000E+01	-7.5120605E+01
43.0	3	-7.466666E+01	+1.527525E+00	-7.3000000E+01	-7.6000000E+01	-7.5421676E+01
44.0	3	-7.700000E+01	+1.000000E+00	-7.6000000E+01	-7.8000000E+01	-7.5522018E+01

AND 3066 PROPELLANT(ANT) GLASS POINT, LINED CARTONS

$F = +4.4695576E+00$  SIGNIFICANCE OF  $F =$   $(+1.6868946E-07) \times X)$   $\sigma_1 = +5.6244614E-06$   
 $R = +2.8133585E-01$  SIGNIFICANCE OF  $R =$  SIGNIFICANT  $S_e = +7.9791328E-08$   
 $t = +2.1141328E+00$  SIGNIFICANCE OF  $t =$  SIGNIFICANT  $S_f = +5.4489357E-06$   
 $N = 54$  DEGREES OF FREEDOM = 52  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = AMB TEMP/RH



AMB 3066 PROPELLANT (ANT) TCLE BELOW GLASS POINT, LINED CARTONS

Figure 7-7

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	3	+5.219990E-05	+4.2460989E-06	+5.4799995E-05	+4.7299996E-05	+5.5071664E-05
15.0	3	+6.239994E-05	+4.9150378E-06	+6.7999903E-05	+5.8799906E-05	+5.5409051E-05
18.0	3	+5.5699987E-05	+2.8581690E-06	+5.8999998E-05	+5.3999989E-05	+5.5915123E-05
19.0	3	+6.1599988E-05	+8.9369307E-06	+7.1299989E-05	+5.3699986E-05	+5.6083808E-05
21.0	3	+5.1966650E-05	+4.1789182E-06	+5.6399992E-05	+4.8099987E-05	+5.6421180E-05
23.0	3	+5.3066658E-05	+2.4581592E-06	+5.5399999E-05	+5.0499991E-05	+5.6758566E-05
25.0	3	+6.0699996E-05	+6.6774687E-06	+6.8999996E-05	+5.6499993E-05	+5.7095938E-05
26.0	3	+5.7966652E-05	+4.0065358E-06	+6.2099992E-05	+5.4099999E-05	+5.7264638E-05
28.0	3	+5.7699988E-05	+4.2296618E-06	+6.2399994E-05	+5.4179990E-05	+5.7602010E-05
30.0	3	+5.1233320E-05	+4.1101562E-06	+5.5499986E-05	+4.7299996E-05	+5.7939396E-05
31.0	3	+5.9399986E-05	+2.0983555E-06	+6.0899998E-05	+5.6999997E-05	+5.8108082E-05
32.0	3	+4.8266650E-05	+2.8536005E-06	+5.1499999E-05	+4.5609998E-05	+5.8276767E-05
35.0	3	+6.3666651E-05	+2.1126171E-06	+6.5899992E-05	+6.1699989E-05	+5.8782839E-05
37.0	3	+6.0066653E-05	+1.0682770E-06	+6.0999998E-05	+5.8999957E-05	+5.9120211E-05
39.0	3	+5.7833327E-05	+1.2694547E-06	+5.9299985E-05	+5.7099958E-05	+5.9457597E-05
40.0	3	+6.0866659E-05	+1.7784401E-06	+6.2899998E-05	+5.9599988E-05	+5.9626283E-05
43.0	3	+6.1199985E-05	+3.298739E-06	+6.4499996E-05	+5.7899989E-05	+6.0132355E-05
44.0	3	+6.3533327E-05	+2.4703820E-06	+6.5799991E-05	+6.0899998E-05	+6.0301041E-05

AND 3066 PROPELLANT(ANT) TOL BELOW GLASS POINT, LINED CARTONS

$Y = ( (-7.4560748E+01) + (-1.3094158E-02) * X )$   
 $F = +7.5938059E+00$  SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_r = +4.0627821E+00$   
 $R = -1.0287039E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +4.7516871E-03$   
 $t = +2.7556861E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_r = +4.0440829E+00$   
 $N = 712$  DEGREES OF FREEDOM = 710  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F, AMB RH

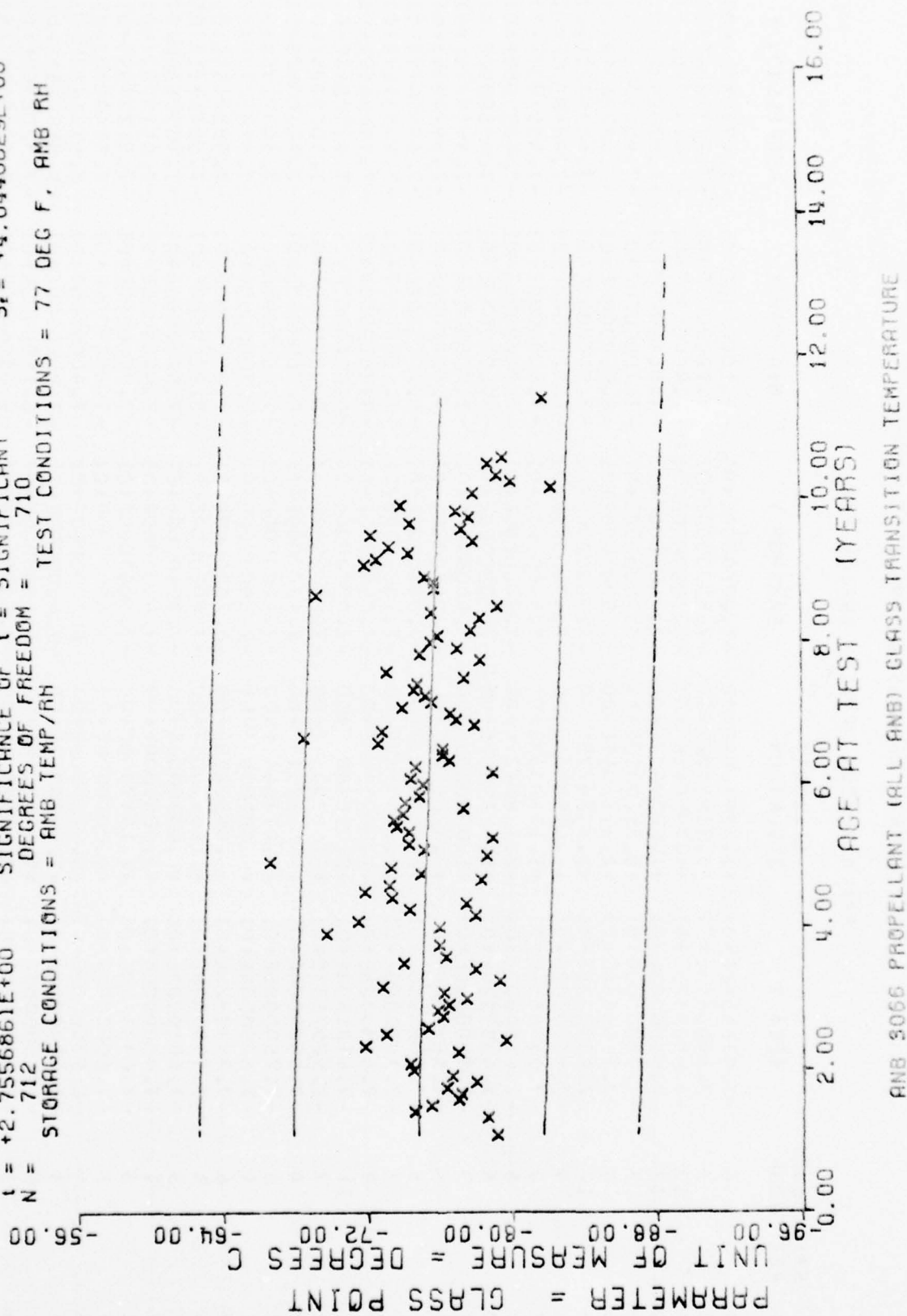


Figure 7-8



\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	6	-7.9166656E+01	+1.3291601E+00	-7.8000000E+01	-8.1000000E+01	-7.4730972E+01
16.0	3	-7.8666656E+01	+3.2145502E+00	-7.5000000E+01	-8.1000000E+01	-7.4770248E+01
17.0	12	-7.4583332E+01	+4.7950416E+00	-6.1000000E+01	-7.9000000E+01	-7.4783340E+01
18.0	12	-7.5500000E+01	+1.8829377E+00	-7.2000000E+01	-7.8000000E+01	-7.4796432E+01
19.0	3	-7.7000000E+01	+0.0000000E+00	-7.7000000E+01	-7.7000000E+01	-7.4809524E+01
20.0	6	-7.7166656E+01	+2.3166067E+00	-7.5000000E+01	-8.0000000E+01	-7.4822631E+01
21.0	12	-7.6333328E+01	+1.3026778E+00	-7.5000000E+01	-7.9000000E+01	-7.4835723E+01
22.0	9	-7.6000000E+01	+4.4158804E+00	-7.4000000E+01	-8.0000000E+01	-7.4848815E+01
23.0	9	-7.6666656E+01	+1.1180339E+00	-7.5000000E+01	-7.8000000E+01	-7.4861907E+01
24.0	6	-7.4500000E+01	+2.7386127E+00	-7.2000000E+01	-7.7000000E+01	-7.4875000E+01
25.0	6	-7.4333328E+01	+1.6329931E+00	-7.2000000E+01	-7.6000000E+01	-7.4888092E+01
27.0	3	-7.7000000E+01	+1.0000000E+00	-7.6000000E+01	-7.8000000E+01	-7.4914276E+01
28.0	6	-7.1833328E+01	+2.2286919E+00	-7.0000000E+01	-7.5000000E+01	-7.4927383E+01
29.0	3	-7.9666656E+01	+2.0816659E+00	-7.8000000E+01	-8.2000000E+01	-7.4940475E+01
30.0	3	-7.3000000E+01	+2.6457513E+00	-7.1000000E+01	-7.6000000E+01	-7.4953567E+01
31.0	9	-7.5333328E+01	+1.5811388E+00	-7.2000000E+01	-7.7000000E+01	-7.4966659E+01
33.0	11	-7.6181808E+01	+2.9263691E+00	-7.0000000E+01	-8.0000000E+01	-7.4992843E+01
34.0	7	-7.5857131E+01	+2.6095064E+00	-7.2000000E+01	-8.0000000E+01	-7.5005935E+01
35.0	4	-7.6500000E+01	+2.6457513E+00	-7.4000000E+01	-8.0000000E+01	-7.5019042E+01
36.0	5	-7.7500000E+01	+2.0736441E+00	-7.4000000E+01	-7.9000000E+01	-7.5032135E+01
37.0	4	-7.6250000E+01	+5.0000000E-01	-7.6000000E+01	-7.7000000E+01	-7.5045277E+01
38.0	6	-7.2833328E+01	+5.8452259E+00	-6.2000000E+01	-7.8000000E+01	-7.5058319E+01
39.0	3	-7.9333328E+01	+1.1547005E+00	-7.8000000E+01	-8.0000000E+01	-7.5071411E+01
41.0	3	-7.8000000E+01	+1.0000000E+00	-7.7000000E+01	-7.9000000E+01	-7.5097595E+01
42.0	1	-7.4000000E+01	+0.0000000E+00	-7.4000000E+01	-7.4000000E+01	-7.5110702E+01
43.0	3	-7.6333328E+01	+1.1547005E+00	-7.5000000E+01	-7.7000000E+01	-7.5123794E+01
45.0	1	-7.6000000E+01	+0.0000000E+00	-7.6000000E+01	-7.6000000E+01	-7.5149978E+01
47.0	4	-6.9750000E+01	+5.6789083E+00	-6.2000000E+01	-7.4000000E+01	-7.5176162E+01
48.0	3	-7.6000000E+01	+1.9999999E+00	-7.4000000E+01	-7.8000000E+01	-7.5189254E+01
49.0	6	-7.1500000E+01	+5.6480084E+00	-6.6000000E+01	-8.1000000E+01	-7.5202362E+01
50.0	3	-7.8000000E+01	+2.6457513E+00	-7.5000000E+01	-8.0000000E+01	-7.5215454E+01

ANB 3066 PROPELLANT (ALL ANB) GLASS TRANSITION TEMPERATURE

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
51.0	3	-7.4333328E+01	+2.0816659E+00	-7.2000000E+01	-7.6000000E+01	-7.5228546E+01
52.0	6	-7.7500000E+01	+5.3944415E+00	-7.1000000E+01	-8.3000000E+01	-7.5241638E+01
53.0	13	-7.3384613E+01	+4.3691811E+00	-6.5000000E+01	-7.9000000E+01	-7.5254730E+01
54.0	16	-7.1875000E+01	+4.2720018E+00	-6.5000000E+01	-7.8000000E+01	-7.5267822E+01
55.0	13	-7.3230758E+01	+4.4376015E+00	-6.7000000E+01	-8.1000000E+01	-7.5280914E+01
56.0	6	-7.8333328E+01	+1.7511900E+00	-7.7000000E+01	-8.1000000E+01	-7.5294021E+01
57.0	6	-7.5000000E+01	+1.6733200E+00	-7.3000000E+01	-7.7000000E+01	-7.5307113E+01
58.0	12	-7.3333328E+01	+4.1633319E+00	-6.2000000E+01	-7.8000000E+01	-7.5320205E+01
59.0	3	-6.6666656E+01	+5.0332229E+00	-6.2000000E+01	-7.2000000E+01	-7.5333297E+01
60.0	9	-7.8666656E+01	+1.9999999E+00	-7.5000000E+01	-8.1000000E+01	-7.5346389E+01
61.0	11	-7.5181808E+01	+4.8952667E+00	-6.9000000E+01	-8.4000000E+01	-7.5359481E+01
62.0	9	-7.4333328E+01	+2.8722813E+00	-6.8000000E+01	-7.9000000E+01	-7.5372573E+01
63.0	9	-7.9000000E+01	+2.1794494E+00	-7.6000000E+01	-8.2000000E+01	-7.5385665E+01
64.0	3	-7.4333328E+01	+1.5275252E+00	-7.3000000E+01	-7.6000000E+01	-7.5398773E+01
65.0	3	-7.3666656E+01	+2.0816659E+00	-7.2000000E+01	-7.6000000E+01	-7.5411865E+01
66.0	4	-7.2500000E+01	+3.4156502E+00	-6.9000000E+01	-7.7000000E+01	-7.5424957E+01
67.0	1	-7.4000000E+01	+0.0000000E+01	-7.4000000E+01	-7.4000000E+01	-7.5438049E+01
68.0	3	-7.7333328E+01	+1.1547005E+00	-7.6000000E+01	-7.8000000E+01	-7.5451141E+01
69.0	18	-7.4111099E+01	+3.3235149E+00	-6.8000000E+01	-8.0000000E+01	-7.5464233E+01
70.0	12	-7.4916656E+01	+5.5670839E+00	-5.8000000E+01	-7.8000000E+01	-7.5477325E+01
72.0	18	-7.5111099E+01	+6.1056206E+00	-5.6000000E+01	-8.1000000E+01	-7.5503524E+01
73.0	9	-7.4444442E+01	+5.7469798E+00	-6.3000000E+01	-7.9000000E+01	-7.5516616E+01
74.0	1	-7.9000000E+01	+0.0000000E+01	-7.9000000E+01	-7.9000000E+01	-7.5529708E+01
75.0	7	-7.4714279E+01	+3.4982989E+00	-7.0000000E+01	-7.8000000E+01	-7.5542800E+01
76.0	5	-7.6599990E+01	+3.2863353E+00	-7.3000000E+01	-7.9000000E+01	-7.5555892E+01
77.0	9	-7.6222213E+01	+3.8980051E+00	-7.0000000E+01	-8.0000000E+01	-7.5568984E+01
78.0	12	-7.6250000E+01	+2.7675062E+00	-7.2000000E+01	-8.2000000E+01	-7.5582092E+01
79.0	6	-7.2666656E+01	+1.0327955E+00	-7.2000000E+01	-7.4000000E+01	-7.5595184E+01
80.0	9	-6.8555541E+01	+5.2941267E+00	-5.7000000E+01	-7.4000000E+01	-7.5608276E+01
81.0	18	-7.2888885E+01	+6.0865221E+00	-5.6000000E+01	-7.9000000E+01	-7.5621368E+01
82.0	3	-7.8000000E+01	+1.0000000E+00	-7.7000000E+01	-7.9000000E+01	-7.5634460E+01

ANB 3066 PROPELLANT (ALL ANB) GLASS TRANSITION TEMPERATURE

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
83.0	4	-7.7000000E+01	+7.0237691E+00	-7.0000000E+01	-8.4000000E+01	-7.5647552E+01
84.0	6	-7.5666666E+01	+2.8751811E+00	-7.4000000E+01	-8.2000000E+01	-7.5660644E+01
85.0	3	-7.4000000E+01	+1.0000000E+00	-7.3000000E+01	-7.5000000E+01	-7.5673751E+01
86.0	3	-7.5666666E+01	+2.0816659E+00	-7.4000000E+01	-7.8000000E+01	-7.5686843E+01
87.0	13	-7.5307678E+01	+2.8978329E+00	-6.8000000E+01	-7.8000000E+01	-7.5699935E+01
88.0	9	-7.4666666E+01	+4.0311288E+00	-7.0000000E+01	-8.1000000E+01	-7.5713027E+01
89.0	21	-7.4857131E+01	+3.4682230E+00	-6.4000000E+01	-7.9000000E+01	-7.5726119E+01
90.0	9	-7.7444442E+01	+4.0034707E+00	-7.0000000E+01	-8.2000000E+01	-7.5739212E+01
91.0	6	-7.3166666E+01	+9.8319208E-01	-7.2000000E+01	-7.4000000E+01	-7.5752304E+01
92.0	3	-7.8333332E+01	+1.1547005E+00	-7.7000000E+01	-7.9000000E+01	-7.5778503E+01
94.0	9	-7.5000000E+01	+2.3452078E+00	-7.2000000E+01	-7.9000000E+01	-7.5791595E+01
95.0	12	-7.7083332E+01	+1.7816403E+00	-7.3000000E+01	-7.9000000E+01	-7.5804687E+01
96.0	18	-7.5611099E+01	+3.1648601E+00	-7.1000000E+01	-8.1000000E+01	-7.5817779E+01
97.0	3	-7.6000000E+01	+0.0000000E+00	-7.6000000E+01	-7.6000000E+01	-7.5830871E+01
98.0	6	-7.7833332E+01	+1.3291601E+00	-7.6000000E+01	-8.0000000E+01	-7.5843963E+01
100.0	3	-7.8333332E+01	+1.5275252E+00	-7.7000000E+01	-8.0000000E+01	-7.5870162E+01
101.0	3	-7.5666666E+01	+1.1547005E+00	-7.5000000E+01	-7.7000000E+01	-7.5883255E+01
102.0	3	-7.9333332E+01	+1.1547005E+00	-7.8000000E+01	-8.0000000E+01	-7.5896347E+01
104.0	3	-6.9333332E+01	+1.1547005E+00	-6.8000000E+01	-7.0000000E+01	-7.5922531E+01
105.0	12	-7.5833332E+01	+1.9462473E+00	-7.2000000E+01	-7.9000000E+01	-7.5935623E+01
106.0	6	-7.5833332E+01	+1.7224014E+00	-7.3000000E+01	-7.8000000E+01	-7.5948715E+01
107.0	3	-7.5333332E+01	+1.1547005E+00	-7.4000000E+01	-7.6000000E+01	-7.5961822E+01
109.0	9	-7.2000000E+01	+6.7268120E+00	-6.0000000E+01	-7.8000000E+01	-7.5988006E+01
110.0	6	-7.2666666E+01	+8.1649658E-01	-7.2000000E+01	-7.4000000E+01	-7.6001098E+01
111.0	12	-7.4416666E+01	+3.8247598E+00	-6.6000000E+01	-8.0000000E+01	-7.6014190E+01
112.0	3	-7.3333332E+01	+2.0816659E+00	-7.1000000E+01	-7.5000000E+01	-7.6027282E+01
113.0	15	-7.8000000E+01	+2.2990681E+00	-7.4000000E+01	-8.1000000E+01	-7.6040374E+01
114.0	3	-7.2333332E+01	+2.3094010E+00	-7.1000000E+01	-7.5000000E+01	-7.6053482E+01
115.0	6	-7.7333332E+01	+1.8618986E+00	-7.5000000E+01	-7.9000000E+01	-7.6066574E+01
116.0	6	-7.4500000E+01	+3.8340579E+00	-7.1000000E+01	-7.8000000E+01	-7.6079666E+01
117.0	9	-7.7777770E+01	+2.3863035E+00	-7.5000000E+01	-8.1000000E+01	-7.6092758E+01

ANB 3066 PROPELLANT (ALL ANB) GLASS TRANSITION TEMPERATURE

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

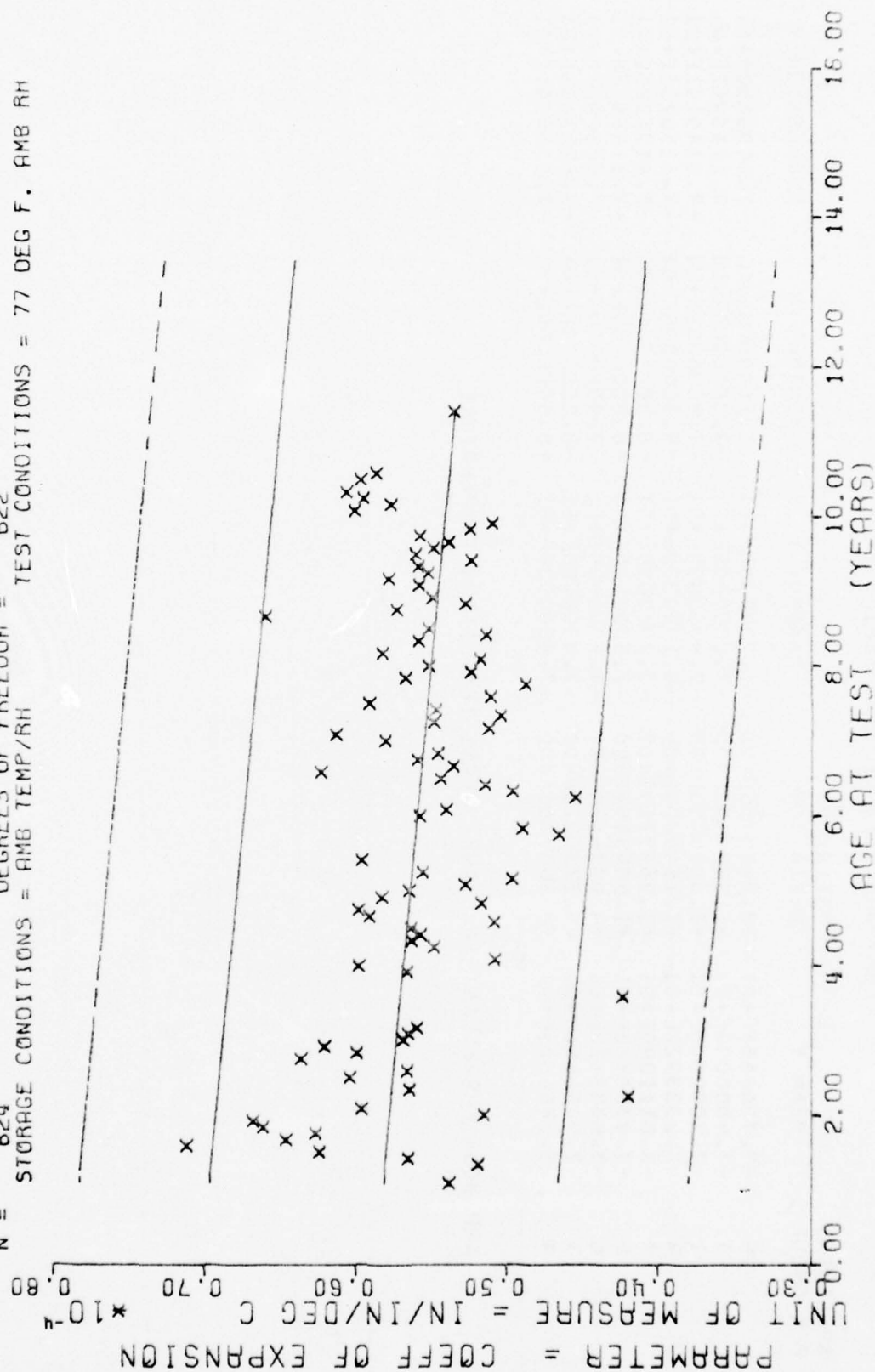
\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
118.0	15	-7.7066665E+01	+2.5485756E+00	-7.2000000E+01	-8.1000000E+01	-7.6105850E+01
119.0	3	-7.4000000E+01	+1.9999999E+00	-7.2000000E+01	-7.6000000E+01	-7.6118942E+01
121.0	1	-7.8000000E+01	+0.0000000E+03	-7.8000000E+01	-7.8000000E+01	-7.6145141E+01
122.0	3	-8.2333332E+01	+1.1547005E+00	-8.1000000E+01	-8.3000000E+01	-7.6158233E+01
123.0	2	-8.0111099E+01	+1.7649710E+00	-7.7000000E+01	-8.3000000E+01	-7.6171325E+01
124.0	6	-7.9333332E+01	+1.5055453E+00	-7.8000000E+01	-8.2000000E+01	-7.6184417E+01
126.0	6	-7.8833332E+01	+4.0824829E-01	-7.8000000E+01	-7.9000000E+01	-7.6210601E+01
127.0	3	-7.9666665E+01	+5.7735026E-01	-7.9000000E+01	-8.0000000E+01	-7.6223693E+01
137.0	2	-8.1888385E+01	+2.2607765E+00	-7.8000000E+01	-8.5000000E+01	-7.6354644E+01

ANB 3066 PROPELLANT (ALL ANB) GLASS TRANSITION TEMPERATURE



$F = +2.3605916E+01$  SIGNIFICANCE OF F = SIGNIFICANT  $\sigma_1 = +6.8301646E-06$   
 $R = -1.9121707E-01$  SIGNIFICANCE OF R = SIGNIFICANT  $S_e = +8.0777504E-09$   
 $t = +4.8585919E+00$  SIGNIFICANCE OF t = SIGNIFICANT  $S_e = +6.7095199E-06$   
 $N = 624$  DEGREES OF FREEDOM = 622  
 STORAGE CONDITIONS = AMB TEMP/RH TEST CONDITIONS = 77 DEG F. AMB RH



AMB 3066 PROPELLANT (ALL AMB) THERMAL COEFFICIENT OF LINEAR EXPANSION (BELOW GP)

Figure 7-9

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
13.0	6	+5.3916621E-05	+6.2753943E-06	+6.0799997E-05	+4.7499997E-05	+5.8258010E-05
16.0	3	+5.1966650E-05	+2.6632660E-06	+5.3699985E-05	+4.8699993E-05	+5.8140270E-05
17.0	12	+5.6624936E-05	+4.0034709E-06	+6.2699997E-05	+4.9999987E-05	+5.8101024E-05
18.0	12	+6.2508232E-05	+3.5568773E-06	+6.7799992E-05	+5.7099998E-05	+5.8061777E-05
19.0	3	+7.1266651E-05	+9.0687181E-07	+7.2099996E-05	+7.0299996E-05	+5.8022531E-05
20.0	6	+6.4733321E-05	+3.7419723E-06	+7.1699992E-05	+6.0599995E-05	+5.7983284E-05
21.0	12	+6.2741572E-05	+3.9486626E-06	+6.9899993E-05	+5.7699998E-05	+5.7944038E-05
22.0	9	+6.6221288E-05	+5.5745868E-06	+7.6699987E-05	+5.5499993E-05	+5.7904791E-05
23.0	9	+6.6888795E-05	+3.9360438E-06	+7.1299989E-05	+5.9699988E-05	+5.7865545E-05
24.0	6	+5.1583279E-05	+1.2947237E-05	+6.4699997E-05	+3.4699987E-05	+5.7826298E-05
25.0	6	+5.9716636E-05	+4.1448114E-06	+6.5499989E-05	+5.4099989E-05	+5.7787052E-05
27.0	3	+4.2033323E-05	+4.7647920E-06	+4.5499997E-05	+3.6599987E-05	+5.7708559E-05
28.0	6	+5.6533288E-05	+4.2836247E-06	+6.1099999E-05	+4.9299997E-05	+5.7669312E-05
30.0	3	+6.0499995E-05	+3.1430244E-06	+6.3299987E-05	+5.7099998E-05	+5.7590819E-05
31.0	9	+5.6677701E-05	+1.2959945E-05	+7.4999989E-05	+3.9199992E-05	+5.7551573E-05
33.0	9	+6.3733212E-05	+3.7361734E-06	+7.0599999E-05	+5.8899997E-05	+5.7473080E-05
34.0	3	+6.0033315E-05	+2.0852762E-07	+6.0199992E-05	+5.9799989E-05	+5.7433833E-05
35.0	3	+6.2166654E-05	+1.9292866E-06	+6.3699990E-05	+5.9599991E-05	+5.7394507E-05
36.0	6	+5.6949939E-05	+7.2962472E-06	+6.7499990E-05	+4.8799993E-05	+5.7355340E-05
37.0	3	+5.6633313E-05	+1.2344127E-06	+5.7999990E-05	+5.5599986E-05	+5.7316094E-05
38.0	6	+5.6049975E-05	+6.6662801E-06	+6.5999993E-05	+5.0399990E-05	+5.7276847E-05
43.0	3	+4.2399988E-05	+5.2847069E-06	+4.7299996E-05	+3.6799989E-05	+5.7080615E-05
47.0	3	+5.6666656E-05	+2.9397870E-06	+5.9099998E-05	+5.3399999E-05	+5.6923629E-05
48.0	3	+5.9899990E-05	+8.5766375E-06	+6.7299988E-05	+5.0499991E-05	+5.6884382E-05
49.0	6	+5.0883303E-05	+4.0678773E-06	+5.6299992E-05	+4.6199993E-05	+5.6845135E-05
51.0	3	+5.4933319E-05	+1.0944074E-05	+6.2599996E-05	+4.2399988E-05	+5.6766642E-05
52.0	6	+5.6399963E-05	+4.9435968E-06	+6.3499988E-05	+4.9999987E-05	+5.6727396E-05
53.0	12	+5.5824901E-05	+6.7602796E-06	+6.6999986E-05	+4.4399988E-05	+5.6688149E-05
54.0	15	+5.6439908E-05	+6.1620465E-06	+6.5299987E-05	+4.5999986E-05	+5.6648903E-05
55.0	12	+5.0916583E-05	+3.6674069E-06	+5.7499986E-05	+4.6599991E-05	+5.6609656E-05
56.0	6	+5.9199941E-05	+3.4376909E-06	+6.2999999E-05	+5.4099989E-05	+5.6570410E-05

AND 3066 PROPELLANT (ALL AND) THERMAL COEFFICIENT OF LINEAR EXPANSION (BELOW GP)

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
57.0	6	+5.9916594E-05	+2.6611937E-06	+6.3399987E-05	+5.7199998E-05	+5.6531163E-05
58.0	9	+5.1777693E-05	+3.9071397E-06	+5.6599974E-05	+4.3599985E-05	+5.6491917E-05
59.0	3	+5.8366555E-05	+3.9206639E-06	+6.2499995E-05	+5.4699994E-05	+5.6452670E-05
60.0	6	+5.6566583E-05	+2.2623002E-06	+5.9399986E-05	+5.3699986E-05	+5.6413424E-05
61.0	8	+5.2862422E-05	+7.6518538E-06	+6.3799991E-05	+4.2599992E-05	+5.6374177E-05
62.0	9	+4.9733236E-05	+6.3610258E-06	+6.0999998E-05	+4.5099994E-05	+5.6334931E-05
63.0	9	+5.5655444E-05	+3.1493921E-06	+6.1899991E-05	+5.1899987E-05	+5.6295684E-05
65.0	3	+5.9699988E-05	+7.9189182E-06	+6.8699999E-05	+5.3799987E-05	+5.6217191E-05
69.0	6	+4.6633300E-05	+2.7080220E-06	+5.0999995E-05	+4.3099993E-05	+5.6060205E-05
70.0	6	+4.9033318E-05	+4.3084001E-06	+5.2799994E-05	+4.3999985E-05	+5.6020959E-05
72.0	15	+5.5853233E-05	+5.2494332E-06	+6.8599998E-05	+4.7499997E-05	+5.5942466E-05
73.0	9	+5.4099931E-05	+6.2053731E-06	+5.9899990E-05	+4.1299994E-05	+5.5903219E-05
75.0	3	+4.5533321E-05	+7.5233595E-06	+5.4099989E-05	+3.9999998E-05	+5.5824726E-05
76.0	3	+4.9666661E-05	+1.2213629E-06	+5.0999995E-05	+4.8599991E-05	+5.5785480E-05
77.0	9	+5.1488837E-05	+5.1402858E-06	+5.9499987E-05	+4.3499996E-05	+5.5746233E-05
78.0	9	+5.4455478E-05	+5.6651894E-06	+6.0999998E-05	+4.6799992E-05	+5.5706987E-05
79.0	6	+6.2366598E-05	+3.7807496E-06	+6.6399996E-05	+5.6599994E-05	+5.5667740E-05
80.0	9	+5.3611060E-05	+7.0627172E-06	+6.6399996E-05	+4.4299988E-05	+5.5628494E-05
81.0	18	+5.5988784E-05	+6.8188093E-06	+6.8199995E-05	+4.4999993E-05	+5.5589247E-05
82.0	3	+5.4633331E-05	+2.7061202E-06	+5.7599987E-05	+5.2299990E-05	+5.5550000E-05
84.0	3	+5.8099991E-05	+1.8187427E-06	+6.0199992E-05	+5.6599997E-05	+5.5471507E-05
85.0	3	+6.1366648E-05	+2.8358293E-06	+6.3199986E-05	+5.8099991E-05	+5.5432261E-05
86.0	3	+5.1266644E-05	+6.1239834E-06	+5.5799988E-05	+4.4299988E-05	+5.5393014E-05
87.0	12	+5.4899923E-05	+5.4743172E-06	+6.2199993E-05	+4.4599993E-05	+5.5353768E-05
88.0	9	+5.0444386E-05	+6.8172401E-06	+6.0199992E-05	+4.2799991E-05	+5.5314521E-05
89.0	21	+5.4757067E-05	+7.7618801E-06	+6.9799993E-05	+4.2999992E-05	+5.5275275E-05
90.0	9	+5.9166559E-05	+5.2093016E-06	+6.9599991E-05	+5.3399999E-05	+5.5236028E-05
91.0	6	+5.1133247E-05	+6.5578822E-06	+6.0099991E-05	+4.0599992E-05	+5.5196782E-05
93.0	3	+4.8799993E-05	+4.8661364E-06	+5.1999988E-05	+4.3199994E-05	+5.5118289E-05
94.0	9	+5.6777716E-05	+6.4687665E-06	+6.9099987E-05	+4.8999994E-05	+5.5079042E-05
95.0	12	+5.2424918E-05	+5.0811790E-06	+5.9999991E-05	+4.3899999E-05	+5.5039796E-05

ANB 3066 PROPELLANT (ALL ANB) THERMAL COEFFICIENT OF LINEAR EXPANSION (BELOW GP)

\*\*\* LINEAR REGRESSION ANALYSIS \*\*\*

\*\*\* ANALYSIS OF TIME SERIES \*\*\*

AGE (MONTHS)	SPECIMENS PER GROUP	MEAN Y	STANDARD DEVIATION	MAXIMUM Y	MINIMUM Y	REGRESSION Y
96.0	15	+5.5233263E-05	+4.8590212E-06	+6.6399996E-05	+4.4399988E-05	+5.5000549E-05
97.0	3	+5.1799986E-05	+4.2884217E-06	+5.5499986E-05	+4.7099994E-05	+5.4961303E-05
98.0	6	+5.8299978E-05	+7.5985227E-06	+6.7499990E-05	+4.9557987E-05	+5.4922056E-05
100.0	3	+5.5899989E-05	+2.8928541E-06	+5.9199999E-05	+5.3799987E-05	+5.4843563E-05
101.0	3	+5.1399983E-05	+3.7400820E-06	+5.3899988E-05	+4.7099994E-05	+5.4804317E-05
102.0	3	+5.5233322E-05	+5.4269820E-06	+6.1499988E-05	+5.2099989E-05	+5.4765070E-05
104.0	3	+6.6033317E-05	+3.9256168E-06	+6.8299996E-05	+6.1499988E-05	+5.4686577E-05
105.0	12	+5.7349883E-05	+6.3187546E-06	+6.6199994E-05	+4.8499990E-05	+5.4647331E-05
106.0	6	+5.2766641E-05	+3.6474095E-06	+5.7399985E-05	+4.6799992E-05	+5.4608084E-05
107.0	3	+5.4966658E-05	+5.6959798E-07	+5.5599986E-05	+5.4499992E-05	+5.4568838E-05
109.0	9	+5.5844371E-05	+9.0857988E-06	+6.7799992E-05	+4.2199986E-05	+5.4490345E-05
110.0	6	+5.7883284E-05	+4.2391026E-06	+6.4099993E-05	+5.2299990E-05	+5.4451098E-05
111.0	12	+5.524925E-05	+4.0103590E-06	+6.0699996E-05	+4.6999994E-05	+5.4411852E-05
112.0	3	+5.5899989E-05	+6.4466916E-06	+6.0299993E-05	+4.8499990E-05	+5.4372605E-05
113.0	15	+5.2386589E-05	+6.0595534E-06	+5.9999991E-05	+4.0299986E-05	+5.4333359E-05
114.0	3	+5.6066652E-05	+2.0029906E-06	+5.7999990E-05	+5.3599989E-05	+5.4294112E-05
115.0	6	+5.4899952E-05	+5.9822675E-06	+6.1599988E-05	+4.3999985E-05	+5.4254865E-05
116.0	6	+5.3866606E-05	+2.8020926E-06	+5.8899997E-05	+5.0299990E-05	+5.4215619E-05
117.0	9	+5.5766577E-05	+4.2585946E-06	+6.4299994E-05	+4.8099987E-05	+5.4176372E-05
118.0	15	+5.2439892E-05	+5.3291840E-06	+6.1899991E-05	+4.2099985E-05	+5.4137126E-05
119.0	3	+5.0966656E-05	+4.0266854E-07	+5.1199996E-05	+5.0499991E-05	+5.4097879E-05
121.0	1	+6.0099991E-05	+0.0000000E+00	+6.0099991E-05	+6.0099991E-05	+5.4019386E-05
122.0	3	+5.7699988E-05	+3.4043063E-06	+6.0999998E-05	+5.4199990E-05	+5.3980140E-05
123.0	9	+5.9555488E-05	+3.6383637E-06	+6.4299994E-05	+5.3499999E-05	+5.3940893E-05
124.0	6	+6.0683261E-05	+1.5181951E-06	+6.2799997E-05	+5.8299992E-05	+5.3901647E-05
126.0	6	+5.9733283E-05	+2.4770897E-06	+6.3299987E-05	+5.6399992E-05	+5.3823154E-05
127.0	3	+5.8699981E-05	+3.1605510E-06	+6.1999991E-05	+5.5699987E-05	+5.3783907E-05
137.0	9	+5.3522147E-05	+5.4206517E-06	+6.1999991E-05	+4.4099986E-05	+5.3391442E-05

ANB 3066 PROPELLANT (ALL ANB) THERMAL COEFFICIENT OF LINEAR EXPANSION (BELOW GP)



SECTION VIII  
CASE LINER BONDS

Cartons of propellant were lined with SD-851-2 liner/V-45 rubber. In the preparation of these cartons there are marked irregularities in the liner with the liner frequently penetrating up to 0.3" into the propellant. Moreover, some of these liners are pink with varying degrees of tackiness while others are buff colored and usually with little tackiness.

Two reports (MANCP Report Nr. 357(76) and ASPC Report 0162-06SAAS-15, Addendum 1, April 1976) detail a cooperative study on several cartons which had this problem. In this report ANB and ANT cartons of several ages have been combined to obtain time to failure (Table 8-1). The stress to cause failure at 100 minutes is well above the alert limit for storage for both constant load tensile and constant load shear. Plots are shown in Figures 8-1 thru 8-4. All show a significant decrease. It may be possible in the next report to do lot analyses to pinpoint those lots in which early failure may occur.

TABLE 8-1

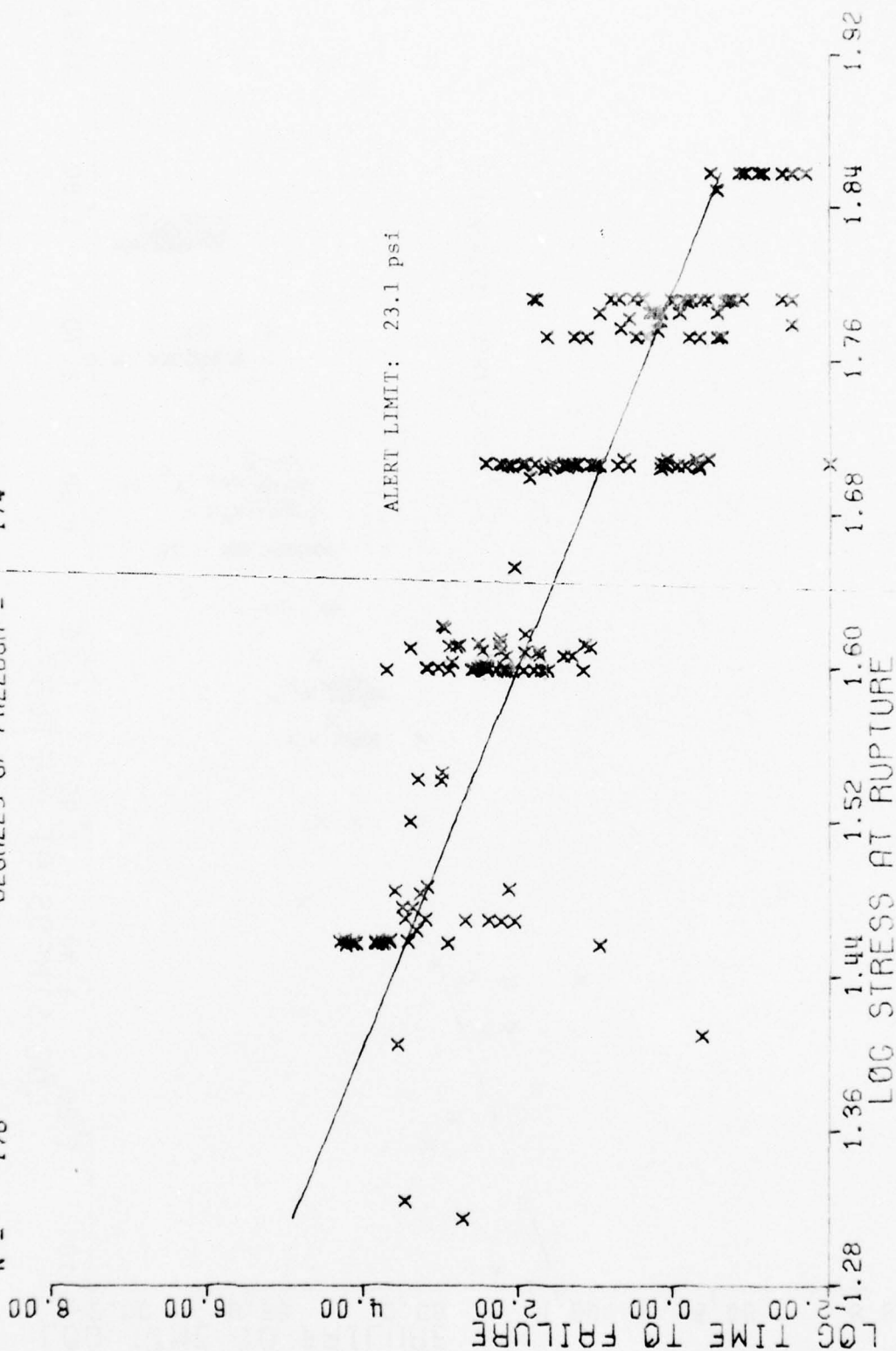
## SUMMARY OF REGRESSION ANALYSIS, STRESS VS TIME TO FAILURE

Test	Proplnt Type	Intercept		Slope		Std(1) error s <sub>yx</sub>	Correl Coeff.	Nr of Spec	Mean		Predicted Stress To Cause Failure		95% Confidence Limits		Mean		95% Confidence Limits	
		Mean a	Std Dev a	Mean b	Std Dev b				95% CI	95% CI	UL	LL	UL	LL	95% CI	95% CI	UL	LL
Constant Load Tensile	ANB	18.308	0.868	-10.177	0.522	0.874	-0.828	176	69.951	130.230	58.942	40.038	52.369	23.760				
	ANT	17.649	0.936	-9.356	0.529	0.930	-0.828	145	76.980	163.010	65.130	47.057	60.495	24.198				
Constant Load Shear	ANB	12.282	0.375	-7.496	0.229	0.498	-0.906	234	43.504	60.857	33.120	23.535	17.807	9.651				
	ANT	12.583	0.548	-7.469	0.332	0.438	-0.888	137	48.395	69.262	40.391	26.122	20.162	11.666				

Regression Model:  $\log(\text{time to failure}) = a + b(\log \text{ stress, psi})$ 

(1) Std error stated in terms of log time since time is dependent variable

$\text{LOG (Y)} = ((+1.8307735\text{E}+01) + (-1.0176585\text{E}+01) * \text{LOG (X)})$   
 $F = +3.7945674\text{E}+02$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = -8.2801708\text{E}-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +1.9479649\text{E}+01$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 176$  DEGREES OF FREEDOM = 174



ANB CONSTANT LOAD TENSILE LOG TIME TO FAILURE VS LOG STRESS AT RUPTURE

Figure 8-1

$\text{LOG } (Y) = ( (-7.4957068E+00) + (1.2281972E+01) ) + ( -7.4957068E+00 ) * \text{LOG } (X)$   
 $F = +1.0655816E+03$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = -9.0620409E-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +3.2643248E+01$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 234$  DEGREES OF FREEDOM = 232

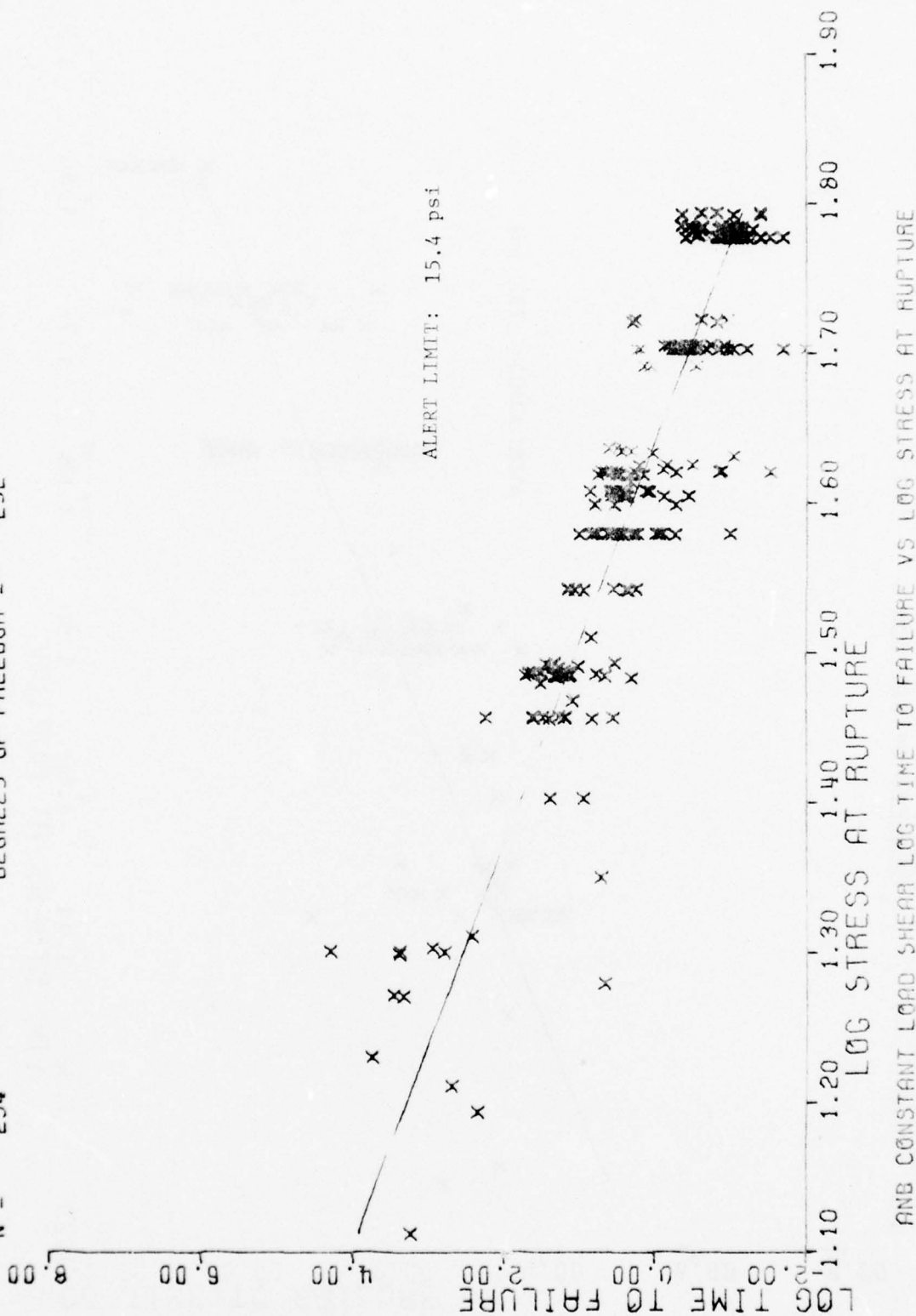


Figure 8-2



$\text{LOG}(Y) = [(+1.7649601E+01) + (-9.3563413E+00)] \times \text{LOG}(X)$   
 $F = +3.1228631E+02$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = -8.2819800E-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +1.7671624E+01$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 145$  DEGREES OF FREEDOM = 143

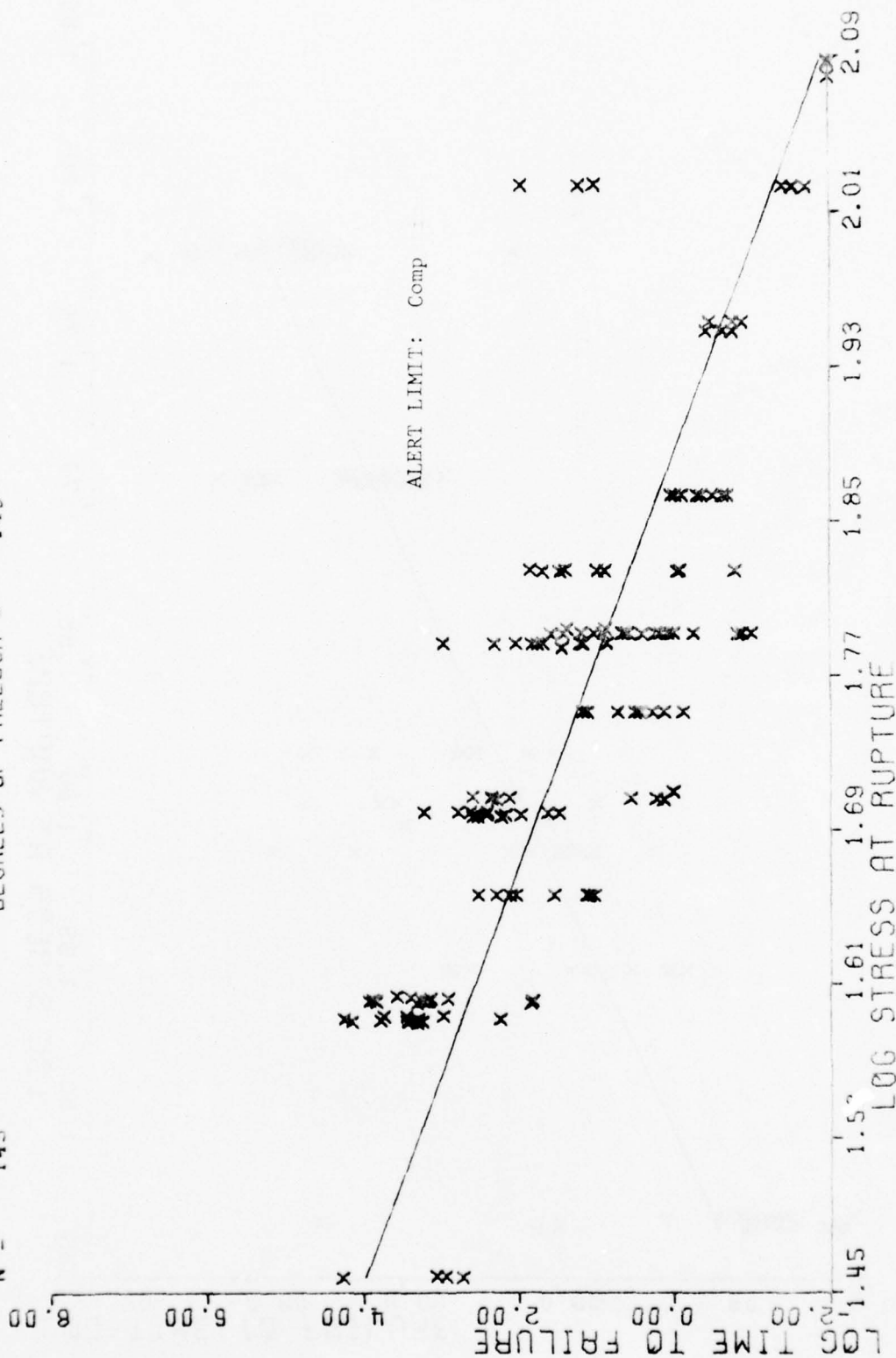


Figure 8-3

$\text{LOG (Y)} = ((+1.2583084\text{E}+01) + (-7.4685835\text{E}+00)) \times \text{LOG (X)}$   
 $F = +5.0525531\text{E}+02$  SIGNIFICANCE OF F = SIGNIFICANT  
 $R = -8.8833924\text{E}-01$  SIGNIFICANCE OF R = SIGNIFICANT  
 $t = +2.2477885\text{E}+01$  SIGNIFICANCE OF t = SIGNIFICANT  
 $N = 137$  DEGREES OF FREEDOM = 135

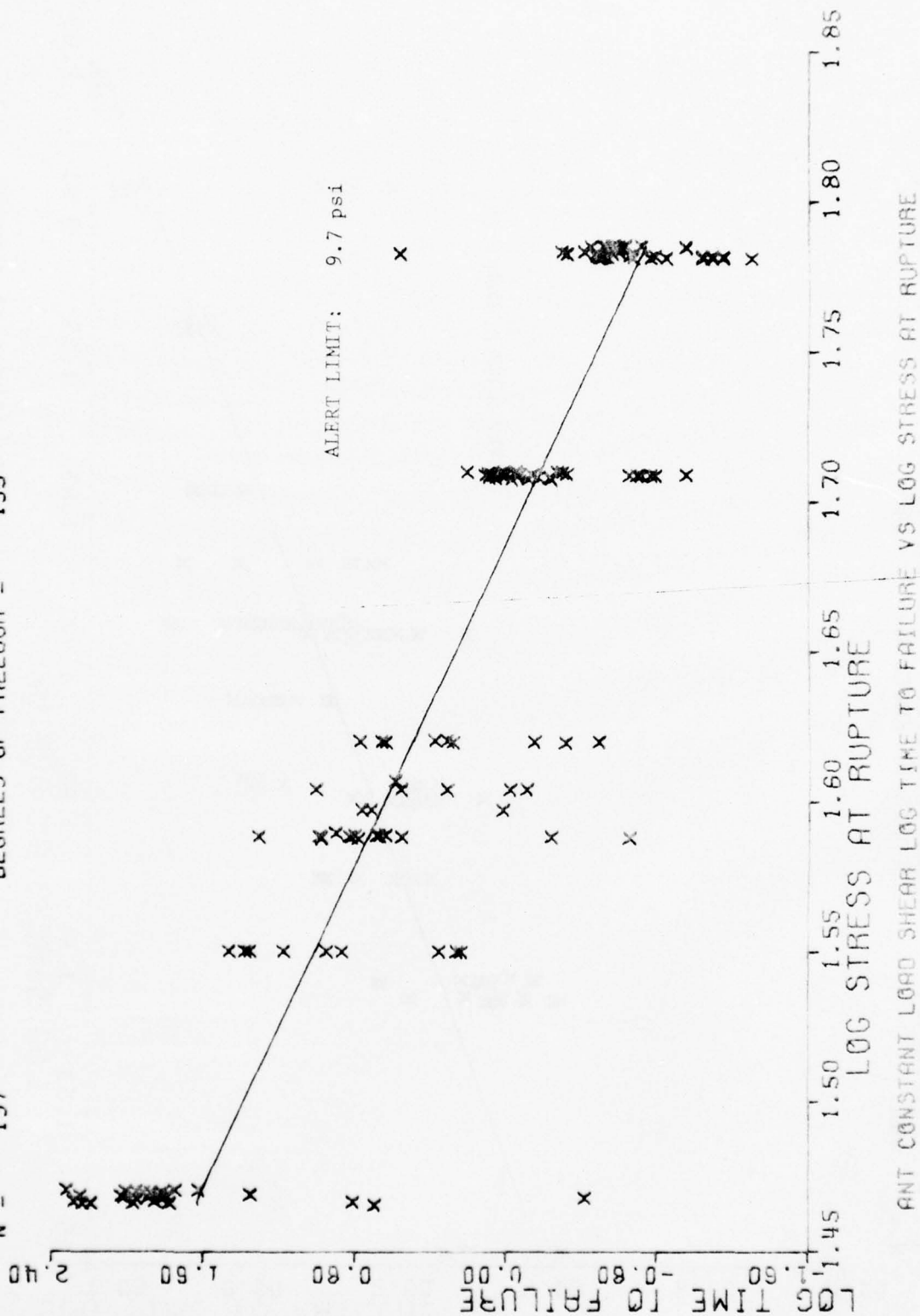


Figure 8-4

APPENDIX  
ANALYSIS OF COVARIANCE

The results of the analysis of covariance as described in Section III are summarized in Table A-A. The number in each block refer to the table number of each analysis. The tables show the specific F ratio and an associated degrees of freedom for each statistical test conducted.

TABLE A-A

ANALYSIS OF COVARIANCE  
SUMMARY OF SIGNIFICANCE

Propellant Group	VLR Tensile		HR Triax Tensile				Stress Relax		TCLE	
	Sm	er	E	Sm	er	E	E <sub>10</sub>	1% Strain E <sub>1000</sub>	TCLE Above	Glass Point
ANT(Lined) vs ANT(Unlined)	1 Sig	2 Sig	3 Sig	28 Sig	29 Sig	30 Sig	55 Sig	56 Sig	69 Sig	70 Sig
ANB(Lined) vs ANT(Lined)	4 Sig	5 Sig	6 N.S.	31 Sig	32 Sig	33 Sig	57 Sig	58 Sig		
ANA(Unlined) vs ANB(Unlined)	7 Sig	8 Sig	9 Sig	34 Sig	35 Sig	36 Sig	59 Sig	60 Sig	71 Sig	72 Sig
ANA(Unlined) vs ANB(Unlined) vs ANT(Unlined)	10 Sig	11 Sig	12 Sig	37 Sig	38 Sig	39 Sig	61 Sig	62 Sig	73 Sig	74 Sig
ANB(Lined) Lot to Lot	13 Sig	14 Sig	15 Sig	40 Sig	41 Sig	42 Sig				
ANT(Lined) Lot to Lot	16 Sig	17 Sig	18 Sig	42 Sig	44 Sig	45 Sig	63 Sig	64 Sig		
ANA(Unlined) Lot to Lot	19 Sig	20 Sig	21 Sig	46 Sig	47 Sig	48 Sig	65 Sig	66 Sig		
ANB(Unlined) Lot to Lot	22 Sig	23 Sig	24 Sig	49 Sig	50 Sig	51 Sig				
ANT(Unlined) Lot to Lot	25 Sig	26 Sig	27 Sig	52 Sig	53 Sig	54 Sig	67 Sig	68 Sig		

Blanks - Data not available for covariance analysis.



TABLE A-1

## ANALYSIS OF COVARIANCE TABLE

CORRECTED SUMS OF SQUARES AND PRODUCTS				DEVIATIONS ABOUT REGRESSION			REGRESSION COEFFICIENT
SOURCE	DF	X	XY	Y	SS	AS	
UNLINED	323	46052.4375	18665.4375	24775.0000	17209.7422	52.4464	0.4052062E+01
LINED	77	5317.4375	1109.8125	4067.1250	3865.4932	50.0723	0.2087114E+01
WITHIN	400	51369.8750	19775.2500	28812.1250	21199.4644	52.1315	0.3845560E+01
AMONG	1	4153.1250	3569.7500	3065.8750	2.4424	0.0000	0.0000000E+00
TOTAL	401	55523.0000	23345.0000	31878.0000	22062.4453	55.1561	0.0000000E+00
F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.4894 DF = 1 390							
F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 16.2420 DF = 1 399							
F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 143.2791 DF = 1 399							

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.4294 DF = 1, 398  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 16.2420 DF = 1, 399  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 143.2791 DF = 1, 399

ANT LINED VS UNLINED CARTONS VLR TESTSILE 77 DEG F, 0.0002 IN/MIN, MAXIMUM STRESS

TABLE A-2

## ANALYSIS OF COVARIANCE TABLE

CORRECTED			DEVIATIONS			ABOUT REGRESSION		REGRESSION	
SUMS OF SQUARES AND PRODUCTS			COEFFICIENT						
SOURCE	DF	X	XY	Y	SS	SS	AS		
UNLINE	320	0.460124E+00	0.220680E+02	0.118772E+00	0.104305E+00	0.223920E+00	0.453356E-02		
LITERO	77	0.531704E+00	0.270657E+01	0.100000E+00	0.152504E+01	0.200000E+00	0.514641E-02		
WITFIN	400	0.513699E+00	0.101436E+02	0.130432E+00	0.124023E+00	0.310000E+00	0.552154E-02		
AMONG	1	0.415312E+00	0.216600E+01	0.118097E+00	0.534057E+00	0.000000E+00	0.521068E-02		
TOTAL	401	0.555230E+00	0.203076E+02	0.131664E+00	0.124157E+00	0.210341E+00	0.565712E-02		

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 14.8712 DF = 1, 390  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 0.3456 DF = 1, 399  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 20.6181 DF = 1, 399

AMT LINE1 VS CALLED CANYONS VLN TELSILE 77 DEG F 0000 IN/MIN. STRAIN AT RUPTURE

TABLE A-3

## ANALYSIS OF COVARIANCE TABLE

SOURCE		X		Y		XY		DEVIATIONS		ABOUT REGRESSION		REGRESSION	
DF								SS	DF	SS	MS	COEFFICIENT	
1	323	0.460524E+04	0.152955E+06	0.316557E+07	322	0.737153E+07	0.795548E+04	0.332138E+01					
1	77	0.531794E+04	0.266750E+06	0.421081E+06	76	0.240628E+06	0.648165E+04	0.366150E+01					
1	400	0.517595E+04	0.175633E+06	0.69750E+07	399	0.290265E+07	0.727741E+04	0.338051E+01					
1	1	0.415230E+04	0.246990E+06	0.342890E+06	0	0.352100E+02	0.000000E+00	0.000000E+00					
1	401	0.555250E+04	0.196231E+06	0.383747E+07	400	0.292902E+07	0.732154E+04	0.300000E+01					

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.2101 DF = 1, 399  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 3.4406 DF = 1, 399  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 61.6453 DF = 1, 399

ANY LINE VS UNLINED CARBONS VSR TENSILE 77 DEG F, 0.0002 IN/MIN, MODULUS

TABLE A-4

## ANALYSIS OF COVARIANCE TABLE

CORRECTED			DEVIATIONS			ABOUT REGRESSION			REGRESSION		
SUMS OF SQUARES AND PRODUCTS			Y			SS			AS		
SOURCE	DF	X	XY	Y	DF	SS	AS	RECOEFFICIENT	DF	AS	RECOEFFICIENT
ALL	127	0.166869E+05	0.357937E+04	0.506194E+04	126	0.429415E+04	0.340606E+02	0.2145024E+00	202	0.340606E+02	0.2145024E+00
ATTN	77	0.531744E+04	0.110969E+04	0.403567E+04	76	0.320430E+04	0.500565E+02	0.2086854E+00	203	0.500565E+02	0.2086854E+00
ATTHN	204	0.226044E+05	0.468906E+04	0.905791E+04	203	0.409859E+04	0.398945E+02	0.2130974E+00	203	0.398945E+02	0.2130974E+00
AMONG	1	0.634212E+07	0.519062E+03	0.124672E+03	0	-0.650625E-01	0.000000E+00	0.8183072E+00	203	0.000000E+00	0.8183072E+00
TOTAL	205	0.226389E+05	0.520812E+04	0.952050E+04	204	0.832434E+04	0.406056E+02	0.230054E+00	203	0.406056E+02	0.230054E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.0036 DF = 1, 202  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 5.6588 DF = 1, 203  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 25.0466 DF = 1, 203

ALL VS ATT LINED CARTONS VLR TENSILE 77 DEG F, .0002 IN/MIN, MAXIMUM STRESS



TABLE A-5

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS		COVARIANCES		ELEVATIONS ABOUT REGRESSION		MS		REGRESSION COEFFICIENT	
		X	XY	Y	Y <sup>2</sup>	SS	SS	MS	MS	COEFFICIENT	COEFFICIENT
ANO	127	0.168689E+05	-0.112332E+02	0.558455E-01	126	0.482834E-01	0.383202E-03			-0.573173E-02	
ANT	77	0.531744E+03	-0.273779E+01	0.466557E-01	76	0.256364E-02	0.337521E-14			-0.514870E-02	
ITHT	204	0.220043E+05	-0.135709E+02	0.725150E-01	203	0.636348E-01	0.312471E-03			-0.634916E-02	
AVG	1	0.634125E+03	-0.502262E+00	0.147720E-02	0	0.212221E-06	0.700000E+00			-0.1526474E-02	
TOTAL	205	0.225366E+05	-0.149392E+02	0.739732E-01	204	0.641248E-01	0.314337E-03			-0.659299E-02	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 50.8010 DF = 1, 202  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 1.5639 DF = 1, 203  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 28.2974 DF = 1, 204

ANO VS ANT LINED CARTONS VLR TENSILE 77 DEG F, .0002 IN/IN, STRAIN AT RUPTURE

TABLE A-6

## ANALYSIS OF COVARIANCE TYPE

SOURCE	DF	CORRECTED SUMS OF SQUARES AND PRODUCTS			DEVIATIONS ABOUT REGRESSION			AS	REGRESSION COEFFICIENT
		X	XY	Y	SS	DF	SS		
ME	122	0.140283E+05	0.457890E+05	0.865560E+06	0.701783E+06	121	0.579966E+04	0.3357657E+01	
RET	77	0.523744E+04	0.206750E+05	0.420922E+06	0.340604E+06	76	0.445164E+04	0.3882150E+01	
WITHIN	199	0.203457E+05	0.704640E+05	0.128555E+07	0.104249E+07	198	0.527015E+04	0.3497710E+01	
ANALG	1	0.772312E+03	0.619500E+04	0.456102E+05	.123261E+02	0	0.00000E+00	0.6021262E+01	
TOTAL	200	0.205181E+05	0.766590E+05	0.133563E+07	0.105670E+07	199	0.532109E+04	0.3664727E+01	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.2081 DF = 1, 197  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 2.6857 DF = 1, 198  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 46.7458 DF = 1, 199

AMB VS ALT LINED CARBONS VLR TENSILE 77 DEG F, .0002 IN./MIN. MODULUS

TABLE A-7

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS				REGRESSION COEFFICIENT
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				
SOURCE	DF	X	XY	Y	LF	SS	NS	
ANA	271	97048.0000	8510.8125	10114.0000	270	9367.6250	34.6949	0.07694512+01
APR	1631	444191.0000	53146.0000	108951.0000	1630	100592.2500	61.7130	0.11984672+00
WITHIN	1902	541239.0000	61656.8125	117065.0000	1901	110041.1875	57.8859	0.11391792+00
AMONG	1	48682.0000	-927.8125	20.0000	0	2.3172	0.0000	0.00000000+00
TOTAL	1903	589921.0000	60729.0000	117085.0000	1902	110633.2512	58.2720	0.00000007+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.4050 DF = 1, 1900  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 13.8837 DF = 1, 1501  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 121.3386 DF = 1, 1501

ANA VS APR UNLINED CARTONS VLR TENSILE 77 DEG F, 0.0002 IN/MIN, MAXIMUM STRESS

TABLE A-8

## ANALYSIS OF COVARIANCE TABLE

CORRECTED SUMS OF SQUARES AND PRODUCTS				DEVIATIONS ABOUT REGRESSION				REGRESSION COEFFICIENT	
SOURCE	DF	X	XY	Y	CF	SS	MS		
ANA	271	97048.0000	3.0476	0.0762	270	0.0781	0.0003	0.3140001E-04	
ARB	1633	444301.0000	91.7576	0.9269	1632	0.9379	0.0006	0.2065200E-03	
WITHIN	1904	541349.0000	94.8054	1.0052	1903	0.9886	0.0005	0.1751300E-03	
AMONG	1	48754.0000	-9.9265	0.0021	0	0.0001	0.0000	0.0000000E+00	
TOTAL	1905	590103.0000	84.8789	1.0072	1904	0.9950	0.0005	0.0000000E+00	

\* RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 4.9042 DF = 1, 1902

# RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 12.3084 DF = 1, 1905

§ RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 31.9601 DF = 1, 1903

ANA VS ANB UNLINED CARTONS VLR TENSILE 77 DEG F 0.0002 IN/MIN, STRAIN AT RUPTURE



TABLE A-9

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS				REGRESSION COEFFICIENT
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				
SOURCE	DF	X	XY	Y	LF	SS	AS	
ANA	271	5704.8000	3347.5996	136926.0000	270	127761.2500	510.2009	
ANB	1625	44448.2031	4329.5996	2040576.0000	1624	2040154.0000	1248.5640	
WITHIN	1906	54153.0000	7677.1992	2179512.0000	1905	2176423.0000	1143.5268	
AMONG	1	4877.0996	5209.1992	5576.0000	0	12.0898	0.0000	
TOTAL	1907	59030.0937	12866.3984	2155063.0000	1906	2182274.0000	1144.5492	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.4266 DF = 1, 1904  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 3.3676 DF = 1, 1905  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 0.9518 DF = 1, 1905

ANA VS ANB UNLINED CARTONS VLR TENSILE 77 DEG F 0.0002 IN/MIN. OCULUS

TABLE A-10

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS		CORRECTED		DEVIATIONS		REGRESSION	
		X	XY	Y	CF	SS	MS	COEFFICIENT	
ATA	271	97046.0000	8510.6250	10115.0000	270	5366.6602	34.6913	0.8769500E+01	
ATP	1631	444191.0000	55146.0000	106951.0000	1630	100592.2500	61.7130	0.1196467E+00	
AT	323	48052.4375	18665.4375	24776.0000	322	17210.7422	53.4495	0.4053002E+00	
WITHIN	2225	587291.5000	80322.0625	141840.0000	2224	131654.5937	58.8375	0.1367269E+00	
AMONG	2	65975.5625	5111.9375	2131.0000	1	1734.9150	1734.9150	0.0000000E+00	
TOTAL	2227	653267.0000	85434.0000	143971.0000	2226	132797.9375	59.6577	0.0000000E+00	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 32.1932 DF = 2, 2224  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 16.5145 DF = 2, 2224  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 186.7074 DF = 1, 2224

ATA VS APB & AT UNLINED CARTONS VLA TENSILE 77 DEG F 0.0002 IN/MIN, MAX STRESS

TABLE A-11

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	Sums of Squares and Products		Corrected		Deviations About Regression		Regression Coefficient	
		X	XY	Y	YY	SS	AS	AS	AS
ANAL	271	0.370480E+05	0.304907E+01	0.702509E-01	270	0.701551E-01	0.289453E-03	0.314381E-04	
ANB	1633	0.444301E+05	0.923516E+02	0.925735E+00	1632	0.904535E+00	0.555478E-03	0.207258E-02	
ANT	323	0.450524E+05	0.266795E+02	0.113773E+00	322	0.104307E+00	0.323933E-03	0.453393E-02	
TTTTL	2275	0.875014E+05	0.116201E+03	0.111775E+01	2274	0.913058E+00	0.422502E-03	0.197857E-02	
ANCLG	2	0.650936E+05	0.667964E+01	0.163545E-01	1	0.176764E-01	0.176764E-01	0.104059E-03	
TOTAL	2229	0.653495E+05	0.123160E+03	0.113115E+01	2228	0.111294E+01	0.699525E-03	0.188463E-03	

\*\*\*\*\*

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 5.1441 DF = 50, 2224  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 7.5937 DF = 46, 2274  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 365.2860 DF = 1, 2274

ANAL VS ANB/ANT UNLINED CARTONS VLF TENSILE 77 DEG F .0002 IN/MIN, SIN AT RUPTURE





TABLE A-13

## ANALYSIS OF COVARIANCE TABLE

CORRELATED  
SLOpes AND ELEVATIONS  
ABOUT REGRESSION

SOURCE	DF	X	XY	Y	DF	SS	MS	REGRESSION COEFFICIENT
100	11	0.39766E+04	0.67550E+03	0.22924E+03	10	0.21241E+02	0.21241E+02	0.1732159E+01
150	14	0.35564E+04	0.25265E+03	0.33900E+03	13	0.315153E+03	0.242710E+02	0.14260E+01
150	11	0.31681E+03	0.20709E+03	0.22940E+03	10	0.159241E+03	0.159241E+02	0.7599139E+01
050	11	0.25191E+03	0.22725E+03	0.25711E+03	10	0.160293E+03	0.160293E+02	0.622745E+01
050	11	0.93246E+03	0.382483E+03	0.37510E+03	10	0.217474E+03	0.217474E+02	0.40974E+01
045	5	0.13506E+02	0.51371E+02	0.203217E+03	4	0.13654E+01	0.203413E+01	0.26022E+01
157	5	0.16200E+03	0.11149E+03	0.11105E+03	7	0.435004E+02	0.621435E+01	0.12615E+01
061	5	0.13500E+02	0.27460E+02	0.51328E+02	4	0.92733E+01	0.231633E+01	0.203414E+01
063	5	0.37000E+01	0.11367E+03	0.44331E+03	4	0.26110E+02	0.657775E+01	0.33131E+01
17077	21	0.922679E+09	0.202991E+04	0.256642E+04	20	0.209410E+04	0.261763E+02	0.225642E+01
17077	8	0.45160E+01	0.67000E+03	0.264016E+03	7	0.216967E+03	0.309582E+02	0.600000E+01
TOTAL	49	0.137956E+05	0.295000E+04	0.254151E+04	60	0.231421E+04	0.262979E+02	0.600000E+01

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 7.3583 DF = 8, 72  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 1.0511 DF = 8, 30  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 17.9E73 DF = 1, 30

AND THE CLOSURE TO-TO-CT VON MISES MAX STRESS, 0.0002 IN/MIN, 77 DEG F

TABLE A-14

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	Sums of Squares and Products		Y	DF	REGRESSIONS		MS	REGRESSION COEFFICIENT
		SS	SP			SS	SP		
1	1	0.098223E+04	-2.44471E+00	0.022127E-03	10	0.71165E-03	0.78208E-14	-	0.941030E-04
2	1	0.35448E+04	-0.31531E+01	0.71224E-02	10	0.40595E-02	0.73728E-13	-	0.717520E-04
3	1	0.31256E+03	-0.13731E+01	0.02542E-02	10	0.21924E-02	0.21932E-13	-	0.40740E-04
4	1	0.49191E+03	-0.77524E+00	0.01132E-02	10	0.53170E-03	0.53070E-14	-	0.267759E-04
5	1	0.93661E+03	-0.42053E+00	0.05510E-02	10	0.35113E-02	0.35113E-13	-	0.84556E-04
6	5	0.13500E+02	-0.67169E-01	0.07045E-03	4	0.32263E-04	0.60658E-15	-	0.20125E-04
7	5	0.15200E+03	-0.77345E+00	0.01753E-02	7	0.14210E-02	0.20312E-13	-	0.02045E-04
8	5	0.12500E+03	0.74249E-01	0.08920E-03	4	0.11130E-03	0.45240E-04	-	0.542554E-04
9	5	0.37500E+03	0.22226E+00	0.19010E-02	4	0.44143E-03	0.11535E-13	-	0.219204E-04
10	5	0.92874E+04	-0.64174E+01	0.27704E-01	80	0.26269E-01	0.29086E-13	-	0.691020E-04
11	5	0.45000E+03	-0.05591E+01	0.04400E-01	7	0.99544E-02	0.14224E-12	-	0.00010E-04
12	5	0.10755E+03	-0.10755E+02	0.02212E-01	80	0.33329E-01	0.36112E-13	-	0.00000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 6.5011 DF = 8, 72  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 4.4133 DF = 8, 80  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 15.2461 DF = 1, 80

ADJ. MS. CT. 5 LOT-TC-LOT VLS. TULSILE STA. AT RUPTURE, 0.0002 10/2/10, 77 085 F



TABLE A-16

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED SUMS OF SQUARES AND PRODUCTS			DEVIATIONS ABOUT REGRESSION			REGRESSION COEFFICIENT
		X	XY	Y	DF	SS	AS	
711	11	435.0000	342.5391	1238.6523	10	968.9214	96.8521	0.7874460E+00
712	11	212.0000	-43.7930	106.7383	10	100.5914	10.0591	-.1403620E+00
713	11	350.2500	2.1992	98.3125	10	98.2987	9.8299	0.6276990E+00
819	11	824.2500	676.7109	661.1836	10	105.6028	10.5603	0.8210020E+00
820	11	726.2500	273.0742	177.7422	10	75.3467	7.5347	0.3749732E+00
821	5	1.5000	-0.9220	39.4375	4	38.8708	9.7177	-.6145837E+00
823	5	1.5000	3.2656	15.8047	4	8.6953	2.1738	0.2177087E+01
824	5	13.5000	30.6750	126.9375	4	56.3253	14.0813	0.2287637E+01
WITHIN	70	2666.2500	1283.9492	2464.8086	69	1846.5151	26.7611	0.0000000E+00
AMONG	7	2651.1875	-174.0117	1566.3769	6	1556.9575	259.4929	0.0000000E+00
TOTAL	77	5317.4375	1109.9375	4033.1875	76	2801.5039	50.0198	0.0000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.4015 DF = 7, 62  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 10.4362 DF = 7, 69  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 23.1042 DF = 1, 69

ANT LINED CARTONS VLR TENSILE 77 DEG F, 0.0002 IN/MIN, LOT-10-LOT MAXIMUM STRESS



TABLE A-17

## ANALYSIS OF COVARIANCE TABLE

SOURCE		CORRECTED		SUMS OF SQUARES AND PRODUCTS		DEVIATIONS		ABOUT REGRESSION		REGRESSION	
DF	X	Y	XY	SS	SS	MS	COEFFICIENT				
711	11	0.43500E+03	-0.66868E+00	0.243102E-02	10	0.135573E-02	0.135573E-03	-	0.1576074E-03		
712	11	0.31200E+03	-0.147552E+00	0.467777E-03	10	0.467777E-03	0.467777E-04	-	0.4725242E-04		
713	11	0.350250E+03	0.617371E-04	0.764954E-03	10	0.774051E-03	0.774051E-04	0.	0.1762857E-03		
715	11	0.000250E+03	-0.113600E+00	0.000000E-02	10	0.750000E-03	0.750000E-04	-	0.1454455E-02		
820	11	0.728250E+03	-0.767869E+00	0.981331E-03	10	0.283715E-03	0.283715E-04	-	0.1013209E-02		
824	5	0.135000E+02	0.268480E-01	0.506222E-03	4	0.452825E-03	0.113206E-03	0.	0.1988796E-02		
WITHIN	60	0.265325E+04	-0.254937E+01	0.771511E-02	59	0.627475E-02	0.094025E-04	-	0.9572897E-03		
AMONG	5	0.213584E+04	-0.295358E+00	0.606053E-02	4	0.602350E-02	0.150567E-02	-	0.1389367E-03		
TOTAL	65	0.477909E+04	-0.284473E+01	0.137796E-01	64	0.120899E-01	0.188904E-03	-	0.5940000E-03		

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.1781 DF = 5, 54  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 15.2459 DF = 5, 59  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 27.2963 DF = 1, 59

ACT LINED CAPTIONS 101-10-101 VLR 777511E 77 DEG F .0002 16/MIN, SIPAIN AT EPIURE

TABLE A-18

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS		CORRELATED		DEVIATIONS ABOUT REGRESSION		REGRESSION COEFFICIENT	
		X	XY	Y	LF	SS	MS		
711	11	0.43500E+03	0.334800E+04	0.276640E+05	10	0.189595E+04	0.189594E+03	0.769655E+01	
712	11	0.31200E+03	0.51400E+03	0.899700E+04	11	0.614022E+04	0.614021E+03	0.164743E+01	
713	11	0.350250E+03	0.113075E+04	0.306600E+05	10	0.267910E+05	0.267918E+04	0.339971E+01	
819	11	0.322250E+03	0.756800E+04	0.650750E+05	10	0.776419E+04	0.776419E+03	0.368180E+01	
820	11	0.728250E+03	0.549850E+04	0.822140E+05	10	0.207667E+05	0.207667E+04	0.755029E+01	
824	5	0.12500E+02	0.12000E+03	0.159400E+04	4	0.527333E+03	0.131833E+03	0.688688E+01	
WITHIN	60	0.266325E+04	0.166572E+05	0.214448E+06	59	0.837457E+05	0.141942E+04	0.700544E+01	
AMONG	5	0.212584E+04	0.329231E+04	0.482400E+05	4	0.431412E+05	0.107653E+05	0.154870E+01	
TOTAL	65	0.478909E+04	0.219496E+05	0.262888E+06	64	0.162068E+06	0.253262E+04	0.458323E+01	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.3701 DF = 5, 54

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 11.0386 DF = 5, 59

F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 92.0815 DF = 1, 59

ALT LINE1 CTNS 101-10-101 VLR TENSILE .0002 IN/IN 77 DFG, F, MODULUS

TABLE A-19

## ANALYSIS OF COVARIANCE TABLE

CORRELATIONS ABOUT REGRESSION													
CORRECTED SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				REGRESSION COEFFICIENT					
SOURCE	DF	X	X1	Y	DE	SS	AS						
141	143	0.193989E+04	0.803562E+03	0.402587E+04	142	0.369701E+04	0.260353E+02	0.414230E+00					
142	14	0.510000E+03	0.222199E+03	0.347312E+03	13	0.188046E+03	0.146511E+02	0.718771E+00					
143	14	0.143366E+03	0.154367E+03	0.042537E+03	13	0.176890E+03	0.135915E+02	0.107456E+01					
144	12	0.980359E+03	0.041250E+03	0.100522E+04	12	0.115524E+03	0.882713E+01	0.360107E+00					
145	13	0.924930E+03	0.529812E+03	0.100156E+04	12	0.768394E+02	0.640328E+01	0.394526E+00					
146	13	0.161521E+04	0.881250E+02	0.105125E+03	12	0.100504E+03	0.837534E+01	0.536532E+01					
147	21	0.206300E+04	0.349312E+03	0.382875E+03	20	0.324296E+03	0.162148E+02	0.167696E+00					
148	18	0.656738E+03	0.232375E+03	0.309250E+03	17	0.227628E+03	0.133546E+02	0.353631E+00					
149	249	0.865347E+04	0.294552E+04	0.752856E+04	248	0.652555E+04	0.263143E+02	0.340385E+00					
150	7	0.842202E+03	0.620017E+04	0.236644E+04	6	0.190995E+04	0.218332E+03	0.736165E+01					
151	256	0.925737E+03	0.514569E+04	0.980503E+04	255	0.759438E+04	0.352721E+02	0.984744E+01					

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 11.4586 DF = 7, 241  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 13.4006 DF = 7, 248  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 38.1014 DF = 1, 249

ANA UNLND CARTONS LOT-10-LOT 10R TESTILE 77 DEG F .0002 IN/MIN, MAXIMUM STRESS

TABLE A-20

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		SUMS OF SQUARES AND PRODUCTS		DEVIATIONS ABOUT REGRESSION		MS	REGRESSION COEFFICIENT
		X	XY	Y	LF	SS	SS		
M41	143	0.192989E+04	0.498779E+00	0.366180E-01	142	0.268606E-01	0.257469E-03	0.257117E-02	0.257117E-02
M42	14	0.310000E+03	0.180511E-01	0.155240E-02	13	0.155135E-02	0.119335E-03	0.119335E-03	0.682295E-04
M50	14	0.143333E+03	0.100372E+00	0.167477E-02	13	0.160448E-02	0.123422E-03	0.123422E-03	0.700259E-02
E36	13	0.313350E+02	0.111507E+01	0.291173E-02	12	0.264122E-02	0.220685E-03	0.220685E-03	0.113740E-02
E37	13	0.924930E+03	0.662369E+00	0.180423E-02	12	0.156496E-02	0.111247E-03	0.111247E-03	0.706469E-02
E38	13	0.160521E+04	-0.253769E+00	0.597125E-02	12	0.393613E-02	0.328176E-03	0.328176E-03	0.158090E-03
E40	21	0.208300E+04	0.347783E+01	0.952215E-02	20	0.371649E-02	0.185824E-03	0.185824E-03	0.166962E-02
E44	18	0.656738E+03	-0.130763E+01	0.368887E-02	17	0.108524E-02	0.632379E-04	0.632379E-04	-0.199110E-02
WITHIN	249	0.865347E+04	0.431107E+01	0.628270E-01	243	0.606793E-01	0.244674E-03	0.244674E-03	0.498189E-02
BETWEEN	7	0.842202E+03	-0.923126E+00	0.131799E-01	6	0.131691E-01	0.219496E-02	0.219496E-02	-0.105608E-04
TOTAL	256	0.928737E+05	0.336794E+01	0.760069E-01	255	0.758633E-01	0.297582E-03	0.297582E-03	0.364789E-04

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 5.4098 DF = 7, 241  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 8.8771 DF = 7, 248  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 8.7779 DF = 1, 248

ANA UNLND CAPTURS 101-10-101 VLR TENSILE 77 DEG F .0002 IN/MIN, STRAIN AT RPTURE



TABLE A-21

## ANALYSIS OF COVARIANCE TABLE

SUMS OF SQUARES AND PRODUCTS									
DEVIATIONS									
ABOUT REGRESSION									
SOURCE	DF	X	XY	Y	SS	SS	MS	REGRESSION COEFFICIENT	
B41	143	0.193929E+04	0.519000E+04	0.609128E+06	142	1.794242E+06	0.559326E+04	0.267540E+01	0.267540E+01
B42	14	0.310000E+03	0.104500E+04	0.323240E+05	13	0.200013E+05	0.221549E+04	0.337096E+01	0.337096E+01
B43	14	0.143336E+03	-0.856625E+03	0.296750E+05	13	0.245555E+05	0.188889E+04	-0.597634E+01	-0.597634E+01
B44	13	0.980350E+03	0.295615E+04	0.480190E+05	12	0.350945E+05	0.332457E+04	0.601541E+01	0.601541E+01
B47	13	0.934930E+03	0.546769E+04	0.785160E+05	12	0.405397E+05	0.387051E+04	0.584923E+01	0.584923E+01
B48	13	0.160521E+04	0.522394E+04	0.611770E+05	12	0.547020E+05	0.455050E+04	0.200341E+01	0.200341E+01
B49	21	0.209200E+04	0.376069E+04	0.967450E+05	20	0.899554E+05	0.449777E+04	-0.180541E+01	-0.180541E+01
B44	18	0.556736E+03	-0.159375E+02	0.530930E+05	17	0.520926E+05	0.312309E+04	-0.242676E+01	-0.242676E+01
WITHIN	249	0.865347E+04	0.132456E+05	0.120847E+07	248	0.116818E+07	0.479105E+04	0.153112E+01	0.153112E+01
AMONG	7	0.842202E+05	0.250634E+05	0.150093E+06	5	0.142634E+06	0.237724E+05	0.297594E+00	0.297594E+00
TOTAL	256	0.928737E+05	0.383130E+05	0.125156E+07	255	0.134275E+07	0.526570E+04	0.412527E+00	0.412527E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.7156 DF = 7, 241  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 4.6090 DF = 7, 248  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 4.2343 DF = 1, 245

ATA UNLML CAPTIONS L01-Y0-L01 VLP TENSILE 77 DEG F .0002 IN/MIN. MODULUS

TABLE A-22

## ANALYSIS OF COVARIANCE TABLE

CORRELATED  
SOPS OF SQUARES AND PRODUCTS  
RELATIONS ABOUT REGRESSION

SOURCE	DF	X	XY	Y	DF	SS	RS	REGRESSION COEFFICIENT
005	7	0.187509E+01	-0.033437E+01	0.193215E+03	6	0.174408E+03	0.287476E+02	-0.332506E+01
006	14	0.216253E+02	-0.148758E+02	0.111476E+03	13	0.101462E+03	0.780-78E+01	-0.791507E+00
010	31	0.785500E+03	0.214937E+03	0.749182E+03	30	0.620147E+03	0.230162E+02	0.272245E+00
012	19	0.340280E+03	0.55312E+03	0.199159E+04	18	0.226145E+04	0.12502E+03	0.144035E+01
013	7	0.151875E+03	-0.119992E+03	0.804170E+03	6	0.389268E+03	0.648760E+02	-0.790072E+00
014	16	0.717167E+03	0.231937E+03	0.313437E+03	15	0.277425E+03	0.167782E+02	0.323358E+01
015	19	0.236562E+03	0.392875E+03	0.184503E+04	18	0.997027E+03	0.533914E+02	0.166076E+01
016	49	0.125819E+04	0.341037E+03	0.255135E+04	48	0.246299E+04	0.512123E+02	0.269426E+00
017	40	0.189962E+04	-0.597125E+03	0.139706E+04	39	0.114623E+04	0.304157E+02	-0.551327E+01
018	21	0.105500E+04	-0.710752E+03	0.464438E+04	20	0.107143E+04	0.685118E+02	-0.694553E+01
019	52	0.121561E+04	0.275125E+03	0.210106E+04	51	0.204274E+04	0.400530E+02	0.226239E+00
020	50	0.264169E+04	0.527250E+03	0.447637E+04	49	0.214450E+04	0.427735E+02	0.351004E+00
021	43	0.289775E+04	0.525312E+03	0.136937E+04	42	0.109358E+04	0.260377E+02	0.319493E+00
022	37	0.203160E+04	0.124794E+04	0.14556E+04	36	0.106377E+04	0.301048E+02	0.614444E+00
023	36	0.265937E+04	0.101462E+04	0.267506E+04	35	0.229296E+04	0.555138E+02	0.376571E+00
024	41	0.196719E+04	0.101062E+04	0.152137E+04	40	0.106118E+04	0.250294E+02	0.513741E+00
025	70	0.545675E+04	0.315681E+04	0.894249E+04	69	0.307428E+04	0.445547E+02	0.584773E+01
026	61	0.523712E+04	0.236681E+04	0.688125E+04	60	0.481162E+04	0.801936E+02	0.451929E+00
027	75	0.762347E+04	0.280719E+04	0.599769E+04	74	0.496547E+04	0.671010E+02	0.367763E+00
028	45	0.659037E+04	0.133106E+04	0.193037E+04	44	0.124531E+04	0.373925E+02	0.209303E+00
029	72	0.836606E+04	0.155237E+04	0.304061E+04	71	0.263465E+04	0.371077E+02	0.220877E+01
030	25	0.202250E+04	0.410687E+03	0.572125E+03	24	0.488731E+03	0.203638E+02	0.203059E+00
031	39	0.192681E+04	-0.175000E+03	0.117461E+04	38	0.115893E+04	0.304953E+02	-0.507293E+01
032	48	0.575169E+04	-0.110461E+04	0.153582E+04	47	0.125973E+04	0.276538E+02	-0.202516E+01
033	50	0.445619E+04	0.258314E+03	0.120125E+04	49	0.117242E+04	0.235270E+02	0.003357E+01
034	24	0.149856E+04	0.179187E+03	0.157875E+04	23	0.175250E+04	0.762129E+02	0.366495E+00
035	42	0.108229E+05	-0.474250E+03	0.222075E+04	41	0.220608E+04	0.538069E+02	-0.435738E+01
036	44	0.605462E+04	0.162325E+04	0.140700E+04	43	0.123407E+04	0.286952E+02	0.169003E+00
037	46	0.190607E+04	0.130125E+03	0.353406E+04	45	0.352619E+04	0.783957E+02	0.681828E+01
WITHIN	1125	0.675769E+05	0.179407E+05	0.597703E+05	1124	0.560951E+05	0.499066E+02	0.204856E+01
AMONG	28	0.971181E+05	0.243229E+04	0.167750E+05	27	0.167102E+05	0.618356E+03	0.000000E+00
TOTAL	1153	0.184659E+06	0.204230E+05	0.765440E+05	1152	0.742957E+05	0.644341E+02	0.000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 5.1724 DF = 28, 1096

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 13.0176 DF = 28, 1124

F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 73.6430 DF = 1, 1124

F05-0.050 CTS 117-70-101 VEP TENDILE FACTOR STRESS. 0.0002 IN/IN, 77 116 F

TABLE A-23

ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS			CORRECTED			ANALYSIS OF COVARIANCE			DEVIATIONS ABOUT REGRESSION			REGRESSION COEFFICIENT
		X	XY	Y	CF	SS	SS	SS	SS	SS	SS	SS	SS	
005	7	0.167500E+01	0.427927E+02	0.170000E+02	8	0.169476E+02	0.202400E+03	0.335612E+02						0.335612E+02
006	14	0.218250E+02	0.350200E+02	0.241190E+02	15	0.241190E+02	0.185475E+03	0.162752E+02						0.162752E+02
010	31	0.789500E+03	-0.419220E+00	0.001000E+02	32	0.639515E+02	0.213172E+03	-0.531003E+03						-0.531003E+03
012	19	0.349250E+03	0.116690E+01	0.172000E+01	18	0.139075E+01	0.772000E+03	0.311231E+02						0.311231E+02
013	7	0.151870E+03	0.519552E+00	0.143000E+01	8	0.125400E+01	0.209146E+02	0.542259E+02						0.542259E+02
014	16	0.717100E+03	0.556000E+01	0.590100E+01	17	0.369522E+02	0.229130E+03	0.631635E+04						0.631635E+04
015	15	0.236562E+03	-0.750600E+00	0.797000E+01	16	0.501616E+02	0.295042E+03	-0.355070E+02						-0.355070E+02
016	45	0.125915E+04	0.163000E+04	0.285000E+01	46	0.271099E+01	0.866455E+03	0.104923E+02						0.104923E+02
017	40	0.169962E+04	0.240503E+01	0.076100E+02	39	0.506458E+02	0.137501E+03	0.141503E+02						0.141503E+02
018	23	0.112200E+04	0.078223E+00	0.726000E+02	24	0.605947E+02	0.211754E+02	0.004476E+02						0.004476E+02
019	52	0.121500E+04	-0.112378E+01	0.819000E+02	53	0.715335E+02	0.140262E+03	-0.924363E+02						-0.924363E+02
020	56	0.264169E+04	0.145410E+01	0.159000E+01	49	0.146911E+01	0.299018E+03	0.350444E+03						0.350444E+03
021	43	0.289775E+04	0.921143E+00	0.127000E+01	42	0.124924E+01	0.297439E+03	0.317861E+03						0.317861E+03
022	37	0.203100E+04	0.765322E+00	0.498000E+02	38	0.470844E+02	0.130790E+03	0.347276E+02						0.347276E+02
023	26	0.269437E+04	-0.180013E+01	0.430123E+01	25	0.417004E+01	0.119194E+02	-0.977965E+03						-0.977965E+03
024	41	0.196719E+04	0.468994E+00	0.095915E+02	40	0.604509E+02	0.221127E+03	0.238476E+03						0.238476E+03
025	70	0.548675E+04	0.303832E+01	0.504000E+01	69	0.417970E+01	0.707202E+03	0.555718E+03						0.555718E+03
026	61	0.527712E+04	0.596582E+00	0.196000E+01	60	0.194141E+01	0.323588E+03	0.190291E+03						0.190291E+03
027	75	0.763437E+04	-0.469580E+01	0.253582E+01	74	0.224699E+01	0.303647E+03	-0.615066E+03						-0.615066E+03
028	45	0.659837E+04	-0.355249E+01	0.116800E+01	44	0.977275E+02	0.222108E+03	-0.536386E+03						-0.536386E+03
029	72	0.838606E+04	-0.232422E+00	0.166452E+01	71	0.166428E+01	0.234400E+03	-0.271524E+03						-0.271524E+03
030	25	0.202250E+04	-0.170848E+01	0.124721E+01	24	0.110289E+01	0.059536E+03	-0.644737E+03						-0.644737E+03
031	39	0.192661E+04	-0.424902E+01	0.016231E+01	38	0.327288E+01	0.075600E+03	-0.220292E+02						-0.220292E+02
032	48	0.575169E+04	0.142796E+01	0.242424E+01	47	0.226179E+01	0.508253E+03	0.248271E+03						0.248271E+03
033	50	0.448619E+04	-0.221460E+01	0.511000E+02	49	0.702145E+02	0.143295E+03	-0.495819E+03						-0.495819E+03
034	24	0.149856E+04	0.134644E+00	0.563543E+02	23	0.562734E+02	0.244667E+03	0.698484E+02						0.698484E+02
035	42	0.168829E+05	-0.122119E+01	0.227936E+01	41	0.236066E+01	0.575771E+03	-0.112016E+02						-0.112016E+02
036	44	0.605462E+04	0.278857E+01	0.220175E+01	43	0.207331E+01	0.482166E+03	0.460569E+03						0.460569E+03
037	46	0.190847E+04	0.167795E+01	0.744829E+02	45	0.597102E+02	0.132669E+03	0.675211E+03						0.675211E+03
WITHIN	1127	0.876429E+05	-0.260352E+01	0.922445E+00	1128	0.462261E+00	0.410552E+03	-0.268534E+04						-0.268534E+04
AMONG	28	0.970571E+05	0.419355E+02	0.224805E+00	27	0.216467E+00	0.764766E+02	0.000000E+00						0.000000E+00
TOTAL	1155	0.164700E+06	0.395820E+02	0.616551E+00	1154	0.678468E+00	0.587927E+03	0.000000E+00						0.000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.5992 DF = 28, 1050  
 F RATIO FOR TESTING DIFFERENCES BETWEEN DEVIATIONS = 16.6063 DF = 28, 1126  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 0.1539 DF = 1, 1126

AND UNBUND CIPS 101-10-LOV VLA HENSEL STD AT FUPTOL, 0002 IF/MLN, 77 DEG F

TABLE A-24

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS		CORRECTED		DEVIATIONS ABOUT REGRESSION		SS	DF	Y	AS	REGRESSION COEFFICIENT
		X	XY	X	Y	X	Y					
100	7	0.167500E+01	-0.233750E+02	0.861700E+04	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
101	14	0.214250E+02	-0.180000E+03	0.504700E+05	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
110	31	0.799500E+03	0.289700E+04	0.107400E+05	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
112	19	0.349250E+03	0.469200E+04	0.426710E+05	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
113	7	0.151675E+03	-0.152750E+04	0.137500E+05	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
114	10	0.717167E+03	-0.946620E+04	0.536500E+05	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
115	19	0.236582E+03	0.623636E+04	0.935120E+05	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
116	49	0.126191E+04	-0.142600E+04	0.233650E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
117	40	0.165962E+04	-0.890000E+04	0.175220E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
118	23	0.112600E+04	-0.622131E+04	0.112175E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
119	52	0.121581E+04	0.752600E+04	0.210230E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
120	50	0.264169E+04	0.418600E+04	0.194350E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
121	43	0.265775E+04	0.573400E+04	0.116320E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
122	37	0.203100E+04	0.631300E+04	0.119530E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
123	36	0.255427E+04	0.545900E+04	0.122112E+07	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
124	41	0.196719E+04	0.417800E+04	0.123430E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
125	76	1.546675E+04	0.222040E+05	0.191030E+07	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
126	61	0.523712E+04	0.225920E+05	0.648300E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
127	75	0.767437E+04	0.294200E+05	0.447520E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
128	45	0.659837E+04	0.258590E+05	0.242217E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
129	73	0.947969E+04	0.113700E+05	0.367180E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
130	25	0.202250E+04	0.670256E+04	0.244440E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
131	39	0.192581E+04	0.430462E+04	0.536900E+05	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
132	48	0.575169E+04	0.595100E+04	0.170160E+07	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
133	51	0.473665E+04	0.379600E+04	0.101170E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
134	24	0.149855E+04	0.449637E+04	0.252100E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
135	42	0.102839E+05	0.227200E+04	0.566198E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
136	44	0.605462E+04	0.251700E+04	0.107451E+07	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
137	46	0.150847E+04	-0.244469E+04	0.147292E+06	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
WITHIN	1129	0.860070E+05	0.169113E+06	0.117445E+08	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
BETWEEN	28	0.967223E+05	-0.162961E+06	0.425148E+07	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
TOTAL	1157	0.184929E+06	-0.446000E+06	0.150290E+08	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.9669 DF = 28, 1100  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 17.6549 DF = 28, 1120  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 35.0739 DF = 1, 1123

ADE UNLOD CINS 101-10-LOT VLF TENSILE MODULUS, .0002 10/MIN, 77 DEG. F



TABLE A-25

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS				REGRESSION	
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				COEFFICIENT	
SOURCE	DF	X	XY	Y	SS	MS			
684	60	7577.0625	2661.5000	3377.8125	2442.9404	41.4058	0.3512574E+00		
625	95	10535.9375	4270.5625	7110.5625	5395.8379	57.4025	0.4015219E+00		
686	97	11237.0625	6898.0625	7940.0625	3705.5703	38.5997	0.6134670E+00		
724	56	6216.0625	3515.2500	4767.3125	2779.4014	50.5346	0.5655107E+00		
WITHIN	308	35666.1250	17545.3750	23195.7500	14760.2422	48.0790	0.4863262E+00		
AMONG	3	5472.8750	-1021.6875	216.2500	25.5193	12.7597	0.0000000E+00		
TOTAL	311	41139.0000	16523.6875	23412.0000	16934.8672	54.6286	0.0000000E+00		

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.0880 DF = 3. 304  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 15.0769 DF = 3. 307  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 175.4511 DF = 1. 307

ANT UNLINED CARTONS LOT-TO-LOT VLR TENSILE 77 DEG F 0.0002 IN/IN. MAX STRESS

TABLE A-26

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED SUMS OF SQUARES AND PRODUCTS		DEVIATIONS ABOUT REGRESSION		MS	REGRESSION COEFFICIENT
		X	XY	Y	SS		
684	60	7577.0625	3.7729	0.0258	0.0239	0.0004	0.4979400E+00
685	95	10535.9375	2.8096	0.0443	0.0436	0.0005	0.2641800E+00
686	97	11237.0625	2.4412	0.0127	0.0122	0.0001	0.2172400E+00
724	56	6216.0625	2.8384	0.0121	0.0108	0.0002	0.4566200E+00
WITHIN	308	35566.1250	11.8623	0.0949	0.0910	0.0003	0.3325900E+00
AMONG	3	5472.8750	7.0061	0.0129	0.0039	0.0020	0.0000000E+00
TOTAL	311	41139.0000	18.8684	0.1078	0.0951	0.0013	0.0000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 6.5625 DF = 3, 304  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 5.2161 DF = 3, 307  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 13.3167 DF = 1, 307

ANT UNLINED CARBONS LOT-TO-LOT VLR TENSILE 77 DEG F 0.0002 IN/MIN. SIN AT RUPT

TABLE A-27

## ANALYSIS OF COVARIANCE TABLE

CORRECTED SUMS OF SQUARES AND PRODUCTS				DEVIATIONS ABOUT REGRESSION				REGRESSION COEFFICIENT
SOURCE	DF	X	XY	Y	DF	SS	MS	
684	60	7577.0625	16910.0000	476624.0000	59	440885.3750	7472.6328	0.2231735E+01
685	95	10625.9275	36207.0000	876678.0000	94	756311.5000	8045.8652	0.3404213E+01
686	97	11237.0625	69105.0000	984240.0000	96	559262.5000	5825.6504	0.6149738E+01
724	56	6216.0625	29915.0000	610576.0000	55	466609.1250	8483.8008	0.4912531E+01
WITHIN	308	35666.1250	152137.0000	2953006.0000	307	2304054.0000	7505.0605	0.4265587E+01
AMONG	3	5472.8750	-13692.0000	51024.0000	2	16769.4687	8384.7344	0.0000000E+00
TOTAL	311	41139.0000	138445.0000	3004032.0000	310	2531123.0000	8167.4922	0.0000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.6916 DF = 3, 304  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 10.3960 DF = 3, 307  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 86.4688 DF = 1, 307

ANT UNLINED CARTONS LOT-10-LOT VLR TENSILE 77 DEG F 0.0002 IN/IN, MODULUS

TABLE A-28

## ANALYSIS OF COVARIANCE TABLE

CORRECTED			DEVIATIONS			ABOUT REGRESSION	
SUMS OF SQUARES AND PRODUCTS							
SOURCE	DF	X	XY	Y	SS	AS	REGRESSION COEFFICIENT
UNLTD	165	0.2594476E+05	0.265790E+05	0.181520E+05	164	0.281765E+04	0.698664E+07
UNITED	50	0.355730E+04	0.495477E+04	0.576370E+05	49	0.310159E+05	0.1338207E+07
ATTNED	215	0.331449E+05	0.255217E+05	0.219557E+06	214	0.159905E+06	0.7700047E+07
AVG	1	0.112700E+05	0.254124E+05	0.757770E+05	0	0.40000E+00	0.253012E+07
TOTAL	216	0.444927E+05	0.547390E+05	0.255504E+06	215	0.227827E+06	0.1232090E+07

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = \*09.3782 DF = 1, 213  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 29.8903 DF = 1, 214  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 21.0375 DF = 1, 214

APT LINED VS UNLINED CARTONS HR TRIAX TENSILE 1750 IN/MIN 600 PSI 77 DEG MAX SITES



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PROPELLANT SURVEILLANCE REPORT MINUTEMAN III STAGE III, (U)  
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TABLE A-29

ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		TOTAL		DEVIATIONS		SS	DF	ABOUT REGRESSION		REGRESSION
		X	XY	Y	Y	SS	SS			AS	AS	
UNREP	155	0.000474+05	-0.022656E+01	0.112450E+00	0.112450E+00	0.112450E+00	0.112450E+00	0.112450E+00	155	0.022497E+03	0.022497E+03	-0.211445E+03
UNREP	50	0.000273E+04	-0.037160E+01	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	49	0.022497E+03	0.022497E+03	-0.161514E+03
WITHIN	216	0.001449E+05	-0.121584E+02	0.184530E+00	0.184530E+00	0.184530E+00	0.184530E+00	0.184530E+00	214	0.022497E+03	0.022497E+03	-0.368027E+03
AMONG	1	0.112780E+05	-0.097123E+00	0.428890E+04	0.428890E+04	0.428890E+04	0.428890E+04	0.428890E+04	0	0.000000E+00	0.000000E+00	0.000000E+00
TOTAL	216	0.044423E+05	-0.324953E+02	0.164564E+00	0.164564E+00	0.164564E+00	0.164564E+00	0.164564E+00	215	0.042972E+03	0.042972E+03	0.000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 7.9240 DF = 1, 215  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 0.9262 DF = 1, 214  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 5.5240 DF = 1, 214

ANY LINEAR VS. UNLINED CANYONS ARE TYPICAL, 1750 IN/MIN, 600 PSI, SIN AT RPT

TABLE A-30

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS					
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION					
SOURCE	DF	S	XY	T	TF	SS	VS	REGRESSION	COEFFICIENT
UNLINED	165	0.294476E+05	-0.259120E+06	0.205105E+09	164	0.143609E+09	0.171665E+06	-0.875925E+01	
LINED	50	0.368975E+04	-0.468550E+05	0.426135E+08	49	0.179079E+08	0.467100E+06	-0.162137E+02	
WITHIN	215	0.331445E+05	-0.307975E+06	0.264323E+09	214	0.161618E+09	0.755426E+06	-0.529177E+01	
AMONG	1	0.112783E+05	0.400581E+06	0.172145E+09	1	0.000000E+03	0.000000E+00	0.090612E+02	
TOTAL	216	0.444237E+05	0.132576E+06	0.217310E+09	215	0.261366E+09	0.142421E+06	0.296435E+01	
F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.0044 DF = 1, 215									
F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 26.0442 DF = 1, 214									
F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 3.7281 DF = 1, 214									

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.0244 DF = 1, 215  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 26.0442 DF = 1, 214  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 3.7281 DF = 1, 214

AMT LINED VS UNLINED CAPTIONS OF TAJAN TENSILE 1750 IN/IN 600 PSI 77 DEG MODULUS

TABLE A-31

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		DEVIATIONS		REGRESSION	
		SUMS OF SQUARES	PRODUCTS	ABOUT REGRESSION	SS	MS	COEFFICIENT
		X	XY	Y	DF		
BET	45	0.275896E+04	0.422087E+04	0.257210E+05	44	0.592989E+05	0.134746E+04
WT	50	0.369730E+04	0.494775E+04	0.376270E+05	49	0.710159E+05	0.132977E+03
WITHIN	95	0.644625E+04	0.916862E+04	0.103368E+06	94	0.903876E+05	0.961358E+03
ANALYTIC	1	0.793121E+03	0.162562E+04	0.420000E+04	1	-0.228563E+01	0.00000E+00
TOTAL	96	0.725937E+04	0.734300E+04	0.107568E+06	95	0.100140E+06	0.105411E+04

\*\*\*\*\*

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.0565 DF = 1, 95

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 10.1656 DF = 1, 94

F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 13.5229 DF = 1, 94

ANALYTIC VS ALL LINED CANYONS HR TRIAX TENSILE 1750 IN/MIN 200 PSI 77 DEG MAX STRESS



TABLE A-32

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED SUMS OF SQUARES AND PRODUCTS			DEVIATIONS ABOUT REGRESSION			REGRESSION COEFFICIENT
		X	XY	Y	SS	MS		
ANB	45	0.278896E+04	0.242358E+01	0.109529E-01	0.102210E-01	0.232257E-03	-.5141227E-04	
ANT	50	0.362730E+04	-.597168E+01	0.320564E-01	0.224412E-01	0.457984E-03	-.1615147E-04	
WITHIN	95	0.645625E+04	-.735526E+01	0.436393E-01	0.345216E-01	0.367869E-03	-.1142679E-04	
BEFORE	1	0.752111E+03	0.220037E+00	0.772676E-04	0.526224E-05	0.000000E+00	0.0001268E-03	
TOTAL	96	0.725537E+04	-.715723E+01	0.431168E-01	0.320601E-01	0.279575E-03	-.5859287E-04	

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 5.4649 DF = 1, 96  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 4.0168 DF = 1, 94  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 22.9899 DF = 1, 94

ANB VS ANT LINED CAPIONS PER TRIAX TENSILE 1750 IN/MIN 600 PSI 77 DEG SIN AT RUPT

TABLE A-33

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS			
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION			
SOURCE	DF	X	XY	Y	SS	MS	REGRESSION COEFFICIENT
ENT	45	0.276850E+04	0.510200E+04	0.955750E+07	44	0.954708E+07	0.216997E+06
ANT	50	0.369730E+04	0.405550E+05	0.186235E+08	49	0.179179E+08	0.367100E+06
WITHIN	95	0.646665E+04	-0.430930E+05	0.001510E+03	94	0.270557E+08	0.296763E+06
AMONG	1	0.792101E+05	0.419510E+05	0.201255E+07	0	0.327000E+03	0.000000E+00
TOTAL	96	0.725937E+04	-0.174200E+04	0.000102E+08	95	0.300098E+08	0.320103E+06
F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.2157 DF = 1, 93							
F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 8.4717 DF = 1, 94							
F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 0.9949 DF = 1, 94							

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.2157 DF = 1, 93

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 8.4717 DF = 1, 94

F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 0.9949 DF = 1, 94

AFB VS AIT LINED CARTONS HR TRIAX TENSILE 1750 IN/MIN 600 PST 77 OFG MODULUS

TABLE A-34

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		DEVIATIONS		REGRESSION	
		SS	MS	SS	MS	SS	MS
AREA	65	0.261765E+05	0.204900E+04	0.772960E+05	64	0.771670E+05	0.120542E+04
TIME	214	0.502051E+05	0.281623E+05	0.365120E+06	213	0.249509E+06	0.164065E+04
WTHIN	279	0.789836E+05	0.261130E+05	0.442415E+06	278	0.423783E+06	0.156027E+04
AMONG	1	0.143714E+04	0.100400E+04	0.732100E+03	0	0.345868E+02	0.000000E+00
TOTAL	280	0.304207E+05	0.271170E+05	0.442152E+06	279	0.424000E+06	0.155555E+04

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 4.6265 DF = 1, 277  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 0.1447 DF = 1, 278  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 5.5325 DF = 1, 278

AREA VS AREA UNLOD CTS PER TRIAX TENSILE 1750 IN/MIN 77 DEG F 600 PST MAX STRESS

TABLE A-35

## ANALYSIS OF COVARIANCE TABLE

SOURCE OF VARIATION	SS	DF	MS	REGRESSION COEFFICIENT	DEVIATIONS FROM REGRESSION
TOTAL	0.804207E+05	279	0.288249E+00	0.111167E-02	0.333754E-04
AMONG	0.142712E+05	1	0.142712E+05	0.000000E+00	-0.679932E-02
WITHIN	0.759836E+05	278	0.273322E+00	0.870071E-03	0.157551E-03
AMONG	0.124555E+02	2	0.622775E+00	0.000000E+00	0.142655E-02
WITHIN	0.724780E+01	213	0.340272E+00	0.101423E-02	0.142655E-02
AMONG	0.508051E+05	64	0.793984E+00	0.418408E+01	0.164613E-03
WITHIN	0.267782E+05	213	0.125721E+00	0.101423E-02	0.142655E-02

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 76.7500 DF = 1, 277  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 78.5376 DF = 1, 276  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 2.2575 DF = 1, 278

ANALYSIS OF COVARIANCE TABLE FOR TRIAX TESTS 1750 IN/MIN 77 DEG F 600 PSI SIN AT RUPT



TABLE A-36

## ANALYSIS OF COVARIANCE TABLE

SUMS OF SQUARES AND PRODUCTS										DEVIATIONS										REGRESSION	
CORRECTED		Y		XY		Y		Y		SS		SS		SS		COEFFICIENT					
SOURCE	DF	X	Y	XY	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y	Y				
ANA	65	0.261785E+05	-	775985E+06	0.429186E+08	64	0.215466E+08	0.336666E+06	-	2753219E+02	-	2753219E+02	-	2753219E+02	-	2753219E+02	-				
AMB	214	0.566051E+05	-	816400E+06	0.511755E+09	213	0.493162E+09	0.233888E+07	-	161086E+02	-	161086E+02	-	161086E+02	-	161086E+02	-				
ATTN	279	0.759836E+05	-	139438E+07	0.354281E+09	278	0.522096E+09	0.187804E+07	-	201872E+02	-	201872E+02	-	201872E+02	-	201872E+02	-				
FACTOR	1	0.143712E+04	0.290513E+06	0.827.24E+08	0.827.24E+08	0	-	0.00000E+00	-	0.2921467E+02	-	0.2921467E+02	-	0.2921467E+02	-	0.2921467E+02	-				
TOTAL	250	0.805207E+05	-	130387E+07	0.613707E+09	279	0.551867E+09	0.212139E+07	-	1621312E+02	-	1621312E+02	-	1621312E+02	-	1621312E+02	-				

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.2720 DF = 1, 277  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 37.1510 DF = 1, 278  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 17.1373 DF = 1, 279

ANA VS AMB UNLAD CLAS HR TRIAX TELSILE 1750 IN/MIN 77 DEG F 600 PSI MODULUS

TABLE A-37

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS				REGRESSION	
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				COEFFICIENT	
SOURCE	DF	X	XY	Y	DF	SS	MS		
ANA	65	0.281765E+05	-0.204900E+04	0.773120E+05	64	0.771630E+05	0.120567E+04	-0.727149E+01	
ANB	214	0.508051E+05	0.282150E+05	0.366336E+06	213	0.250666E+06	0.164832E+04	0.555357E+00	
ANT	165	0.294476E+05	0.205690E+05	0.181872E+06	164	0.117505E+06	0.102137E+04	0.698494E+00	
WITHIN	444	0.109431E+06	0.487350E+05	0.625520E+06	443	0.603276E+06	0.136654E+04	0.431010E+00	
AMONG	2	0.354275E+04	-0.128790E+05	0.922860E+05	1	0.454688E+05	0.454688E+05	-0.363531E+01	
TOTAL	446	0.111974E+05	0.338560E+05	0.717608E+06	445	0.615442E+06	0.138302E+04	0.302355E+00	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.7195 DF = 2, 441  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 3.6629 DF = 2, 443  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 14.7404 DF = 1, 443

ANA VS AMBIANT UNLPO CARTONS FOR TPIAX TENSILE 1750 IN/IN 600 PSI MAXIMUM STRESS

TABLE A-38

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		SUNS OF SQUARES AND PRODUCTS		DEVIATIONS ABOUT REGRESSION		REGRESSION COEFFICIENT	
		X	Y	XY	SS	SS	SS	AS	AS
ANA	65	0.261765E+05	0.520776E+01	0.267792E+01	64	0.252167E-01	0.403366E-03	0.1848132E-02	0.1848132E-02
ANB	214	0.508091E+05	0.724707E+01	0.217068E+00	213	0.214034E+00	0.101424E-02	0.142644E-02	0.142644E-02
ANT	165	0.294476E+05	-0.222949E+01	0.152829E+00	164	0.151511E+00	0.923249E-03	-0.211544E-02	-0.211544E-02
WITITE	443	0.105431E+05	0.622534E+01	0.396176E+00	443	0.396319E+00	0.094624E-03	0.574127E-02	0.574127E-02
AMONG	2	0.354275E+04	-0.198191E+02	0.114402E+00	1	0.352654E-02	0.352654E-02	-0.559426E-02	-0.559426E-02
TOTAL	446	0.111974E+05	-0.135937E+02	0.509428E+00	445	0.507777E+00	0.114107E-02	-0.121400E-02	-0.121400E-02

\*\*\*\*\*

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.6573 DF = 2, 441

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 12.2935 DF = 2, 443

F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 0.3995 DF = 1, 443

ANA VS ANB ANT UNLND CTNS HR TRIAX TENSILE 1750 IN/MIN 600 PSI 77 DEG STC AT RUP

TABLE A-39

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED			DEVIATIONS			REGRESSION
		SUMS OF SQUARES AND PRODUCTS			ABOUT REGRESSION			COEFFICIENT
		X	XY	Y	SS	MS		
ANA	65	0.261765E+05	-.775985E+06	0.429158E+08	64	0.215466E+08	0.336666E+06	-.2753819E+09
AMB	214	0.508051E+05	-.813460E+06	0.511304E+09	213	0.498118E+09	0.233858E+07	-.1611018E+09
AMT	165	0.294476E+05	-.359200E+06	0.145889E+09	164	0.143607E+09	0.875652E+06	-.8802067E+01
WITHIN	444	0.105431E+05	-.185366E+07	0.700160E+09	443	0.303219E+09	0.685053E+06	-.1709620E+02
AMONG	2	0.354275E+04	0.650017E+06	0.113480E+09	1	0.144282E+07	0.144282E+07	0.1770328E+03
TOTAL	446	0.111974E+06	-.122365E+07	0.813588E+09	445	0.800216E+09	0.179824E+07	-.1092792E+02

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 93.1016 DF = 2, 442  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 241.0244 DF = 2, 443  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 366.3237 DF = 1, 443

ANA VS AMBXANT UNLND CARTONS HR TRIAX TENSILE 1750 IN/MIN 600 PSI MODULUS



ANALYSIS OF COVARIANCE TABLE

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES =	1.7586	DF =	6,	14
F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS =	5.2753	DF =	6,	20
F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE =	0.1309	DF =	1,	20

ANS LINEO CTS LOT-70-LO7 HR TRIAX TENS MAXIMUM STRESS: 2750 IN/ININ, 600 PSI

TABLE A-41

## ANALYSIS OF COVARIANCE TABLE

CORRECTED			SUMS OF SQUARES AND PRODUCTS			ELEVATIONS			ABOUT REGRESSION		
SOURCE	DF	X	XY	Y	LF	SS	MS	REGRESSION	COEFFICIENT		
051	3	0.107000E+01	-2.16504E-01	0.430942E-03	2	0.908944E-05	0.204472E-05	-2.066040E-01			
053	3	0.400000E+01	-5.59998E-01	0.610000E-03	2	0.202128E-04	0.131040E-04	-1.559990E-01			
056	3	0.400000E+01	0.275235E-02	0.500000E-04	2	0.221445E-04	0.160723E-04	0.698129E-01			
057	3	0.107000E+01	0.605120E-02	0.405120E-03	2	0.442012E-03	0.224956E-03	0.605119E-02			
058	3	0.900000E+01	-1.24359E-01	0.386808E-03	2	0.379624E-03	0.284512E-03	-1.381789E-01			
059	3	0.100000E+01	-9.24683E-02	0.124991E-03	2	0.394871E-04	0.157436E-04	-9.246824E-02			
061	3	0.100000E+01	0.261536E-01	0.124735E-02	2	0.559344E-03	0.279572E-03	0.261535E-01			
WY-TM	21	0.210000E+02	-6.25458E-01	0.372624E-02	20	0.353996E-02	0.176998E-03	-2.97637E-02			
AN016	6	0.162486E+04	-6.21872E+00	0.129150E-02	5	0.104349E-02	0.208699E-03	0.000000E+00			
TOTAL	27	0.164586E+04	-6.68441E+00	0.500774E-02	26	0.472312E-02	0.181659E-03	0.000000E+00			

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.5838 DF = 6, 18  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 1.1141 DF = 6, 20  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 1.0525 DF = 1, 20

ANALYSED CAPTIONS LOT TO LOT HP TRIAX TESTS STD AT FLP, 1750 IN/MIN, 600 PSI

TABLE A-42

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED SUMS OF SQUARES AND PRODUCTS			DEVIATIONS ABOUT REGRESSION			REGRESSION COEFFICIENT
		X	XY	Y	SS	XS	YS	
051	3	0.10000E+01	0.30900E+03	0.18243E+06	2	0.46271E+05	0.251355E+05	0.369000E+03
052	3	0.40000E+01	0.132800E+04	0.57270E+06	2	0.13160E+06	0.65904E+05	0.532000E+03
053	3	0.40000E+01	0.10200E+04	0.23010E+06	2	0.42317E+06	0.33133E+06	0.450000E+03
057	3	0.10000E+01	-0.23250E+03	0.24014E+06	2	0.15295E+06	0.79475E+05	-0.296500E+03
058	3	0.90000E+01	0.173250E+04	0.44904E+06	2	0.11550E+06	0.57766E+05	0.192500E+03
059	3	0.10000E+01	0.23250E+03	0.14036E+06	2	0.86311E+05	0.43155E+05	0.232500E+03
061	3	0.10000E+01	-0.69600E+03	0.12395E+06	2	0.14474E+06	0.73374E+05	-0.69600E+03
WITHIN	21	0.21000E+02	0.363950E+04	0.31554E+07	20	0.25037E+07	0.12518E+06	0.17616E+03
AMONG	6	0.16248E+04	0.314150E+04	0.23113E+07	5	0.22700E+07	0.45419E+06	0.00000E+00
TOTAL	27	0.16458E+04	0.110410E+05	0.54618E+07	26	0.53169E+07	0.20698E+06	0.00000E+00

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.9958 DF = 6, 14  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 3.8215 DF = 6, 20  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 5.2060 DF = 1, 20

AMONG LIGED CARTON'S LOT-TO-LOT 12 UNIAK TENS FOCUS, 1750 IN/MIN, 100 PSI

TABLE A-43

## ANALYSIS OF COVARIANCE TABLE

UNREJECTED  
SOMS OF SQUARES AND PRODUCTS

DEVIATIONS  
ABOUT REGRESSION

SOURCE	DF	Y	X1	Y	LF	SE	MS	REGRESSION COEFFICIENT
711	9	0.242500E+03	0.520187E+03	0.272200E+04	0	0.157256E+04	0.196570E+03	0.217316E+01
712	9	0.120102E+03	0.419625E+03	0.164000E+04	1	0.876207E+04	0.122418E+03	0.149381E+01
713	9	0.157602E+03	0.248675E+03	0.452000E+04	2	0.419771E+04	0.199691E+03	0.212455E+01
819	5	0.600000E+01	0.129562E+03	0.469700E+04	4	0.171928E+04	0.447315E+03	0.215977E+01
820	5	0.150000E+01	-0.421406E+02	0.284100E+04	4	0.245611E+04	0.614628E+03	-0.200937E+01
821	5	0.150000E+01	0.621875E+01	0.210000E+03	4	0.184216E+03	0.460445E+02	0.145332E+01
WITHIN	42	0.529203E+03	0.139033E+04	0.243700E+05	41	0.264853E+05	0.645201E+03	0.262721E+01
AMONG	5	0.285560E+04	0.270861E+04	0.102640E+05	4	0.769589E+04	0.192397E+04	
TOTAL	47	0.335600E+04	0.409894E+04	0.346120E+05	45	0.294400E+05	0.644348E+03	

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.5910 FF = 5. 30  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 3.5498 FF = 5. 41  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 7.2399 FF = 1. 41

ANT LINEO CARTONS LOT-10-LOT NR TRIAX TENSILE 1750 IN/MIN 600 PSI. MAX STRESS



TABLE A-44

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		LEVATIONS		REGRESSION	
		SS	MS	SS	MS	SS	MS
711	9	0.242500E+03	-1.56127E+02	0.416720E-02	0.409767E-02	0.512171E-03	-0.566805E-03
712	9	0.126102E+03	-4.57357E+01	0.449411E-02	0.274727E-02	0.744714E-03	-0.580318E-03
713	9	0.157602E+03	-2.92999E+02	0.323776E-02	0.729304E-02	0.411131E-03	-0.185931E-03
819	5	0.600000E+01	-3.45917E-01	0.267876E-02	0.247632E-02	0.415082E-03	-0.576514E-03
820	5	0.150000E+01	0.374908E-01	0.135279E-02	0.415745E-03	0.103936E-03	0.249939E-03
821	5	0.150000E+01	0.542908E-01	0.303549E-02	0.107049E-02	0.267025E-03	0.561932E-03
WITHIN	42	0.529203E+03	-2.23303E+00	0.195523E-01	0.182714E-01	0.445645E-03	-0.155574E-03
AMONG	5	0.285680E+04	-4.35077E+01	0.103167E-01	0.769248E-02	0.322170E-03	
TOTAL	47	0.338600E+04	-5.17407E+01	0.298710E-01	0.219246E-01	0.477491E-03	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.1332 DF = 5, 50

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 1.5574 DF = 5, 41

F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 2.8741 DF = 1, 41

ANY LINED CARTONS LOT-10-LOT HR TRYX TENSILE 1750 IN/MIN 600 PSI STRAIN AT RUPI

TABLE A-45

## ANALYSIS OF COVARIANCE TABLE

CORRECTED  
SUMS OF SQUARES AND PRODUCTS  
DEVIATIONS  
ABOUT REGRESSION

SOURCE OF VARIATION	SS	DF	Y	XY	SS	REGRESSION COEFFICIENT
711	9 0.242500E+03		0.305530E+07	8 0.910037E+06	0.101255E+06	-0.962126E+02
712	9 0.129102E+03		0.563031E+07	9 0.211568E+07	0.244580E+06	-0.171160E+02
713	9 0.157602E+03		0.282116E+07	0 0.270098E+07	0.336711E+06	-0.204740E+02
819	5 0.600000E+01		0.171794E+07	4 0.157592E+07	0.394590E+06	-0.151246E+02
820	5 0.150000E+01		0.805222E+06	4 0.335420E+06	0.268580E+05	-0.047614E+02
821	5 0.150000E+01		0.232000E+03	4 0.402397E+06	0.150592E+06	-0.158662E+02
WITHIN	42 0.529203E+03		0.146782E+08	41 0.994872E+07	0.242452E+06	-0.345355E+02
AMONG	5 0.285680E+04		0.224597E+07	4 0.204483E+07	0.521159E+06	
TOTAL	47 0.338600E+04		0.169142E+08	46 0.154145E+08	0.336097E+06	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.5595 DF = 5, 36  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 4.5050 DF = 5, 41  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 19.4908 DF = 1, 41

ANT LINED CARTONS LOT-TO-LOT HR TRIAX TENSILE 1750 IN/MIN 600 PSI MODULUS

TABLE A-46

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED			DEVIATIONS			REGRESSION
		SUNS OF SQUARES AND PRODUCTS		ABOUT REGRESSION	COEFFICIENT			
		Y	XY	Y	SS	MS		
*****	*****	*****	*****	*****	*****	*****	*****	
041	19	0.257000E+03	0.121250E+04	0.326150E+05	0.268945E+05	18	0.149414E+04	
015	2	0.240000E+02	0.273125E+02	0.311250E+02	0.428085E-01	1	0.428085E-01	
037	8	0.200000E+01	0.427500E+02	0.122400E+04	0.310219E+03	7	0.443170E+02	
040	8	0.600000E+01	0.254375E+03	0.146450E+05	0.381292E+04	7	0.544703E+03	
044	8	0.600000E+01	-0.346875E+02	0.398000E+03	0.197463E+03	7	0.282090E+02	
WITHIN	45	0.297000E+03	0.154225E+04	0.469131E+05	0.409046E+05	44	0.929849E+03	
AMONG	4	0.205926E+05	-0.999925E+04	0.196219E+05	0.147665E+05	3	0.492216E+04	
TOTAL	49	0.208896E+05	-0.845700E+04	0.685350E+05	0.651112E+05	48	0.135648E+04	
*****	*****	*****	*****	*****	*****	*****	*****	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.1041 DF = 4. 40  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 6.5096 DF = 4. 44  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 8.6146 DF = 1. 44

ANA UNLND CARTONS LOT-10-LOT HF TRIAX TENSILE 1750 IN/MIN 600 PSI. MAX STRESS

TABLE A-47

## ANALYSIS OF COVARIANCE TABLE

SOURCE OF	DEGREES OF FREEDOM	CORRECTED SUMS OF SQUARES AND PRODUCTS		DEVIATIONS ABOUT REGRESSION		REGRESSION COEFFICIENT
		X	XY	Y	SS	SS
19	19	0.287000E+03	-0.275443E+00	0.314955E-02	0.930107E-02	0.416726E-03
115	2	0.240000E+02	0.299885E-01	0.474913E-04	0.775190E-07	0.725090E-07
337	8	0.200000E+01	0.424570E-01	0.166116E-02	0.719905E-03	0.102844E-03
440	6	0.300000E+01	-0.674560E-01	0.117441E-02	0.130790E-03	0.116157E-03
349	8	0.600000E+01	0.276794E-01	0.432909E-03	0.365217E-03	0.436024E-04
417+10	45	0.297000E+03	-0.324800E+00	0.132545E-01	0.128771E-01	0.292661E-03
AMCAG	4	0.205926E+05	0.486240E+01	0.692468E-02	0.537656E-02	0.179219E-02
TOTAL	49	0.204896E+05	0.452759E+01	0.157792E-01	0.117979E-01	0.391623E-03

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.5400 DF = 4, 46  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 5.0577 DF = 4, 44  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 1.2896 DF = 1, 44

ALFA UNLNE CARTONS LOT-TO-LOT OR TENSILE 1750 IN/IN 600 PSI, STA. AT CAPTURE



TABLE A-48

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED SUMS OF SQUARES AND PRODUCTS			ELEVATIONS ABOUT REGRESSION			REGRESSION COEFFICIENT
		X	XY	Y	SS	SS	SS	
M41	19	0.257000E+03	0.135000E+05	0.612966E+07	16	0.542052E+07	0.301140E+06	0.5257917E+02
015	2	0.240000E+02	-0.400000E+04	0.66688E+06	1	0.215000E+02	0.215000E+02	-0.166666E+03
037	6	0.200000E+01	-0.217000E+03	0.157150E+06	7	0.133511E+06	0.190731E+05	-0.108500E+03
040	8	0.200000E+01	-0.266000E+03	0.101350E+07	7	0.10092E+07	0.14274E+06	-0.335000E+02
044	6	0.600000E+01	-0.103600E+04	0.473060E+06	7	0.294397E+06	0.420568E+05	-0.172066E+02
WITHIN	45	0.297000E+03	0.797900E+04	0.844556E+07	44	0.823122E+07	0.167073E+06	0.2686531E+01
AMONG	4	0.205926E+05	-0.710530E+06	0.313714E+08	3	0.685518E+07	0.228506E+07	-0.345040E+02
TOTAL	49	0.206896E+05	-0.702551E+06	0.398170E+08	48	0.161891E+08	0.337272E+06	-0.336315E+02

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.0017 DF = 4, 40  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 10.6347 DF = 4, 44  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 1.1459 DF = 1, 44

APA UNLND CARTONS LCI-10-LOT HR TRIAX TESTILE 1750 IN/MIN 600 PSI. MODULUS

TABLE A-49

## ANALYSIS OF COVARIANCE TABLE

CORRECTED  
SUMS OF SQUARES AND PRODUCTS

DEVIATIONS  
ABOUT REGRESSION

SOURCE	DF	X	XY	Y	DF	SS	XS	YS	REGRESSION COEFFICIENT
016	5	0.52000E+02	-0.60000E+03	0.91800E+04	4	0.811078E+03	0.202770E+03	-0.1269231E+02	
019	6	0.768554E+02	-0.525000E+03	0.650000E+04	5	0.291391E+04	0.532761E+03	-0.083065E+01	
021	5	0.217350E+03	0.300000E+03	0.218000E+04	4	0.152358E+04	0.780080E+03	0.174844E+01	
023	7	0.346000E+03	0.672500E+03	0.257000E+04	6	0.168590E+04	0.277550E+03	0.194374E+01	
025	7	0.527500E+03	0.100000E+03	0.365000E+04	6	0.363139E+04	0.405232E+03	0.166045E+00	
026	7	0.390000E+03	-0.637500E+02	0.471100E+04	6	0.470058E+04	0.763430E+03	-0.163491E+01	
028	5	0.625336E+03	-0.936875E+03	0.532100E+04	4	0.351838E+04	0.979555E+03	-0.150139E+01	
031	5	0.228000E+03	-0.106825E+04	0.522700E+04	4	0.122192E+04	0.305480E+03	-0.468530E+01	
035	13	0.489521E+04	-0.117627E+04	0.261210E+05	12	0.250463E+05	0.215402E+04	-0.2402170E+00	
036	4	0.245203E+03	0.117300E+04	0.565100E+04	3	0.132686E+03	0.445618E+02	0.470703E+01	
041	9	0.135760E+04	0.102294E+04	0.311200E+04	8	0.234223E+04	0.292778E+03	0.753426E+00	
042	8	0.538223E+03	0.113944E+04	0.349400E+04	7	0.108177E+04	0.154538E+03	0.211705E+01	
045	9	0.255240E+04	0.311844E+04	0.468700E+04	8	0.109167E+04	0.136484E+03	0.121699E+01	
047	9	0.182000E+04	0.582250E+03	0.302500E+04	8	0.264273E+04	0.355341E+03	0.319917E+00	
048	12	0.952309E+03	-0.155269E+04	0.900500E+04	11	0.647343E+04	0.588493E+03	-0.163044E+01	
049	11	0.306000E+04	0.314262E+04	0.546100E+04	10	0.225248E+04	0.225342E+03	0.102173E+01	
050	7	0.154000E+04	0.162662E+04	0.311000E+04	6	0.139108E+04	0.251980E+03	0.105625E+01	
WTFY	131	0.194720E+05	0.657237E+04	0.105793E+06	130	0.103402E+06	0.795403E+03	0.358072E+00	
AMCIC	18	0.158025E+05	0.865462E+04	0.122169E+06	17	0.117932E+06	0.693720E+04	0.000000E+00	
TOTAL	149	0.353544E+05	0.156270E+05	0.226763E+06	148	0.221683E+06	0.149786E+04	0.000000E+00	

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.3550 DF = 18, 142  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 0.2614 DF = 18, 130  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 3.1388 DF = 1, 130

ALL UNITS CYAS LOT-TO-LOT HR MAX TENSILE 77 DEG 1750 LB/MIN 600 PSI MAX STRESS

TABLE A-50

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS			CORRECTED			DEVIATIONS ABOUT REGRESSION			REGRESSION COEFFICIENT	
		X	XY	Y	LF	SS	XS	SS	XS	XS	COEFFICIENT	*****
016	5	0.520000E+02	0.101074E+00	0.284749E-02	4	0.265103E-02	0.462758E-03	0.194373E-02	0.194373E-02	0.194373E-02	0.194373E-02	*****
019	6	0.768594E+02	-0.685898E+00	0.824173E-02	5	0.277772E-02	0.545547E-03	-0.924102E-02	-0.924102E-02	-0.924102E-02	-0.924102E-02	*****
021	5	0.217336E+03	0.399002E+00	0.157231E-02	4	0.839792E-03	0.209948E-03	0.1835877E-02	0.1835877E-02	0.1835877E-02	0.1835877E-02	*****
027	7	0.347000E+03	0.291107E+00	0.182436E-02	6	0.133354E-02	0.220589E-03	0.1413501E-01	0.1413501E-01	0.1413501E-01	0.1413501E-01	*****
025	7	0.537500E+03	0.176634E+01	0.869199E-02	5	0.268641E-02	0.481068E-03	0.3286217E-02	0.3286217E-02	0.3286217E-02	0.3286217E-02	*****
026	7	0.390000E+03	0.728500E+00	0.21767E-02	6	0.761587E-02	0.130284E-02	0.1627945E-02	0.1627945E-02	0.1627945E-02	0.1627945E-02	*****
028	5	0.625333E+03	0.765980E-01	0.26463E-02	4	0.263675E-02	0.659166E-03	0.1256893E-02	0.1256893E-02	0.1256893E-02	0.1256893E-02	*****
029	1	0.000000E+00	0.000000E+00	0.140452E-02	0	0.140452E-02	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	*****
030	1	0.000000E+00	0.000000E+00	0.391463E-03	0	0.391463E-03	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	*****
031	5	0.225000E+03	-0.544861E+00	0.195503E-02	4	0.653016E-03	0.162254E-03	-0.238574E-02	-0.238574E-02	-0.238574E-02	-0.238574E-02	*****
035	13	0.489921E+04	0.610681E+01	0.222362E-01	12	0.146241E-01	0.12166E-02	0.1246444E-02	0.1246444E-02	0.1246444E-02	0.1246444E-02	*****
036	4	0.249203E+03	0.776439E+00	0.263202E-02	3	0.212568E-03	0.708560E-04	0.311588E-02	0.311588E-02	0.311588E-02	0.311588E-02	*****
041	9	0.135760E+04	-0.121471E+01	0.364408E-02	8	0.275723E-02	0.344554E-03	-0.8947444E-02	-0.8947444E-02	-0.8947444E-02	-0.8947444E-02	*****
042	8	0.538223E+03	0.210390E+01	0.297902E-02	7	0.754952E-03	0.10740E-03	0.390092E-02	0.390092E-02	0.390092E-02	0.390092E-02	*****
045	9	0.256240E+04	0.334778E+01	0.930112E-02	8	0.493125E-02	0.616406E-03	0.130650E-02	0.130650E-02	0.130650E-02	0.130650E-02	*****
047	5	0.182000E+04	0.239757E+01	0.466367E-02	8	0.150524E-02	0.188155E-03	0.131734E-02	0.131734E-02	0.131734E-02	0.131734E-02	*****
048	12	0.952309E+03	-0.352417E+00	0.113759E-01	11	0.102455E-01	0.931409E-03	-0.370065E-02	-0.370065E-02	-0.370065E-02	-0.370065E-02	*****
049	11	0.306000E+04	0.370435E+01	0.612194E-02	10	0.256558E-02	0.251558E-03	0.120272E-02	0.120272E-02	0.120272E-02	0.120272E-02	*****
050	7	0.154000E+04	0.137057E+01	0.171682E-02	6	0.499030E-03	0.631717E-04	0.899923E-02	0.899923E-02	0.899923E-02	0.899923E-02	*****
WITHIN	131	0.194720E+05	0.203743E+02	0.116936E+00	130	0.898201E-01	0.689586E-03	0.1046337E-02	0.1046337E-02	0.1046337E-02	0.1046337E-02	*****
AMONG	18	0.158825E+05	-0.111421E+02	0.320516E-01	17	0.242351E-01	0.142559E-02	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	*****
TOTAL	149	0.353544E+05	0.923218E+01	0.142590E+00	148	0.140579E+00	0.949680E-03	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	*****

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.7020 DF = 18, 112  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 4.1065 DF = 18, 130  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 30.9237 DF = 1, 130

AME UNLNO CTIS LOT-TO-LOT HR TRIAX TENSILE 77 DEG 1750 IN/IN 600 PSI STA AT RUP

TABLE A-51

## ANALYSIS OF COVARIANCE TABLE

CORRECTED  
SUMS OF SQUARES AND PRODUCTS

DEVIATIONS  
ABOUT REGRESSION

SOURCE OF	X	XY	Y	DF	SS	MS	REGRESSION COEFFICIENT
018	5	0.520000E+02	0.347315E+07	4	0.155008E+07	0.387519E+06	-0.1925077E+02
019	6	0.745594E+02	0.511153E+07	5	0.509544E+07	0.101365E+07	0.1747344E+02
021	5	0.217235E+03	0.867334E+07	4	0.115847E+07	0.284517E+06	-0.1607227E+02
022	7	0.347100E+03	0.917139E+07	6	0.705621E+07	0.448270E+06	-0.1231214E+02
025	7	0.527500E+03	0.712000E+07	6	0.147555E+07	0.245852E+06	-0.1060465E+02
026	7	0.350000E+03	0.923688E+07	6	0.901436E+07	0.150239E+07	-0.2884615E+02
028	5	0.625336E+03	0.298000E+07	4	0.162563E+07	0.406458E+06	-0.4653497E+02
029	1	0.000000E+00	0.720000E+06	0	0.720000E+06	0.000000E+00	0.000000E+00
036	1	0.000000E+00	0.405000E+06	0	0.405000E+06	0.000000E+00	0.000000E+00
031	5	0.226000E+03	0.337722E+07	4	0.336618E+07	0.841546E+06	0.6956139E+01
035	13	0.449221E+04	0.305208E+08	12	0.696642E+07	0.582202E+06	-0.6933517E+02
036	4	0.249203E+05	0.444400E+04	3	0.265152E+07	0.893773E+06	0.1785280E+02
041	9	0.135760E+04	0.379350E+05	8	0.648047E+07	0.810059E+06	0.2794266E+02
042	8	0.538223E+03	0.412710E+05	7	0.340502E+06	0.486431E+05	-0.7668015E+02
045	9	0.255240E+04	0.279349E+06	8	0.386263E+07	0.482829E+06	-0.1090184E+02
047	9	0.182000E+04	0.225996E+06	8	0.114251E+07	0.142014E+06	-0.1241734E+02
048	12	0.952309E+03	0.116721E+06	11	0.631894E+07	0.574449E+06	-0.1225663E+02
049	11	0.308000E+04	0.244586E+06	10	0.145709E+07	0.145730E+06	-0.7944346E+02
050	7	0.154000E+04	0.124126E+06	6	0.185281E+07	0.308755E+06	-0.5060129E+02
WITHIN	131	0.194723E+05	0.151141E+07	130	0.925508E+08	0.712237E+06	-0.7761931E+02
AMONG	19	0.154825E+05	0.572372E+06	17	0.100652E+09	0.592075E+07	0.000000E+00
TOTAL	149	0.353544E+05	0.331166E+09	148	0.208244E+09	0.206922E+07	0.000000E+00

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 3.4896 DF = 18, 112

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 16.5653 DF = 18, 130

F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 164.7141 DF = 1, 130

AMB UNLND CTS LOT-TO-LOT MK TRIAX TENSILE 77 DEG 1750 16/MIN 600 PSI MODULUS



TABLE A-52

## ANALYSIS OF COVARIANCE TABLE

SOURCE		X		Y		X <sup>2</sup>		XY		Y <sup>2</sup>		DEVIATIONS		FROM REGRESSION		SS		DF		MS		REGRESSION		COEFFICIENT	
31	0.152275	0.000000	0.04	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
31	0.221708	0.000000	0.04	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
31	0.200822	0.000000	0.04	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
28	0.103940	0.000000	0.04	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
121	0.693720	0.000000	0.04	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
3	0.116974	0.000000	0.03	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
124	0.511654	0.000000	0.05	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.0006 DF = 3, 117  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 21.5936 DF = 3, 120  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 38.0704 DF = 1, 120

ADJ UPLAND CIMS LOT-10-LOT 10R MAX TENSILE MAX STRESS, 1750 IN/MIN, 600 PSI 77 0

TABEL A-53

ANALYSIS OF COVARIANCE TABLE

SOURCES OF SQUARES AND DEGREES OF FREEDOM				ADJUSTED TOTALS				REGRESSION COEFFICIENTS			
SOURCE	DF	SS	MS	Y	DF	SS	MS	Y	DF	SS	MS
BETWEEN	21	0.1632750E+04	0.77750E+01	0.16270E+01	30	0.127259E+01	0.42419E+00	0.769450E+00	117		
WITHIN	31	0.2228750E+04	0.71895E+01	0.441675E+01	30	0.206732E+01	0.68910E+00	0.754820E+00	120		
TOTAL	52	0.386150E+04	0.74322E+01	0.604375E+01	60	0.334000E+01	0.55667E+00	0.160892E+00	120		
ADJUSTED	28	0.1632750E+04	0.58312E+01	0.425142E+01	27	0.104274E+01	0.38620E+00	0.155804E+00	117		
ADJUSTED	121	0.693720E+04	0.57332E+02	0.835743E+01	120	0.614947E+01	0.51245E+00	0.178403E+00	120		
ADJUSTED	3	0.118974E+04	0.12330E+01	0.12330E+01	2	0.110023E+01	0.55011E+00	0.100100E+00	120		
TOTAL	124	0.810694E+04	0.65616E+02	0.558044E+01	123	0.719517E+01	0.57716E+00	0.006000E+00	120		

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.5831 DF = 3, 117  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 6.1771 DF = 3, 120  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 43.0660 DF = 1, 120

ADJUSTED MEAN TENSILE STRENGTH, 1740 IN/INCH, 600 PSI

TABLE A-54

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		TOTALS		ADJUSTED		REGRESSION		RESIDUAL
		SS	MS	SS	MS	SS	MS	SS	MS	
BETWEEN	31	0.182275E+04	0.587984E+03	0.182275E+04	0.587984E+03	0.119742E+08	0.386297E+06	0.359135E+08	0.386297E+06	0.774797E+02
WITHIN	31	0.222275E+04	0.717016E+03	0.222275E+04	0.717016E+03	0.230555E+08	0.745339E+06	0.110198E+07	0.353865E+06	0.214055E+02
TOTAL	62	0.404550E+04	0.652500E+03	0.404550E+04	0.652500E+03	0.349897E+08	0.567336E+06	0.469333E+08	0.760262E+06	0.988852E+02
ADJUSTED	30	0.182275E+04	0.607583E+03	0.182275E+04	0.607583E+03	0.202002E+08	0.673340E+06	0.746376E+06	0.248652E+06	0.828819E+02
AMONG	121	0.697720E+04	0.576628E+03	0.697720E+04	0.576628E+03	0.101522E+09	0.846017E+06	0.175623E+07	0.145523E+06	0.000000E+00
TOTAL	120	0.879995E+04	0.733333E+03	0.879995E+04	0.733333E+03	0.303524E+09	0.252937E+06	0.822473E+06	0.685394E+06	0.000000E+00

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.6831 CF = 3. 117  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 3.0576 CF = 3. 120  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 7.6041 CF = 1. 120

ADJUSTED CROS LOSS 101-10-LOF HR TRIAX TENSILE MODULUS, 1750 IN/MIN, 600 PSI, 77 DEG

TABLE A-55

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	Sums of Squares and Products		Corrected		Deviations from Regression		Regression Coefficient	
		X	Y	XY	CF	SS	VS		
UNLAD	107	0.147220E+05	0.216940E+05	0.246643E+07	106	0.244149E+07	0.230229E+05	0.129733E+01	
LIFED	56	0.378604E+04	0.227350E+05	0.847172E+06	55	0.629701E+06	0.114100E+05	0.756973E+01	
WTHIN	163	0.205000E+03	0.504290E+05	0.821750E+07	162	0.319350E+07	0.197120E+05	0.245258E+01	
TOTAL	1	0.115472E+05	0.773765E+05	0.501024E+06	0	.226751E+02	0.000000E+00	0.000000E+00	
TOTAL	164	0.324552E+05	0.127799E+05	0.581853E+07	163	0.331529E+07	0.203392E+05	0.000000E+00	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 6.4075 DF = 1, 161  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 6.1784 DF = 1, 162  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 6.2405 DF = 1, 162

ANT LIVER VS UNLAD CTNS STRESS RELAXATION 77 DEG F 1A STRAIN ACQUILUS AT 10 SEC



TABLE A-56

## ANALYSIS OF COVARIANCE TABLE

CORRECTED			DEVIATIONS			ABOUT REGRESSION		REGRESSION	
SUMS OF SQUARES AND PRODUCTS								COEFFICIENT	
SOURCE	DF	X	XY	Y	SS	MS			
UNREP	107	0.167220E+05	0.131540E+05	0.547094E+06	104	0.505000E+06	0.882641E+04	0.667025E+00	
UNREP	50	0.372604E+04	0.304107E+05	0.303261E+06	50	0.204844E+06	0.379716E+04	0.512691E+00	
WTRT	163	0.205000E+05	0.205047E+05	0.125140E+07	162	0.121505E+07	0.744331E+04	0.149037E+00	
AWG	1	0.119472E+05	0.341213E+05	0.979170E+05	0	.365025E+01	0.000000E+00	0.000000E+00	
TOTAL	164	0.224552E+05	0.640860E+05	1.134165E+07	163	0.121992E+07	0.748419E+04	0.000000E+00	

\*\*\*\*\*

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 8.6783 DF = 1, 161  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 1.8909 DF = 1, 162  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 6.1198 DF = 1, 162

ANT LINED VS UNLINED CINS STRESS RELAXATION 77 DEG F 1% STRAIN MODULUS AT 1000 S

TABLE A-57

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS				ABOUT REGRESSION		REGRESSION	COEFFICIENT
Sums of Squares and Products											
SOURCE	DF	X	XY	Y	DF	SS	MS				
110	47	0.255800E+04	-0.515500E+04	0.214200E+06	46	0.210699E+06	0.457868E+04	-0.123247E+01			
111	56	0.270604E+04	0.227350E+05	0.247288E+06	55	0.624797E+06	0.114599E+05	0.758972E+01			
112	100	0.265404E+04	0.299700E+05	0.116291E+07	100	0.104597E+07	0.103501E+05	0.402471E+01			
113	1	0.225727E+03	0.490700E+04	0.107141E+06	1	0.218125E+02	0.000000E+00	0.000000E+00			
TOTAL	104	0.657905E+04	0.304770E+05	0.126571E+07	103	0.119853E+07	0.109588E+05	0.000000E+00			

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 12.7866 DF = 1, 101  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 6.6160 DF = 1, 102  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 9.9036 DF = 1, 102

MEAN VS MEAN LINEAR CORRELATION STRESS RELAXATION 77 DEG F IN STRAIN MODULES AT 10 SEC

TABLE A-58

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS		CORRECTED		ELEVATIONS		ADJUST REGRESSION		REGRESSION COEFFICIENT
		X	XY	Y	Y	SS	SP	SS	SP	
TOTAL	47	0.255800E+04	-0.140500E+04	0.978000E+05	42	0.970000E+05	0.210000E+04	0.558000E+06	0.512000E+01	
ADJ	56	0.275000E+04	0.154100E+05	0.800000E+05	53	0.200000E+06	0.275000E+04	0.512000E+01	0.282000E+01	
WITHIN	103	0.655400E+04	0.179750E+05	0.400000E+05	102	0.255000E+06	0.240000E+04	0.282000E+01	0.000000E+00	
AMONG	1	0.225000E+03	0.200000E+04	0.200000E+05	1	0.225000E+06	0.000000E+00	0.000000E+00	0.000000E+00	
TOTAL	104	0.657900E+04	0.205000E+05	0.474000E+05	103	0.270000E+06	0.255000E+04	0.000000E+00	0.000000E+00	

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 16.3351 DF = 1, 101  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 4.4196 DF = 1, 102  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 14.5987 DF = 1, 102

ME VS ADJ LINED CARTONS STRESS RELAY, 77 DEG F, 1X STRAIN, AGGULUS AT 1000 SEC

TABLE A-59

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		TOTAL		DEVIATIONS		ABOUT REGRESSION		REGRESSING	
		X	XY	Y	Y	SS	SS	SS	SS	COEFFICIENT	COEFFICIENT
ANA	24	0.230508E+04	0.205120E+05	0.110140E+07	31	0.517996E+06	0.298128E+05	0.269625E+01			
ANA	53	0.812087E+04	0.252520E+05	0.123795E+07	52	0.120953E+07	0.232601E+05	0.210569E+01			
WITHIN	25	0.109286E+03	0.407040E+05	0.232143E+07	84	0.216775E+07	0.260447E+05	0.556496E+01			
ANALYT	1	0.677750E+03	-0.120500E+05	0.247040E+06	1	0.293125E+02	0.000000E+00	0.000000E+00			
TOTAL	86	0.111143E+05	0.329140E+05	0.263203E+07	85	0.253406E+07	0.298164E+05	0.000000E+00			

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.5498 DF = 1, 85

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 13.3158 DF = 1, 84

F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 7.7050 DF = 1, 84

ANA VS ANA UNLINED CRUIS STRESS RELAXATION 77 DEG F 1% STRAIN MODULUS AT 10 SEC



TABLE A-60  
ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS		CORRECTED		DEVIATIONS		ABOUT REGRESSION		MS	REGRESSION COEFFICIENT
		X	XY	Y	DF	SS	SS	SS	SS		
ANA	32	0.227569E+04	0.410400E+04	0.302590E+05	31	0.266698E+06	0.867413E+04	0.384006E+01			
ANB	52	0.812007E+09	0.172330E+05	0.492827E+06	51	0.435581E+06	0.876887E+04	0.212006E+01			
WITHIN	85	0.104366E+05	0.260910E+05	0.795425E+06	84	0.780153E+06	0.869276E+04	0.250054E+01			
ANCLG	1	0.677750E+03	-0.793590E+04	0.210500E+05	1	0.612500E+01	0.000000E+00	0.000000E+00			
TOTAL	86	0.111143E+05	0.161570E+05	0.866320E+06	85	0.858657E+06	0.101019E+05	0.000000E+00			

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.6085 DF = 1. 83  
F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 14.7782 DF = 1. 84  
F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 7.5941 DF = 1. 84

ANA VS ANB UNLINED CRDS STRESS RELAXATION 77 DEG F 1% STRAIN MODULUS AT 1000 S

TABLE A-61

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	SUMS OF SQUARES AND PRODUCTS			CORRECTED			DEVIATIONS ABOUT REGRESSION			REGRESSION COEFFICIENT
		Y	XY	Y	XY	Y	Y	SS	SS	SS	
AME	22	0.2205651+04	0.2205120E+05	0.110148E+07	31	0.51799E+06	0.296128E+05	0.8896159E+01			
AME	53	0.612187E+04	0.252528E+05	0.125795E+07	52	0.121953E+07	0.237601E+05	0.6105692E+01			
AM	107	0.187260+05	0.215940E+05	0.245782E+07	106	0.244147E+07	0.230327E+05	0.1297333E+01			
WITHEL	192	0.271586E+05	0.674530E+05	0.467604E+07	191	0.466745E+07	0.245375E+05	0.2482857E+01			
AMONG	2	0.515819E+04	-0.379090E+05	0.527124E+06	1	0.151371E+06	0.151371E+06	0.000000E+00			
TOTAL	194	0.353167E+05	0.295490E+05	0.516557E+07	193	0.516084E+07	0.267401E+05	0.000000E+00			

\*\*\*\*\*

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 2.5129 DF = 2, 189  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 9.5766 DF = 2, 191  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 6.8230 DF = 1, 191

AME VS AMBIENT UNILID CTMS STRESS RELAXATION 77 DEG F 1X STRAIN MODULUS AT 10 SEC

TABLE A-62

## ANALYSIS OF COVARIANCE TABLE

REGRESSION COEFFICIENT									
ABOUT REGRESSION									
REVIATIONS									
SUMS OF SQUARES AND PRODUCTS									
CONSTRUCTED									
SOURCE	DF	X	XY	Y	DF	SS	MS	SS	MS
ANA	22	0.230569E+04	0.603460E+04	0.012690E+06	21	0.200890E+06	0.967412E+04	0.3840069E+04	0.3840069E+04
ADR	53	0.812087E+04	0.172380E+05	0.492527E+06	52	0.495981E+06	0.976067E+04	0.2120067E+04	0.2120067E+04
ADY	107	0.167820E+05	0.111540E+05	0.243740E+06	106	0.923600E+06	0.882341E+04	0.882341E+04	0.882341E+04
WITHIN	192	0.271586E+05	0.372460E+05	0.172440E+07	191	0.169730E+07	0.888447E+04	0.1371427E+04	0.1371427E+04
AMONG	2	0.815819E+04	-0.148540E+05	0.989110E+05	1	0.725890E+05	0.725890E+05	0.0000000E+00	0.0000000E+00
TOTAL	194	0.353167E+05	0.225920E+05	0.183730E+07	193	0.182292E+07	0.944520E+04	0.0000000E+00	0.0000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.5312 DF = 2, 189  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 7.6710 DF = 2, 194  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 5.7819 DF = 1, 191

ANA VS. AFRASANT UNLND CINS STRESS RELAXATION 77 DEG F IN STRAIN NODULUS AT 1000 S

TABLE A-63

## ANALYSIS OF COVARIANCE TABLE

CORRECTED									
SUMS OF SQUARES AND PRODUCTS									
DEVIATIONS									
ABOUT REGRESSION									
REGRESSION									
COEFFICIENT									
SOURCE	DF	X	XY	Y	UF	SS	S		
711	8	0.36600E+03	-0.67000E+03	0.32690E+05	7	0.32690E+05	0.463750E+04	-0.102040E+01	
712	8	0.29400E+03	0.36500E+04	0.00000E+05	7	0.10000E+05	0.140348E+04	0.1309520E+02	
713	8	0.26000E+03	0.27165E+04	0.40000E+05	7	0.20000E+05	0.299203E+04	0.102131E+02	
815	8	0.50000E+03	0.119337E+04	0.40000E+05	7	0.40000E+05	0.622634E+04	-0.204344E+01	
820	8	0.341559E+03	0.315112E+04	0.342230E+05	7	0.515160E+04	0.735943E+03	-0.922572E+01	
921	5	0.33750E+03	0.427500E+04	0.582840E+05	4	0.413402E+04	0.102380E+04	-0.126866E+02	
WY+IN	45	0.218906E+04	0.145162E+05	0.281710E+06	44	0.165450E+06	0.421476E+04	0.6631247E+01	
AMONG	5	0.120345E+04	0.121937E+05	0.365090E+06	4	0.291939E+06	0.604948E+05	0.000000E+00	
TOTAL	50	0.339251E+04	0.267099E+05	0.647200E+06	49	0.436907E+06	0.891647E+04	0.000000E+00	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 4.5392 DF = 5, 39  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 11.9322 DF = 5, 44  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 22.6389 DF = 1, 44

ANY LINED CROS LOT-10-LOT STRESS RELAXATION 77 DEG 1% STRAIN MODULUS AT 10 SECS



TABLE A-64

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS				REGRESSION COEFFICIENT
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				
SOURCE	DF	Y	XY	OF	SS	MS		
711	8	0.355000E+03	-0.190000E+03	7	0.131124E+05	0.167177E+04	-0.5151257E+00	
712	8	0.294000E+03	0.203000E+04	7	0.267234E+04	0.410334E+03	0.5904760E+01	
713	8	0.265000E+03	0.209337E+04	7	0.354850E+04	0.506907E+03	0.7869625E+01	
819	8	0.584000E+03	0.245337E+04	7	0.106494E+05	0.154992E+04	0.4200987E+01	
820	8	0.341559E+03	0.227337E+04	7	0.206868E+04	0.295526E+03	0.5655662E+01	
821	5	0.337500E+03	0.330000E+04	4	0.246734E+04	0.616834E+03	0.9777777E+01	
WITHIN	45	0.212906E+04	0.119601E+05	44	0.562578E+05	0.132404E+04	0.5463559E+01	
AMONG	5	0.120245E+04	0.673894E+04	4	0.874032E+05	0.218508E+05	0.0000000E+00	
TOTAL	50	0.339251E+04	0.186991E+05	49	0.145675E+06	0.297296E+04	0.0000000E+00	

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 5.0697 DF = 5 39  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 13.2047 DF = 5 44  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 49.3529 DF = 1 44

ANT LINED CTNS LOT-10-LOT STRESS RELAXATION 77 DEG 1% STRAIN MODULUS AT 1000 SEC

TABLE A-65

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		DEVIATIONS		ABOUT REGRESSION		REGRESSION	
		SUMS OF SQUARES	AND PRODUCTS	Y	CF	SS	MS	COEFFICIENT	
B4C	11	0.350250E+03	0.901250E+04	0.324492E+06	10	0.392500E+06	0.392500E+05	0.2573161E+02	
B44	11	0.872250E+03	-0.755800E+03	0.507670E+05	10	0.501135E+05	0.501135E+04	-0.055775E+00	
AVI-HA	22	0.122250E+04	0.823750E+04	0.675259E+06	21	0.619482E+06	0.294552E+05	0.375461E+01	
AMONG	1	0.735000E+02	0.446250E+04	0.270937E+02	0	-0.375000E+00	0.000000E+00	0.000000E+00	
TOTAL	23	0.129600E+04	0.127200E+05	0.346196E+06	22	0.621251E+06	0.373342E+05	0.000000E+00	

\*\*\*\*\*

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 7.9866 DF = 1, 20  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 6.8432 DF = 1, 21  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 1.8908 DF = 1, 21

ANA UNLND CAPTENS LOT-10-LOT STRESS RELAXATION MODULUS AT 10 SEC, 1X STRAIN

TABLE A-66

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS				REGRESSION	
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				COEFFICIENT	
SOURCE	DF	X	XY	Y	SS	SS	NS		
040	11	0.350250E+03	0.470000E+04	0.173800E+06	1	0.108565E+06	0.108565E+05	0.136473E+02	
044	11	0.572250E+03	-0.120000E+04	0.389000E+05	1	0.371491E+05	0.171491E+04	-0.137575E+01	
WITJA	22	0.122250E+04	0.350000E+04	0.192000E+06	22	0.182116E+06	0.167280E+04	0.292842E+01	
AMONG	1	0.735000E+02	0.210000E+04	0.800000E+05	1	0.000000E+00	0.000000E+00	0.000000E+00	
TOTAL	23	0.129600E+04	0.568000E+04	0.252600E+06	22	0.227706E+06	0.103503E+05	0.000000E+00	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 8.9730 DF = 1, 20  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 5.2570 DF = 1, 21  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 1.2089 DF = 1, 21

ANA UNLNO CARTONS LOT-TO-LOT STRESS RELAXATION MODULUS AT 1000 SEC. 1% STRAIN

TABLE A-67

## ANALYSIS OF COVARIANCE TABLE

SOURCE				CORRECTED				DEVIATIONS				REGRESSION	
SOMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				ABOUT REGRESSION				COEFFICIENT	
SOURCE	DF	X	XY	Y	EF	SS	AS						
504	20	0.249257E+04	-0.241453E+03	0.002701E+06	19	0.640006E+06	0.236045E+05					-0.1004977E+02	
505	20	0.125000E+04	-0.152931E+04	0.466707E+02	19	0.451511E+06	0.241479E+05					-0.1213739E+01	
696	20	0.148900E+04	-0.529000E+04	0.241475E+05	19	0.222343E+06	0.117022E+05					-0.562231E+01	
724	23	0.114562E+04	-0.523625E+03	0.197799E+06	22	0.157697E+06	0.897711E+04					-0.515802E+00	
822	5	0.150000E+01	-0.700000E+02	0.060000E+04	4	0.253333E+04	0.633333E+03					-0.466666E+02	
WITHIN	80	0.629770E+04	-0.317232E+05	0.178879E+07	67	0.162899E+07	0.187241E+05					-0.503727E+01	
AMONG	4	0.705299E+04	0.423792E+05	0.408665E+06	3	0.154322E+06	0.514407E+05					0.000000E+00	
TOTAL	92	0.133507E+05	0.106560E+05	0.219776E+07	91	0.216925E+07	0.240577E+05					0.000000E+00	

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 1.4705 DF = 4, 83  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 7.4805 DF = 4, 87  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 8.5344 DF = 1, 87

ANT UNLND CAPTIONS LOT-10-LOT STRESS RELAXATION MODULUS AT 10 SEC, 1X STRAIN



TABLE A-68

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		DEVIATIONS		REGRESSION	
		SS	SS	SS	SS	SS	SS
ABF	20	0.145800E+04	-0.391000E+04	0.921100E+03	19	0.019592E+05	0.431364E+04
724	23	0.119562E+04	-0.177625E+04	0.094600E+03	22	0.007420E+05	0.894262E+04
684	20	0.240257E+04	-0.124771E+04	0.029010E+03	19	0.027718E+06	0.119052E+05
205	20	0.126000E+04	-0.940000E+03	0.197524E+03	19	0.196023E+06	0.102591E+05
822	5	0.150000E+04	-0.250000E+02	0.188237E+04	4	0.106671E+04	0.268677E+03
WITHIN	88	0.629770E+04	-0.191284E+05	0.073099E+06	87	0.615699E+06	0.707471E+04
AMONG	4	0.705299E+04	0.233634E+05	0.167793E+06	3	0.110400E+06	0.368001E+05
TOTAL	92	0.133507E+05	0.423500E+04	0.061392E+06	91	0.000048E+06	0.945108E+04

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F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.7399 DF = 4, 83  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 8.6417 DF = 4, 87  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIATE = 8.2123 DF = 1, 87

ANT UNLND CARTONS LOT-TO-LOT STRESS RELAXATION MODULUS AT 1000 SEC. 1% STRAIN

TABLE A-69

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED SUMS OF SQUARES AND PRODUCTS		DEVIATIONS ABOUT REGRESSION		VS	REGRESSION COEFFICIENT
		X	XY	Y	SS		
UNLINE	236	0.431144E+05	0.181469E+06	0.264266E+07	0.187868E+07	0.799440E+04	0.4209471E+01
LINE	53	0.466350E+04	-0.253100E+04	0.811940E+05	0.797303E+05	0.152328E+04	-0.342725E+01
WITHIN	289	0.477779E+05	0.173954E+06	0.272376E+07	0.205345E+07	0.713004E+04	0.374582E+01
ANCOV	1	0.600062E+04	-0.335920E+05	0.527809E+05	0.113719E+03	0.000000E+00	0.000000E+00
TOTAL	290	0.544380E+05	0.160360E+06	0.277581E+07	0.200343E+07	0.797034E+04	0.000000E+00

\*\*\*\*\*

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 13.3276 DF = 1, 287

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 35.0598 DF = 1, 288

F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 94.0119 DF = 1, 289

\*\*\*\*\*

ANT LINE VS UNLID CARTON'S TOL (TOL ABOVE GLASS POINT)

TABLE A-70

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRECTED		DEVIATIONS		SS	MS	REGRESSION COEFFICIENT
		SS	XY	Y	DF			
UNLINED	267	0.564540E+03	0.163600E+03	0.033400E+04	266	0.613353E+04	0.214459E+02	0.268730E+02
LINED	53	0.466250E+04	-0.466000E+03	0.232000E+03	52	7.165034E+03	0.355835E+01	-0.100392E+01
WITHIN	340	0.611175E+03	-0.305000E+03	0.636800E+04	339	0.636844E+04	0.187743E+02	-0.499036E+02
AMONG	1	0.104600E+03	-0.129400E+04	0.167000E+03	0	.796950E+01	0.000000E+00	0.000000E+00
TOTAL	341	0.715777E+03	-0.159900E+04	0.652000E+04	340	0.649028E+04	0.190851E+02	0.000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES =

2.4561

DF =

1.

339

F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS =

6.7006

DF =

1.

339

F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE =

0.0811

DF =

1.

339

ANT LINED VS UNLINED CANYONS TOE (GLASS POINT)

TABLE A-71

## ANALYSIS OF COVARIANCE TABLE

CORRECTED				DEVIATIONS				REGRESSION	
SUMS OF SQUARES AND PRODUCTS				ABOUT REGRESSION				COEFFICIENT	
SOURCE	DF	X	XY	Y	SS	DF	MS		
AREA	105	0.405283E+05	0.572437E+03	0.298106E+04	0.292700E+04	104	0.267217E+02	0.159663E+01	
AREA	281	0.741842E+05	0.237100E+04	0.510400E+04	0.502822E+04	280	0.179579E+02	0.315679E+01	
WATER	385	0.115112E+05	0.294344E+04	0.209506E+04	0.202360E+04	384	0.208410E+02	0.255700E+01	
AREA	1	0.101022E+03	-0.127370E+03	0.278775E+03	0.157166E+01	0	0.000000E+00	0.000000E+00	
TOTAL	387	0.115214E+05	0.277600E+04	0.837106E+04	0.821111E+04	386	0.215314E+02	0.000000E+00	

\*\*\*\*\*

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.4083 DF = 1, 384  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 13.7361 DF = 1, 385  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 2.5113 DF = 1, 385

AREA UNLND VS ARE UNLND CAUTIONS TOLE ABOVE GLASS POINT)



TABLE A-72

## ANALYSIS OF COVARIANCE TABLE

COLUMNS				DEVIATIONS				REGRESSION			
SQUARES AND PRODUCTS				ABOUT MEANS				COEFFICIENT			
SOURCE	DF	X	XY	Y	DF	SS	AS				
ANA	99	0.370953E+05	0.220961E+06	0.230116E+07	99	0.921458E+06	0.540243E+04	0.602672E+01			
AMB	281	0.741842E+05	-0.140340E+05	0.814733E+07	281	0.214018E+07	0.290721E+05	-0.189177E+00			
WTF-ID	379	0.112179E+06	0.211527E+06	0.106440E+06	379	0.100222E+06	0.264703E+05	0.191592E+01			
WCC-C	1	0.425125E+03	0.684900E+04	0.117108E+06	1	-0.154569E+03	0.000101E+00	0.000100E+00			
TOTAL	381	0.112610E+06	0.221776E+06	0.105513E+06	380	0.101345E+08	0.266172E+05	0.000000E+00			

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 40.4879 DF = 1, 379  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 3.1096 DF = 1, 379  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANCE = 15.5564 DF = 1, 379

ANA UNLID VS AMB UNLID CARTONS TOL (GLASS POINT)

TABLE A-73

## ANALYSIS OF COVARIANCE TABLE

SOURCE	DF	CORRELATED SUMS OF SQUARES AND PRODUCTS		DEVIATIONS ABOUT REGRESSION		AS	REGRESSION COEFFICIENT
		X	XY	Y	SS		
ANA	99	0.378953E+05	0.226986E-01	0.230280E-07	98	0.922778E-08	0.541610E-10
AME	281	0.741842E+05	-0.141235E-02	0.144158E-07	281	0.816141E-07	0.290765E-19
ANT	239	0.431144E+05	0.181574E-01	0.684705E-07	239	0.165002E-07	0.800128E-10
ATHT	615	0.152594E+06	0.396433E-01	0.120175E-06	615	0.120797E-06	0.106418E-09
AMONG	2	0.120631E+05	-0.902095E-02	0.927206E-08	1	0.242596E-08	0.243596E-08
TOTAL	616	0.167357E+06	0.305624E-01	0.140190E-06	617	0.134609E-06	0.216166E-09

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 31.7996 DF = 2: 613  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 35.1496 DF = 2: 615  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 51.5235 DF = 1: 615

ANA VS AGE VS ANT UNLIMITED CARRIAGES TOLE (TOLE ABOVE GLASS POINT)

TABLE A-74

ANALYSIS OF COVARIANCE TABLE

SUMS OF SQUARES AND PRODUCTS      CORRECTED      DEVIATIONS      ABOUT REGRESSION

SOURCE	DF	X	XY	Y	DF	SS	AS	REGRESSION COEFFICIENT
AMB	105	0.405263E+05	0.572437E+03	0.259506E+04	104	0.258706E+04	0.287217E+02	0.1398634E-01
AMB	261	0.741642E+05	0.237100E+04	0.510900E+04	260	0.502822E+04	0.175579E+02	0.3196758E-01
WYTH	287	0.564540E+05	0.163000E+03	0.913400E+04	286	0.613233E+04	0.214459E+02	0.2887304E-01
WYTH	673	0.171566E+06	0.310544E+04	0.142321E+05	672	0.141768E+05	0.210924E+02	0.1810631E-01
AMONG	2	0.682750E+04	0.130756E+04	0.600937E+03	1	0.356521E+03	0.350521E+03	0.000000E+00
TOTAL	675	0.178394E+06	0.441400E+04	0.148340E+05	674	0.147248E+05	0.218469E+02	0.000000E+00

F RATIO FOR TESTING DIFFERENCES BETWEEN SLOPES = 0.6632 DF = 2, 670  
 F RATIO FOR TESTING DIFFERENCES BETWEEN ELEVATIONS = 12.9872 DF = 2, 672  
 F RATIO FOR TESTING SIGNIFICANCE OF COVARIANT = 2.6661 DF = 1, 672

AMB VS AMB VS ANY UNLITTED CARTONS 10LE (GLASS POINT)

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<p>This report contains test results from testing of Minuteman III, Stage III propellant manufactured by Aerojet Solid Propulsion Company and Thiokol Corporation, Wasatch Division. These results are compared statistically with propellant of similar ages from Minuteman II Stage II.</p> <p>Regressions are given for only statistically significant parameters from very low rate tensile, high rate biaxial tensile under pressure, stress relaxation and thermal coefficient of linear expansion tests. There are some significant regressions in each of these tests. (OVER)</p>		

↓  
Case liner bonds also show significant changes which are potentially life limiting.

Significant changes in other parameters may be the result of limited testing, both in numbers and ages.

Analysis of covariance for test data from lined and unlined cartons of Stage II and Stage III propellant and for the four tests listed above are given in the statistical appendix.

